



Lake Street/4th Street/Central Avenue
Intersection Control Evaluation (ICE)
Report

City of Madera

**Lake Street/4th Street/Central Avenue
Intersection Control Evaluation (ICE) Report**

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1. Introduction

1.1 Purpose

This document has been prepared to present the results of a conceptual alternatives analysis performed by Omni-Means for the City of Madera in support of the Intersection Control Evaluation (ICE) process. The analysis evaluates potential alternative improvements at the Lake Street/4th Street/Central Avenue intersection. Though this intersection is not on the state highway system, this analysis has been conducted consistent with guidelines provided in Caltrans Traffic Operations Policy Directive 13-02 for intersection improvements on the state highway system.

The purpose of the study is to identify viable alternatives (project) to improve safety, reduce delay, and enhance mobility for all travel modes at the intersection of Lake Street/4th Street/Central Avenue. The project would improve traffic circulation, access, and safety for all modes of transportation. It would relieve anticipated future traffic congestion associated with planned development in the City and improve local traffic circulation.

The intersection of Lake Street/4th Street/Central Avenue is located in the northeast quadrant of the City of Madera, in the urbanized City limits, south of the Fresno River, east of SR 99 and northwest of Highway 145. Although this intersection currently does not experience severe delay or congestion, traffic forecast data shows this intersection reaching an LOS of E in the PM peak hour by the year 2040. There are five approaches to the intersection (as shown in Figure 1) and the 5-legged nature of this intersection presents unique design challenges.



Figure 1: Study Area

This document contains a description of the following sections consistent with the Caltrans ICE document guidelines including:

- Screening Objectives;
- Screening Criteria;
- Capacity Assessment/Analysis;
- Footprint Development & Assessment;
- Safety Considerations
- Life-Cycle Costs; and
- Recommendations & Documentation.

1.2 Project Setting/ Land Use

The intersection of Lake Street/4th Street/Central Avenue is located in the northeast quadrant of the City of Madera, east of SR 99 and northwest of Highway 145. Lake Street serves as a north-south arterial in the City. About half a mile to the southwest Lake Street intersects Sunrise Avenue, and at the study intersection Lake Street turns and continues due north well beyond the City limits. The southwest leg of 4th Street is an arterial and has an interchange with SR 99 about half a mile southwest of the study intersection. The northeast leg of 4th Street is a local road that terminates at Flume Street after one block. Central Avenue is an east/west collector street that extends from H Street to Lake Street.

The primary land use directly adjacent to the study intersection is single family residential. Centennial Park is located northeast of the intersection at the end of 4th Street. It includes a pool, youth and community center, and a community garden. City of Madera Fire Station #6 is located north of the study intersection on Lake Street. Although there are residential homes located at each corner of the intersection, there are not a significant number of driveways. Most properties in this area have their access off of an alley that serves as a communal driveway for an entire block of houses. This will result in minimal impacts to property access, even if there are other property impacts around the intersection. There is also a significant heavy vehicle presence at this intersection during the morning peak hour.

Lake Street crosses the Fresno River approximately 400 feet north of the study intersection. The bridge at this location is a constraint and any impacts to it should be avoided.

2. Screening Objectives

In August 2013, Caltrans issued Traffic Operations Policy Directive (TOPD) 13-02 regarding Intersection Control Evaluation (ICE). According to this directive, all proposals to install or modify intersection control on state highways must consider all three intersection control strategies (traffic signal, yield control roundabout, and all-way stop control) and the supporting design configurations during the ICE screening process. Consistent with the intent of this Directive, the objective of this report is to determine which of these intersection control strategies are context-appropriate, practical to implement, and merit further consideration.

2.1 Project Analysis Scenarios

This section contains a brief description of the time frames for which the traffic operations analysis was conducted. The project design alternatives (discussed within the next section) were analyzed for Existing Year (Year 2017) and Design Year (Year 2040) conditions. The analysis was

conducted for both the AM and PM peak hour conditions. The peak hour turning movement volumes are summarized on Figure 2.

Comparing the traffic data, the AM and PM peak hours are fairly balanced, but there are about 10% more vehicles entering the intersection in the PM peak hour. Northbound Lake Street and eastbound 4th Street have significantly more vehicles in the PM peak hour than in the AM Peak Hour. The other three legs are more balanced between the two peak hours.

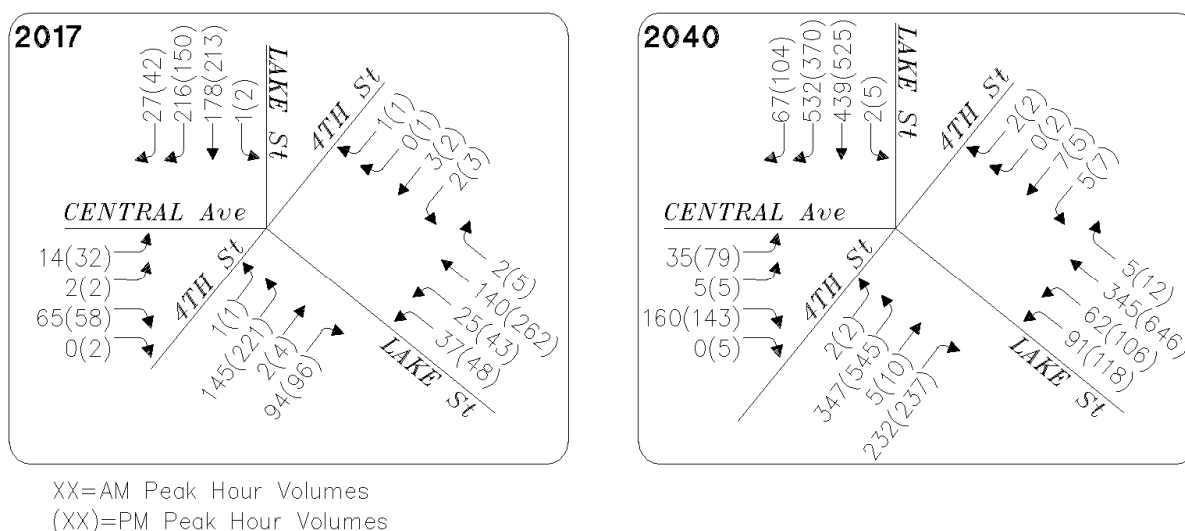


Figure 2: Peak Hour Traffic Volumes

A comparison of volumes by directionality (NB and SB on the corridor) indicated that, in general, the northbound traffic volumes (northbound Lake Street and 4th Street) are higher than the southbound Lake Street volumes. This trend is more significant in the PM peak hour.

One of the primary objectives of TOPD 13-02 is to balance the needs of all modes and users with system performance goals. For that reason, volumes for pedestrians and bicycles were also collected and analyzed. There were 6 cyclists using the study intersection during the AM peak hour and 10 in the PM peak hour. In the AM peak hour, about half of the cyclists were approaching from Central Avenue. In the PM peak hour, about half were approaching from the northeast leg of 4th Street. About 24 pedestrians used the intersection during the AM peak hour and about 27 pedestrians in the PM peak hour. Pedestrians cross on each leg of the intersection during both peak hours.

2.1.1 Existing Year (2017)

Traffic volumes collected in February 2017 during both AM and PM peak hours are utilized in this study. Pedestrian, cyclist, and truck volumes were measured as part of the counts, and peak hour factors were determined. These volumes were used as a base line for future year projections. See Figure 2 for a summary of the turning movement volumes for the study intersection.

2.1.2 Design Year (2040)

Omni-Means received year 2035 forecast volumes from the Madera County Transportation Commission (MCTC) Regional Travel Demand Model (RTDM) on February 22, 2017. The forecast volumes were link-based volumes; therefore, Omni-Means converted the existing traffic

count data to approach volumes, in order to compare them to the data provided by MCTC. The growth rates between the existing traffic counts and MCTC's 2035 traffic forecast volumes were calculated for each leg of the intersection and were found to be about 4%.

As a 4%/year growth rate seemed high, Omni-Means requested existing year volumes that were used in the MCTC RTDM. Omni-Means received the requested 2017 link based traffic volumes from the RTDM and determined that these traffic volumes had an average annual growth rate of about 0-1.1% between the RTDM's 2017 and 2035 volumes. Based on this determination, Omni-Means used a 1% annual growth rate applied on the existing turning movements' counts to the year 2040. See Figure 2 for the forecasted 2040 traffic volumes.

2.2 Project Design Alternatives

This study analyzes three alternatives. The first is a No Build Alternative that assumes existing lane geometrics and all-way stop control. The second alternative is signalization with modified lane geometrics. The third alternative is a yield-control roundabout with modified lane geometrics.

2.2.1 No Build Alternative

The No-Build Alternative leaves the existing lane geometrics and all-way stop-control in place.

2.2.2 Traffic Signal Alternative

With this alternative, the intersection is signalized and the lane geometrics have been modified to accommodate the Design Year volumes. The northeast leg of 4th Street will be terminated at the alley, and the intersection will only feature 4 legs. The Signal Alternative lane geometrics can be found on Figure 3 and is provided in Appendix B of this report.

2.2.3 Roundabout Alternative

This alternative would replace the intersection with a modern single lane roundabout designed to accommodate the Design Year traffic forecast volumes. The northeast leg of 4th Street will be terminated at the alley, and the intersection will only feature 4 legs. The Roundabout Alternative layout shown on Figure 4 and is provided in Appendix C of this report.

3. Screening Criteria

The traffic operations for the No-Build Alternative, Signal Alternative, and Roundabout Alternative were analyzed for the AM and PM peak hours under existing (2017) and design (2040) year conditions.

Both the No-Build and Signal Alternatives were analyzed using Synchro 9 and SimTraffic analysis software. Synchro 9 is a macroscopic analysis and optimization application that reports the Level of Service (LOS) and delay as per the Highway Capacity Manual (HCM) 2010 methodologies. SimTraffic is a traffic micro-simulation application that individually tracks and records each vehicle in the model simulating real world conditions. SimTraffic was used to record queuing characteristics for the No-Build and Traffic Signal Alternatives.

SIDRA analysis software was used for the Roundabout Alternative to determine the LOS, volume to capacity ratio (V/C), delay, and the 95th percentile queues. The volume to capacity ratio (V/C) compares roadway demand (vehicle volume) with roadway carrying capacity. A V/C of 1.00 indicates that a roadway facility is operating at full capacity.

3.1 Traffic Operations Analysis

Traffic operations have been quantified through the determination of LOS. LOS is a qualitative measure of traffic conditions, whereby a letter grade "A" through "F" is assigned to an intersection or roadway segment representing progressively worsening traffic conditions. LOS definitions for different types of intersection controls are outlined in Table 1.

**TABLE 1
LEVEL-OF-SERVICE (LOS) CRITERIA**

| LOS | Type of Flow | Delay | Maneuverability | Stopped Delay/Vehicle | |
|----------|---------------------------|--|---|------------------------|------------------------|
| | | | | Signal/ Rndbt | Unsig- nalized |
| A | Stable Flow | Very slight delay. Progression is very favorable, with most vehicles arriving during the green phase not stopping at all. | Turning movements are easily made, and nearly all drivers find freedom of operation. | < 10.0 | < 10.0 |
| B | Stable Flow | Good progression and/or short cycle lengths. More vehicles stop than for LOS A, causing higher levels of average delay. | Vehicle platoons are formed. Many drivers begin to feel somewhat restricted within groups of vehicles. | >10.0 and < 20.0 | >10.0 and < 15.0 |
| C | Stable Flow | Higher delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures may begin to appear at this level. The number of vehicles stopping is significant, although many still pass through the intersection without stopping. | Back-ups may develop behind turning vehicles. Most drivers feel somewhat restricted | >20.0 and < 35.0 | >15.0 and < 25.0 |
| D | Approaching Unstable Flow | The influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high volume-to-capacity ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable. | Maneuverability is severely limited during short periods due to temporary back-ups. | >35.0 and < 55.0 | >25.0 and < 35.0 |
| E | Unstable Flow | Generally considered to be the limit of acceptable delay. Indicative of poor progression, long cycle lengths, and high volume-to-capacity ratios. Individual cycle failures are frequent occurrences. | There are typically long queues of vehicles waiting upstream of the intersection. | >55.0 and < 80.0 | >35.0 and < 50.0 |
| F | Forced Flow | Generally considered to be unacceptable to most drivers. Often occurs with over saturation. May also occur at high volume-to-capacity ratios. There are many individual cycle failures. Poor progression and long cycle lengths may also be major contributing factors. | Jammed conditions. Back-ups from other locations restrict or prevent movement. Volumes may vary widely, depending principally on the downstream back-up conditions. | > 80.0 | > 50.0 |

In the City's General Plan Circulation and Infrastructure Element, Policy CI-22 states that "in the Downtown District (as defined in the Land Use Element of this General Plan), the City shall seek to maintain LOS D." This intersection is located within the Downtown District; therefore, LOS "D"

is assumed to represent the appropriate LOS target.

In addition to providing acceptable LOS and delay, a goal of the build alternatives will be to reduce standing queues on all approaches.

3.2 Analysis Factors

The following criteria are incorporated in the analysis in order to most accurately reflect intersection operating conditions:

- The peak hour factor (PHF) was calculated based on data from the traffic counts collected in February 2017. The PHF represents how constant vehicle volumes are during the peak hour and is equal to the peak hour volume divided by 4 times the peak 15-minute volume. A PHF of 0.81 was used for the AM peak hour, and a PHF of 0.98 was used for the PM peak hour.
- Truck percentages were calculated based on data from counts collected in February 2017. The AM peak hour experiences about 4% heavy vehicles, and about 1% in the PM peak hour.
- SIDRA software includes an environmental factor that modifies capacity reflecting driver response times, standard of intersection geometry, visibility, operating speeds, vehicle sizes, pedestrian interference, parking, buses stopping, etc. For the analysis performed for this report, an environmental factor of 1.02 was used for roundabout analysis.

4. Capacity Assessment/Analysis – Existing Intersection (5-Leg)

Section 4 includes a capacity assessment and analysis of the existing 5-legged Lake Street/4th Street/Central Avenue intersection for the No Build Alternative as well as for a Traffic Signal Alternative and for a Roundabout Alternative. Each alternative is evaluated under both Existing (2017) and Design Year (2040) conditions. LOS worksheets for each alternative are provided in Appendix A.

4.1 No Build Analysis

The following section summarizes the traffic operations analysis and results for the No-Build Alternative under Existing (2017) and Design Year (2040) conditions. LOS worksheets for each analysis condition are provided in Appendix A.

4.1.1 Existing Year (2017)

Tables 2A and 2B present the Existing Condition peak hour intersection LOS and delay for the No Build Alternative.

**TABLE 2A
NO BUILD - EXISTING YEAR (2017) AM PEAK HOUR TRAFFIC OPERATIONS**

| Intersection/Approach | Delay (sec) ² | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|-----------------------------|---------------------|----------------------|--|
| Intersection | 10.2 | B | -- | |
| Northbound Lake Street Left/Thru/Right | 9.9 | A | 350 | 75 |
| Southbound Lake Street Left/Thru | 15.9 | B | 660 | 190 |
| Southbound Lake Street Right | | | 65 | 20 |
| Eastbound 4th Street Left | 7.4 | A | 60 | 50 |
| Eastbound 4th Street Thru | | | 320 | 10 |
| Eastbound 4th Street Right | | | 75 | 40 |
| Eastbound Central Avenue Left/Thru/Right | 11.5 | B | 445 | 70 |
| Westbound 4th Street Left/Thru/Right | 8.4 | A | 325 | 25 |

1. V/C ratio not available for 5-leg AWSC intersection.

2. Traffic Operation outputs calculated using SimTraffic simulation results.

As shown in Table 2A, the No Build Alternative is currently providing acceptable intersection LOS and delay for the study intersection during the AM peak hour. The No Build Alternative has acceptable 95th percentile queues for all movements.

**TABLE 2B
NO BUILD - EXISTING YEAR (2017) PM PEAK HOUR TRAFFIC OPERATIONS**

| Intersection/Approach | Delay (sec) ² | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|-----------------------------|---------------------|----------------------|--|
| Intersection | 14.8 | B | -- | |
| Northbound Lake Street Left/Thru/Right | 18.2 | B | 350 | 170 |
| Southbound Lake Street Left/Thru | 20.1 | C | 660 | 175 |
| Southbound Lake Street Right | | | 65 | 20 |
| Eastbound 4th Street Left | 12.5 | C | 60 | 75 |
| Eastbound 4th Street Thru | | | 320 | 20 |
| Eastbound 4th Street Right | | | 75 | 35 |
| Eastbound Central Avenue Left/Thru/Right | 13.2 | C | 445 | 75 |
| Westbound 4th Street Left/Thru/Right | 5.8 | A | 325 | 30 |

1. V/C ratio not available for 5-leg AWSC intersection.

2. Traffic Operation outputs calculated using SimTraffic simulation results.

As shown in Table 2B, the No Build Alternative is currently providing acceptable intersection LOS and delay the study intersection during the PM peak hour. The No Build Alternative has acceptable 95th percentile queues for all movements, except for the following:

- The queue for the eastbound 4th Street left-turn exceeds the available storage.

4.1.2 Design Year (2040)

Tables 3A and 3B present the Design Year Condition peak hour intersection LOS and delay for the No Build Alternative.

**TABLE 3A
NO BUILD - DESIGN YEAR (2040) AM PEAK HOUR TRAFFIC OPERATIONS**

| Intersection/Approach | Delay (sec) ² | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|-----------------------------|---------------------|----------------------|--|
| Intersection | 23.0 | C | -- | |
| Northbound Lake Street Left/Thru/Right | 15.1 | B | 350 | 125 |
| Southbound Lake Street Left/Thru | 42.3 | E | 660 | 420 |
| Southbound Lake Street Right | | | 65 | 195 |
| Eastbound 4th Street Left | 10.6 | B | 60 | 70 |
| Eastbound 4th Street Thru | | | 320 | 20 |
| Eastbound 4th Street Right | | | 75 | 50 |
| Eastbound Central Avenue Left/Thru/Right | 12.7 | B | 445 | 90 |
| Westbound 4th Street Left/Thru/Right | 8.0 | A | 325 | 20 |

1. V/C ratio not available for 5-leg AWSC intersection.

2. Traffic Operation outputs calculated using SimTraffic simulation results.

As shown in Table 3A, the No Build Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The projected 95th percentile queues are accommodated for all movements, except for the following:

- The projected queue for the southbound Lake Street right-turn exceeds the available storage.
- The queue for the eastbound 4th Street left-turn exceeds the available storage.

**TABLE 3B
NO BUILD - DESIGN YEAR (2040) PM PEAK HOUR TRAFFIC OPERATIONS**

| Intersection/Approach | Delay (sec) ² | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|---|-----------------------------|---------------------|----------------------|--|
| Intersection | 43.4 | E | -- | |
| Northbound Lake Street Left/Thru/Right | 53.4 | F | 350 | 380 |
| Southbound Lake Street Left/Thru | 59.6 | F | 660 | 415 |
| Southbound Lake Street Right | | | 65 | 240 |
| Eastbound 4th Street Left | 39.7 | E | 60 | 125 |
| Eastbound 4th Street Thru | | | 320 | 260 |
| Eastbound 4th Street Right | | | 75 | 135 |
| Eastbound Central Avenue Left/Thru/Right | 15.2 | B | 445 | 70 |
| Westbound 4th Street Left/Thru/Right | 14.0 | B | 325 | 30 |

1. V/C ratio not available for 5-leg AWSC intersection.

2. Traffic Operation outputs calculated using SimTraffic simulation results.

As shown in Table 3B, the No Build Alternative is not projected to provide acceptable intersection LOS or delay for the study intersection during the PM peak hour. The projected 95th percentile

queues are accommodated for all movements, except for the following:

- The projected queue for the northbound Lake Street exceeds the available storage and would spill back into the intersection of 5th Street.
- The projected queue for the southbound Lake Street right-turn lane exceeds the available storage.
- The queues for the eastbound 4th Street left-turn and right-turn lanes exceed the available storages.

4.2 Traffic Signal Analysis

This section provides a summary of the AM and PM peak hour intersection operations associated with installation of a traffic signal with the existing 5-legged intersection under Existing Year (2017) and Design Year (2040) conditions. LOS worksheets for each analysis condition and lane geometrics used for this analysis are provided in Appendix A.

4.2.1 Existing Year (2017)

Tables 4A and 4B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile queues for Existing Year conditions during AM and PM peak hour conditions, respectively.

**TABLE 4A
SIGNAL - EXISTING YEAR (2017) AM PEAK HOUR TRAFFIC OPERATIONS**

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | 0.46 | 20.4 | C | -- | |
| Northbound Lake Street Left | 0.43 | 17.7 | B | 200 | 30 |
| Northbound Lake Street Thru/Right | | | | 350 | 65 |
| Southbound Lake Street Left | 0.49 | 18.8 | B | 100 | 0 |
| Southbound Lake Street Thru | | | | 660 | 105 |
| Southbound Lake Street Right | | | | 200 | 135 |
| Eastbound 4th Street Left | 0.39 | 22.8 | C | 150 | 40 |
| Eastbound 4th Street Left | | | | 320 | 110 |
| Eastbound 4th Street Thru/Right | | | | 320 | 25 |
| Eastbound Central Avenue Left/Thru/Right | 0.52 | 28.8 | C | 445 | 85 |
| Westbound 4th Street Left | 0.01 | 21.3 | C | 100 | 0 |
| Westbound 4th Street Thru/Right | | | | 325 | 10 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 4A, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Traffic Signal Alternative has acceptable 95th percentile queues for all movements.

TABLE 4B
SIGNAL - EXISTING YEAR (2017) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | 0.45 | 20.2 | C | -- | |
| Northbound Lake Street Left/Thru/Right | 0.47 | 18.0 | B | 200 | 105 |
| Northbound Lake Street Thru/Right | | | | 350 | 155 |
| Southbound Lake Street Left | 0.44 | 18.8 | B | 100 | 5 |
| Southbound Lake Street Left/Thru | | | | 660 | 100 |
| Southbound Lake Street Right | | | | 200 | 60 |
| Eastbound 4th Street Left | 0.44 | 22.2 | C | 150 | 40 |
| Eastbound 4th Street Left | | | | 320 | 145 |
| Eastbound 4th Street Thru/Right | | | | 320 | 25 |
| Eastbound Central Avenue Left/Thru/Right | 0.50 | 28.2 | C | 445 | 85 |
| Westbound 4th Street Left | 0.01 | 20.3 | C | 100 | 5 |
| Westbound 4th Street Thru/Right | | | | 325 | 15 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 4B, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Traffic Signal Alternative has acceptable 95th percentile queues for all movements.

4.2.2 Design Year (2040)

Tables 5A & 5B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile queues for Design Year conditions during AM and PM peak hour conditions, respectively.

TABLE 5A
SIGNAL - DESIGN YEAR (2040) AM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | 0.56 | 25.7 | C | -- | |
| Northbound Lake Street Left | 0.53 | 21.9 | C | 200 | 95 |
| Northbound Lake Street Thru/Right | | | | 360 | 155 |
| Southbound Lake Street Left | 0.63 | 24.2 | C | 100 | 5 |
| Southbound Lake Street Thru | | | | 660 | 125 |
| Southbound Lake Street Right | | | | 200 | 155 |
| Eastbound 4th Street Left | 0.51 | 29.4 | C | 150 | 115 |
| Eastbound 4th Street Left | | | | 320 | 65 |
| Eastbound 4th Street Thru/Right | | | | 320 | 15 |
| Eastbound Central Avenue Left/Thru/Right | 0.50 | 31.8 | C | 445 | 90 |
| Westbound 4th Street Left | 0.02 | 27.0 | C | 100 | 0 |
| Westbound 4th Street Thru/Right | | | | 325 | 15 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 5A, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Traffic Signal Alternative

has acceptable 95th percentile queues for all movements. Although the intersection delay and LOS are acceptable, they are worse than those projected for the No Build Alternative. The main long-term benefit of the Traffic Signal Alternative is the reduction in 95th percentile queues and delay on the southbound Lake Street approach.

TABLE 5B
SIGNAL - DESIGN YEAR (2040) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | 0.55 | 26.4 | C | -- | |
| Northbound Lake Street Left/Thru/Right | 0.49 | 21.6 | C | 200 | 110 |
| Northbound Lake Street Thru/Right | | | | 360 | 260 |
| Southbound Lake Street Left | 0.55 | 25.1 | C | 100 | 5 |
| Southbound Lake Street Left/Thru | | | | 660 | 150 |
| Southbound Lake Street Right | | | | 200 | 130 |
| Eastbound 4th Street Left | 0.60 | 31.0 | C | 150 | 110 |
| Eastbound 4th Street Left | | | | 320 | 200 |
| Eastbound 4th Street Thru/Right | | | | 320 | 45 |
| Eastbound Central Avenue Left/Thru/Right | 0.52 | 34.2 | C | 445 | 140 |
| Westbound 4th Street Left | 0.02 | 27.0 | C | 100 | 10 |
| Westbound 4th Street Thru/Right | | | | 325 | 15 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 5B, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Traffic Signal Alternative also has acceptable 95th percentile queues for all movements. For the design year PM peak hour, the Traffic Signal Alternative operates better than the No Build Alternative by reducing intersection delay from 43.4 seconds to 26.4 seconds and eliminates all 95th percentile queuing impacts.

4.3 Roundabout Analysis

This section provides a summary of the AM and PM peak hour intersection operations associated with installation of a roundabout with the existing 5-legged intersection under Existing Year (2017) and Design Year (2040) conditions. LOS worksheets for each analysis condition and lane geometrics used for this analysis are provided in Appendix A.

4.3.1 Existing Year (2017)

Tables 6A and 6B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile queues for Existing Year conditions during AM and PM peak hour conditions, respectively.

TABLE 6A
ROUNABOUT - EXISTING YEAR (2017) AM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.49 | 7.4 | A | -- | |
| Northbound Lake Street | 0.23 | 5.4 | A | 350 | 35 |
| Southbound Lake Street | 0.49 | 9.1 | A | 660 | 100 |
| Eastbound 4th Street | 0.30 | 6.7 | A | 320 | 50 |
| Eastbound Central Avenue | 0.13 | 6.0 | A | 445 | 20 |
| Westbound 4th Street | 0.01 | 4.1 | A | 325 | 0 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 6A, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements.

TABLE 6B
ROUNABOUT - EXISTING YEAR (2017) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.44 | 7.4 | A | -- | |
| Northbound Lake Street | 0.44 | 8.5 | A | 350 | 80 |
| Southbound Lake Street | 0.36 | 7.1 | A | 660 | 60 |
| Eastbound 4th Street | 0.34 | 7.0 | A | 320 | 55 |
| Eastbound Central Avenue | 0.11 | 5.1 | A | 445 | 15 |
| Westbound 4th Street | 0.01 | 4.6 | A | 325 | 0 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 6B, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements.

For both the AM and PM peak hours, the Roundabout Alternative operates better than the No Build Alternative by improving LOS from B to A and significantly reducing the 95th percentile queues.

4.3.2 Design Year (2040)

Tables 7A & 7B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile queues for Design Year conditions during AM and PM peak hour conditions, respectively.

TABLE 7A
ROUNDBOUT - DESIGN YEAR (2040) AM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.67 | 10.5 | B | -- | |
| Northbound Lake Street | 0.67 | 14.0 | B | 350 | 195 |
| Southbound Lake Street | 0.31 | 6.6 | A | 660 | 50 |
| Eastbound 4th Street | 0.42 | 8.9 | A | 320 | 75 |
| Eastbound Central Avenue | 0.20 | 8.2 | A | 445 | 35 |
| Westbound 4th Street | 0.01 | 4.5 | A | 325 | 0 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 7A, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements. The Roundabout Alternative is projected to improve the design year intersection LOS from a C to a B and reduces the projected queues.

TABLE 7B
ROUNDBOUT - DESIGN YEAR (2040) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.60 | 10.3 | B | -- | |
| Northbound Lake Street | 0.60 | 12.6 | B | 350 | 150 |
| Southbound Lake Street | 0.49 | 9.5 | A | 660 | 95 |
| Eastbound 4th Street | 0.47 | 9.5 | A | 320 | 85 |
| Eastbound Central Avenue | 0.17 | 6.4 | A | 445 | 25 |
| Westbound 4th Street | 0.02 | 5.6 | A | 325 | 0 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 7B, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements. The Roundabout Alternative is projected to improve the design year intersection LOS from a E to a B and reduces the projected queues.

5. Build Alternatives Footprint Development & Assessment

The following section summarizes the development of preliminary concept layouts of both a Traffic Signal Alternative and for a Roundabout Alternative. The layouts are useful for preliminary right-of-way needs for each alternative and also to illustrate truck-turning movements. The lane geometry for the alternatives is the same for all analysis scenarios and include terminating the northeast leg of 4th Street at the alley in advance of the intersection. Termination of this leg was discussed with and agreed to by the City.

5.1 Traffic Signal Alternative

The Traffic Signal Alternative features converting the intersection of Lake Street/4th Street/Central Avenue from a 5-way all-way stop-control to a 4-way traffic signal as shown in Figure 3. The Lake Street bridge over the Fresno River will be retained with no impacts to the structure. In order to accommodate the design vehicle turning movements, all five curb returns will need to be reconstructed. Other intersection lane geometrics improvements are illustrated in Figure 3 and are listed below:

- The northbound 4th Street approach shows the existing left-turn lane eliminated, and the existing through lane converted to a left-turn lane.
- The northbound Lake Street approach features a narrow median with a separate left-turn lane and a shared through/right-turn lane.
- The southbound 4th Street approach is terminated at the alley in advance of the intersection.
- The southbound Lake Street approach remains two lanes at the intersection.
- Central Avenue remains a single lane approach.
- The traffic signal footprint encroaches beyond the right-of-way on the northwest corner of Central Avenue and Lake Street.

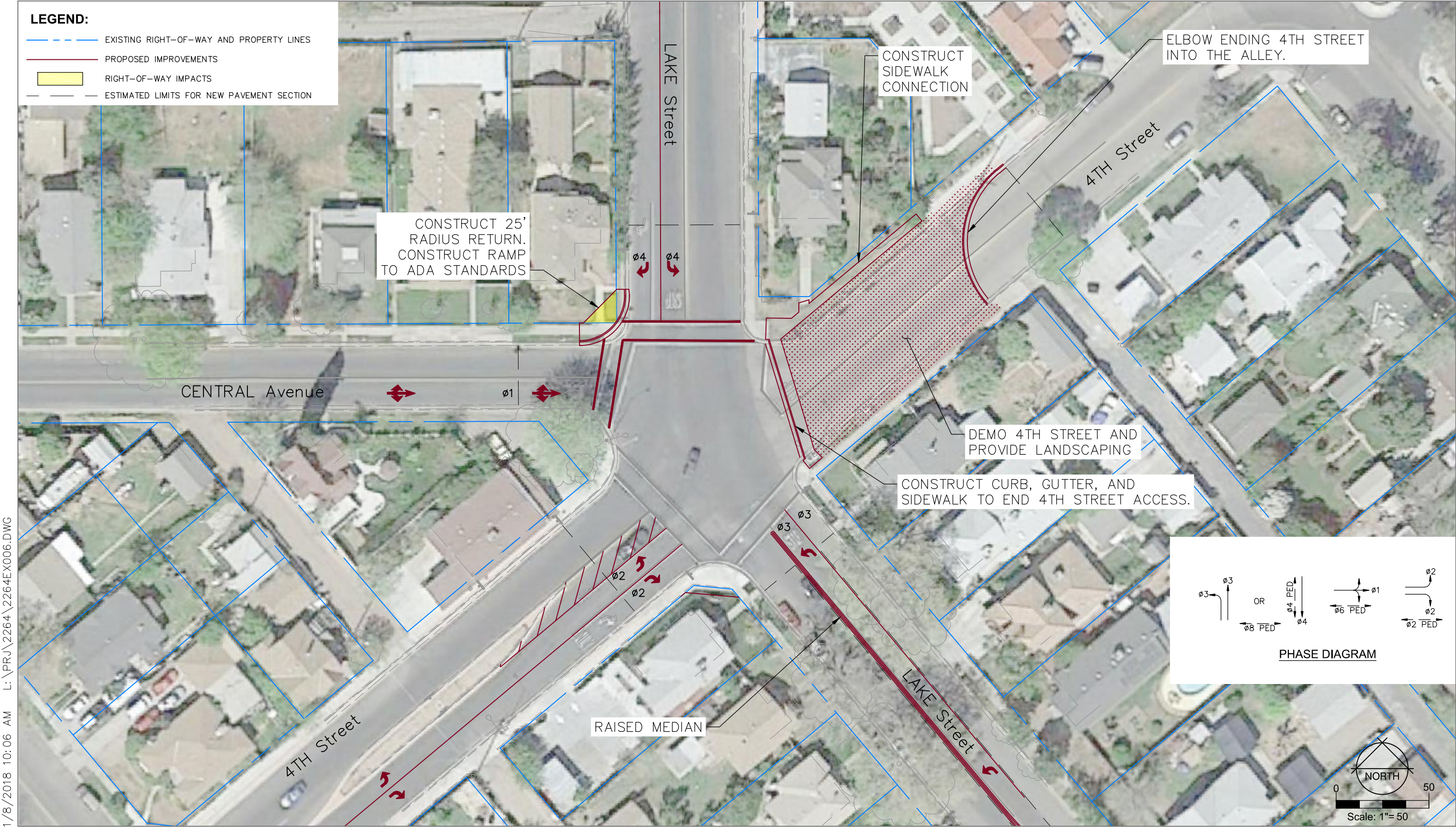
5.1.1 Traffic Signal Performance Checks

The following design criteria were used to analyze the geometrics and safety performance of the proposed Traffic Signal Alternative:

- The “WB-40” design vehicle from the American Association of State Highway and Transportation Officials (AASHTO) Geometric Design of Highways and Streets, 5th Edition (updated 2004), shall be accommodated on all movements.
- The “S-BUS-40” design vehicle from the American Association of State Highway and Transportation Officials (AASHTO) Geometric Design of Highways and Streets, 5th Edition (updated 2004), shall be accommodated on all movements.

Exhibits illustrating the truck turns for each condition are provided in Appendix B.

Traffic Signal Alternative: Preliminary Layout



LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Madera, California

Figure 3



5.2 Roundabout Alternative

The Roundabout Alternative features converting the intersection of Lake Street/4th Street/Central Avenue from a 5-way all-way stop-control to a modern 4-leg single lane roundabout as shown on Figure 4. All approaches to the intersection are shown with shared lane markings, consistent with Madera County 2011 Regional Bicycle Transportation Plan. The Lake Street bridge over the Fresno River will be retained with no impacts to the structure. The roundabout has an inscribed circle diameter of 116' with an 84' diameter central island, 16' circulatory roadway, and an 8' truck apron. The shared-use path has a width of 10' with a minimum landscaped buffer of 3'-5'. Pedestrian crossings are shown a minimum of 20'-25' from the circulatory roadway, and the pedestrian refuges at the splitter islands are at least 6' wide. Other intersection lane geometrics improvements are illustrated in Appendix C and are listed below:

- The roundabout was centered in between the existing structures located on each corner, in order to minimize right-of-way impacts.
- The northbound 4th Street approach shows a wider median, in order to provide speed control on this entry.
- In order to accommodate a right-turning truck, a truck blister was added to the northwest and southern corners of the roundabout. The truck blister is constructed out of the same material as the truck apron and allows the back tires of the truck's trailer to off-track onto it as the truck completes the right turn.
- The approach roadways are shown with splitter islands, which provide necessary deflection and speed control for entering vehicles.
- The roundabout footprint encroaches beyond the right-of-way in four of the five corners with impacts to the adjacent properties. Property impacts could be reduced by modifying the minimum width of the proposed shared-use path and landscape buffer. The National Cooperative Highway Research Program (NCHRP) Report 672 entitled "Roundabouts: An Informational Guide, 2nd edition" is the design guide used to design roundabouts. This guide recommends a shared-use path width of 10' with 8' being the minimum, and a landscape buffer of 5' with 3' being the minimum. Removing the landscape buffer can be done, but a vertical barrier would be required between the circulatory roadway and the shared-use path, in order to be ADA compliant.
- In addition to direct property impacts due to the construction footprint, there are other property impacts due to sight distance requirements. As illustrated on Figure 4, these property impacts encroach into three corners, and buildings on the west side restrict the available sight distance.

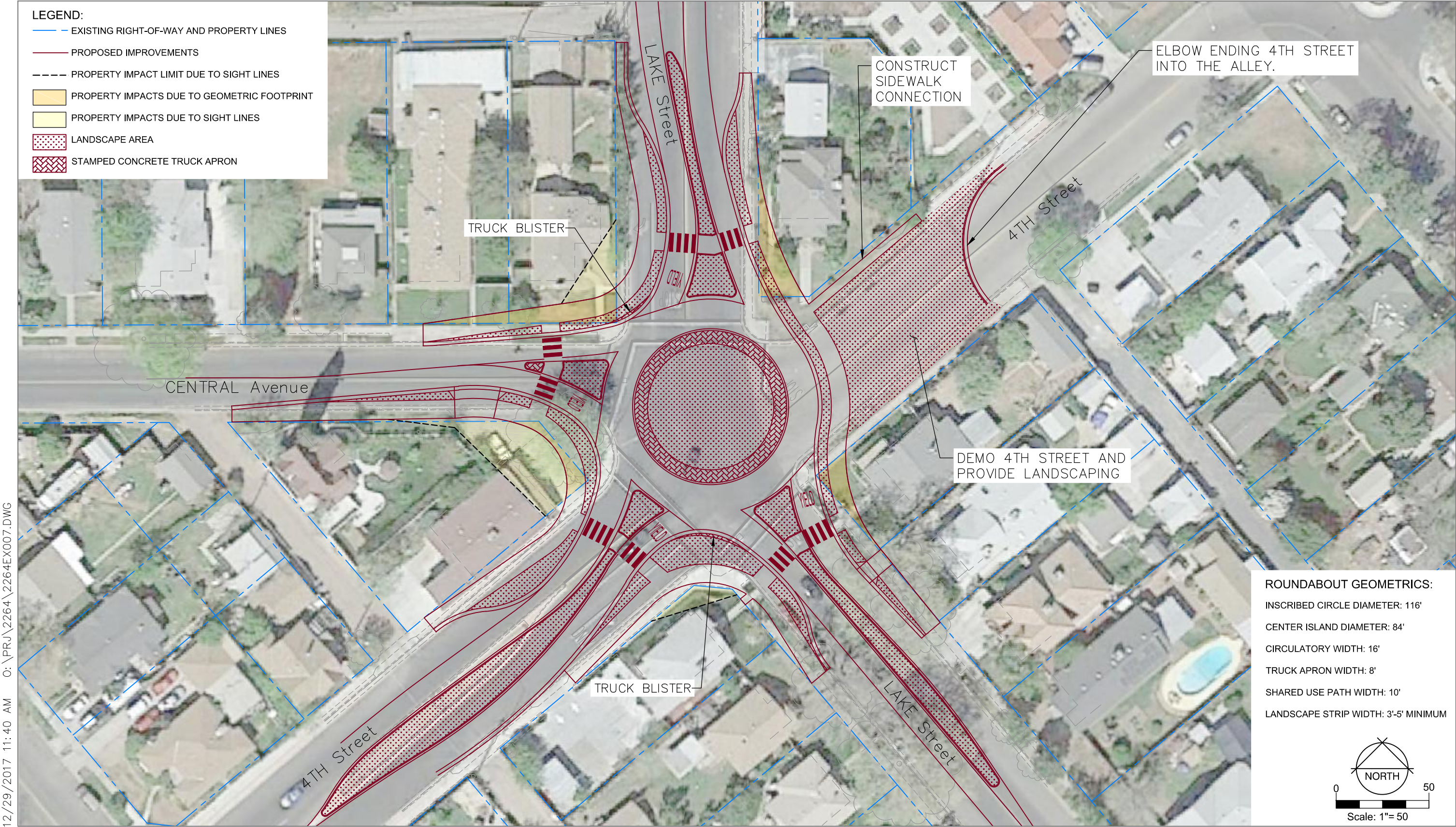
5.2.1 Roundabout Performance Checks

Due to the complexity in the design, several performance checks have been conducted to verify the Roundabout's feasibility. These performance checks meet current Caltrans TOPD 13- 02 and HDM 405.10 which mandates conformance with the National Cooperative Highway Research Program (NCHRP) Report 672 entitled "Roundabouts: An Informational Guide, 2nd edition".

The following design criteria were used to analyze the geometrics and safety performance of the proposed Roundabout Alternative:

- Criteria and methodologies to be consistent with Caltrans DIB 80-01, Caltrans Highway Design Manual, and Report 672 of the National Cooperative Highway Research Program (NCHRP) titled *Roundabouts: An Informational Guide (Second Edition)*. This document

Roundabout Alternative: Preliminary Layout



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LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Madera, California

Figure 4



supersedes the original roundabout guide published by the FHWA in 2000.

- The “WB-40” design vehicle from the American Association of State Highway and Transportation Officials (AASHTO) Geometric Design of Highways and Streets, 5th Edition (updated 2004), shall be accommodated on all movements. This vehicle shall be accommodated such that the tractor portion of the vehicle does not need to mount any truck aprons.
- The “S-BUS-40” design vehicle from the American Association of State Highway and Transportation Officials (AASHTO) Geometric Design of Highways and Streets, 5th Edition (updated 2004), shall be accommodated on all movements. This vehicle shall be accommodated such that the bus does not need to mount any truck aprons.
- Fast path entry speeds on single lane roundabout approaches should be 25 mph or less.
- Minimum stopping sight distance for posted speed limits should be provided for vehicles approaching roundabout entrances and pedestrian crosswalks.
- View angles for all legs of the roundabout should be no more than 15 degrees.
- Entry angles for all legs of the roundabout should be between 20 and 40 degrees.

Exhibits illustrating the truck turns for each condition and the fastest path analysis, stopping sight and intersection sight distance analysis, and intersection view angle exhibits are provided in Appendix C.

5.2.2 Fastest Path and Vehicle Speed Checks

The “Fastest Path” represents the path that the most aggressive drivers could take through the roundabout and assumes no other traffic to be within the intersection. NCHRP Report 672 indicates that the recommended maximum vehicle entry speeds along the fastest path should be less than 25 mph at urban single-lane roundabouts. NCHRP Report 672 also indicates that the differential speed between consecutive or conflicting projected fast path speeds should be less than 15 mph.

Fastest path speeds are determined for five locations per approach. These include entry speeds (referred to as V1); through movement circulating speeds (V2); exiting speeds (V3); left turn movement circulating speeds (V4); and right turn speeds (V5). A diagram of the described locations is shown in Figure 5.

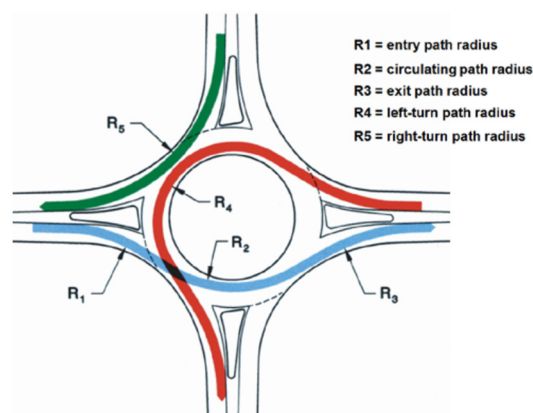


Figure 5 - Fast Path Critical Speed Locations

Fastest path speeds for the Roundabout Alternative are shown in Table 8. Exhibits illustrating the fastest path analysis can be found in Appendix C.

TABLE 8: FASTEST PATH SPEEDS (MPH)

| MOVEMENT | NB LAKE STREET (N#) | SB LAKE STREET (S#) | NEB 4TH STREET (NE#) | EB CENTRAL AVENUE (E#) |
|------------------|----------------------------|----------------------------|-----------------------------|-------------------------------|
| ENTERING (R1) | 21.9 | 22.4 | 21.8 | 20.8 |
| CIRCULATING (R2) | 22.5 | 24.4 | | 31.2 |
| EXITING (R3) | 31.4 | 21.7 | | 38.1 |
| LEFT TURN (R4) | 14.6 | | 14.8 | 14.0 |
| RIGHT TURN (R5) | | 13.4 | 15.7 | 15.4 |

Notes:

All values are in miles per hour

V3 exiting speeds are derived from vehicle acceleration formulas in NCHRP 672

V3 fast path speed measured at exit crosswalk or 100 feet downstream from V2.

N/A = Fastest path speed does not exist for this approach

2% cross-slope assumed for determining Fastest path

As shown in Table 8, the fastest path entering and right-turn speeds are less than the maximum speed of 25 mph for a single lane approach. Therefore, these fastest path speeds are acceptable for this ICE planning document. Because the Roundabout Alternative naturally slows vehicles to 25 mph or less, the vehicle traffic will be quieter than the Traffic Signal Alternative.

5.2.3 Sight Distance

Intersection sight distance differs at roundabouts versus other intersections. Drivers must be able to see potentially conflicting oncoming traffic from the left as they approach the roundabout entry. NCHRP Report 672 provides methodologies to establish the required sight distance triangles for conflicting traffic, as well as pedestrians in crosswalks, for both the entering and circulating vehicle movements. The stopping and intersection sight distance triangles were overlaid onto the proposed Roundabout Alternative to show clear vision areas for the intersection. Sight distance lengths vary according to vehicle fast path vehicle speeds. Intersection sight distances were calculated using a critical headway time t_c of 5.0 seconds, unless noted otherwise.

Table 9 presents the required intersection sight distances with the corresponding sight triangles shown in Appendix C.

TABLE 9: INTERSECTION SIGHT DISTANCE

| LEG | APPROACH | CONFLICTING SPEED (MPH) | SIGHT TRIANGLE LENGTH (FT) |
|-------------------|-------------------|--------------------------------|-----------------------------------|
| NB LAKE STREET | NEB 4TH STREET | ENTERING LEG (D1) | 21.8 |
| | EB CENTRAL AVENUE | CIRCULATING LEG (D2) | 14.0 |
| SB LAKE STREET | NB LAKE STREET | CIRCULATING LEG (D2) | 14.6 |
| NEB 4TH STREET | EB CENTRAL AVENUE | ENTERING LEG (D1) | 26.0 |
| | SB LAKE STREET | CIRCULATING LEG (D2) | 24.4 |
| EB CENTRAL AVENUE | SB LAKE STREET | ENTERING LEG (D1) | 23.4 |

Notes: Intersection Stopping Sight Distance criteria obtained from NCHRP Report 672 with 5 second Critical Headway (t_c)

*Critical Headway = 4.8 seconds.

**Critical Headway = 4.77 seconds.

Required stopping sight distances at the entries to the roundabout are provided in Table 10 and

the pedestrian crossing stopping distances are provided in Table 11.

TABLE 10: STOPPING SIGHT DISTANCE TO ENTRY

| APPROACH | INITIAL SPEED (MPH) | STOPPING SIGHT DISTANCE (FT) |
|-------------------|--------------------------------|---|
| NB LAKE STREET | 35.0 | 247.3 |
| SB LAKE STREET | 35.0 | 247.3 |
| NEB 4TH STREET | 35.0 | 247.3 |
| EB CENTRAL AVENUE | 35.0 | 247.3 |

TABLE 11: STOPPING SIGHT DISTANCE TO PEDESTRIAN CROSSING

| LEG | APPROACH | CONFLICTING SPEED (MPH) | SIGHT TRIANGLE LENGTH (FT) |
|----------------|--|--|---|
| NB LAKE STREET | NB LAKE STREET INITIAL SPEED | 35.0 | 247.3 |
| | NEB 4TH STREET RIGHT TURN (V5) | 15.7 | 81.8 |
| | EB CENTRAL AVENUE CIRCULATING SPEED (V2) | 26.0 | 161.0 |
| SB LAKE STREET | SB LAKE STREET INITIAL SPEED | 35.0 | 247.3 |
| | NB LAKE STREET CIRCULATING SPEED (V2) | 22.2 | 129.2 |
| NEB 4TH STREET | NEB 4TH STREET INITIAL SPEED | 35.0 | 247.3 |
| | EB CENTRAL AVENUE RIGHT TURN (V5) | 15.4 | 79.6 |
| | SB LAKE STREET CIRCULATING SPEED (V2) | 23.4 | 139.0 |
| EB CENTRAL | EB CENTRAL AVENUE INITIAL SPEED | 35.0 | 247.3 |
| | SB LAKE STREET RIGHT TURN (V5) | 13.4 | 66.3 |

From Tables 9, 10, and 11 and the corresponding figures in Appendix C, the proposed Roundabout Alternative provides sufficient sight distance. Special consideration to landscaping features in the sight triangles will be necessary to ensure proper sight distance at the intersections.

5.2.4 View Angles

The angle between consecutive entries must not be overly acute in order to allow drivers to comfortably turn their heads to the left to view oncoming traffic from the adjacent upstream entry. Guidance from the NCHRP section 6.7.4 recommends a minimum 75° intersection angle (15° view angle). All approaches have view angles that are less than 15°; see Appendix C for the figure showing the view angles.

6. Build Alternatives Capacity Assessment/ Analysis

Section 6 includes a capacity assessment and analysis of the 4-leg Lake Street/4th Street/Central Avenue intersection for the Traffic Signal Alternative and for the Roundabout Alternative. Each alternative is evaluated under both Existing (2017) and Design Year (2040) conditions.

6.1 Traffic Signal Alternative Analysis

This section provides a summary of the AM and PM peak hour intersection operations associated with the Traffic Signal Alternative under Existing Year (2017) and Design Year (2040) conditions. LOS worksheets for each analysis condition and lane geometrics used for this analysis are

provided in Appendix B.

6.1.1 Existing Year (2017)

Tables 12A and 12B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile queues for Existing Year conditions during AM and PM peak hour conditions, respectively.

TABLE 12A
TRAFFIC SIGNAL ALTERNATIVE - EXISTING YEAR (2017) AM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | | 23.8 | C | -- | |
| Northbound Lake Street Thru | 0.86 | 40.0 | D | 350 | 160 |
| Northbound Lake Street Left | 0.40 | | | 200 | 65 |
| Southbound Lake Street Thru | 0.59 | 17.4 | B | 400 | 190 |
| Southbound Lake Street Right | 0.39 | | | 200 | 100 |
| Eastbound 4th Street Left | 0.67 | 21.8 | C | 320 | 105 |
| Eastbound 4th Street Right | 0.08 | | | 200 | 0 |
| Eastbound Central Avenue Left/Thru/Right | 0.54 | 22.6 | C | 445 | 65 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 12A, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Traffic Signal Alternative has acceptable 95th percentile queues for all movements.

TABLE 12B
TRAFFIC SIGNAL ALTERNATIVE - EXISTING YEAR (2017) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | | 24.3 | C | -- | |
| Northbound Lake Street Thru | 0.74 | 26.7 | C | 350 | 300 |
| Northbound Lake Street Left | 0.27 | | | 200 | 90 |
| Southbound Lake Street Thru | 0.58 | 21.8 | C | 400 | 145 |
| Southbound Lake Street Right | 0.13 | | | 200 | 45 |
| Eastbound 4th Street Left | 0.66 | 23.2 | C | 320 | 185 |
| Eastbound 4th Street Right | 0.07 | | | 200 | 0 |
| Eastbound Central Avenue Left/Thru/Right | 0.57 | 28.6 | C | 445 | 85 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 12B, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Traffic Signal Alternative has acceptable 95th percentile queues for all movements.

6.1.2 Design Year (2040)

Tables 13A & 13B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile

queues for Design Year conditions during AM and PM peak hour conditions, respectively.

TABLE 13A
TRAFFIC SIGNAL ALTERNATIVE - DESIGN YEAR (2040) AM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | | 28.2 | C | -- | |
| Northbound Lake Street Thru | 0.90 | 49.7 | D | 350 | 220 |
| Northbound Lake Street Left | 0.42 | | | 200 | 85 |
| Southbound Lake Street Thru | 0.60 | 21.6 | C | 400 | 190 |
| Southbound Lake Street Right | 0.56 | | | 200 | 180 |
| Eastbound 4th Street Left | 0.57 | 20.7 | C | 320 | 160 |
| Eastbound 4th Street Right | 0.09 | | | 200 | 15 |
| Eastbound Central Avenue Left/Thru/Right | 0.63 | 30.6 | C | 445 | 95 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 13A, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Traffic Signal Alternative has acceptable 95th percentile queues for all movements. Although the intersection delay and LOS are acceptable, they are worse than those projected for the No Build Alternative. The main long term benefit of the Traffic Signal Alternative is the reduction in 95th percentile queues and delay on the southbound Lake Street approach.

TABLE 13B
TRAFFIC SIGNAL ALTERNATIVE - DESIGN YEAR (2040) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio ¹ | Delay (sec) ¹ | Level Of Service | Available Storage | 95 th Percentile Queue (ft) |
|--|------------------------|--------------------------|------------------|-------------------|--|
| Intersection | | 38.3 | D | -- | |
| Northbound Lake Street Thru | 0.86 | 39.5 | D | 350 | 375 |
| Northbound Lake Street Left | 0.31 | | | 200 | 115 |
| Southbound Lake Street Thru | 0.84 | 37.4 | D | 400 | 290 |
| Southbound Lake Street Right | 0.49 | | | 200 | 140 |
| Eastbound 4th Street Left | 0.85 | 38.5 | D | 320 | 320 |
| Eastbound 4th Street Right | 0.09 | | | 200 | 35 |
| Eastbound Central Avenue Left/Thru/Right | 0.63 | 37.6 | D | 445 | 115 |

1. Traffic Operation outputs calculated using Synchro 9 (Queues/Signalized Intersection Summary - HCM 2000)

As shown in Table 13B, the Traffic Signal Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Traffic Signal Alternative has acceptable 95th percentile queues for all movements except the northbound Lake Street through movement and vehicles queuing on this approach may occasionally back into and block the 5th Street intersection. For the design year PM peak hour, the Traffic Signal Alternative operates better than the No Build Alternative by reducing intersection delay from 43.4 seconds to 38.3 seconds and eliminates 95th percentile queuing impacts except as noted above.

6.2 Roundabout Alternative Analysis

This section provides a summary of the AM and PM peak hour intersection operations associated with the Roundabout Alternative under Existing Year (2017) and Design Year (2040) conditions. LOS worksheets for each analysis condition and lane geometrics used for this analysis are provided in Appendix C.

6.2.1 Existing Year (2017)

Tables 14A and 14B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile queues for Existing Year conditions during AM and PM peak hour conditions, respectively.

TABLE 14A
ROUNDBOUT ALTERNATIVE - EXISTING YEAR (2017) AM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.49 | 7.4 | A | -- | |
| Northbound Lake Street | 0.23 | 5.4 | A | 350 | 35 |
| Southbound Lake Street | 0.49 | 9.0 | A | 660 | 100 |
| Eastbound 4th Street | 0.30 | 6.7 | A | 320 | 50 |
| Eastbound Central Avenue | 0.13 | 5.9 | A | 445 | 20 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 14A, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements.

TABLE 14B
ROUNDBOUT ALTERNATIVE - EXISTING YEAR (2017) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.43 | 7.3 | A | -- | |
| Northbound Lake Street | 0.35 | 7.0 | A | 350 | 60 |
| Southbound Lake Street | 0.43 | 8.4 | A | 660 | 80 |
| Eastbound 4th Street | 0.33 | 6.9 | A | 320 | 55 |
| Eastbound Central Avenue | 0.11 | 5.1 | A | 445 | 15 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 14B, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements.

For both the AM and PM peak hours, the Roundabout Alternative operates better than the No Build Alternative by improving LOS from B to A and significantly reducing the 95th percentile

queues.

6.2.2 Design Year (2040)

Tables 15A & 15B show the projected volume/capacity (V/C) ratio, delay, LOS, and 95th percentile queues for Design Year conditions during AM and PM peak hour conditions, respectively.

TABLE 15A
ROUNABOUT ALTERNATIVE - DESIGN YEAR (2040) AM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.66 | 10.3 | B | -- | |
| Northbound Lake Street | 0.30 | 6.5 | A | 350 | 50 |
| Southbound Lake Street | 0.66 | 13.6 | B | 660 | 190 |
| Eastbound 4th Street | 0.41 | 8.7 | A | 320 | 75 |
| Eastbound Central Avenue | 0.20 | 8.0 | A | 445 | 35 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 15A, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the AM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements. The Roundabout Alternative is projected to improve the design year intersection LOS from a C to a B and reduces the projected queues.

TABLE 15B
ROUNABOUT ALTERNATIVE - DESIGN YEAR (2040) PM PEAK HOUR TRAFFIC OPERATIONS

| Intersection/Approach | V/C Ratio | Delay (sec) | Level of Service ¹ | Available Storage | 95 th Percentile Queue (ft) |
|--------------------------|-------------|-------------|-------------------------------|-------------------|--|
| Intersection | 0.59 | 10.1 | B | -- | |
| Northbound Lake Street | 0.48 | 9.2 | A | 350 | 90 |
| Southbound Lake Street | 0.59 | 12.3 | B | 660 | 145 |
| Eastbound 4th Street | 0.46 | 9.2 | A | 320 | 85 |
| Eastbound Central Avenue | 0.16 | 6.3 | A | 445 | 25 |

1. Lane LOS values are based on average delay and v/c ratio per lane.

As shown in Table 15B, the Roundabout Alternative is projected to provide acceptable intersection LOS and delay for the study intersection during the PM peak hour. The Roundabout Alternative has acceptable 95th percentile queues for all movements. The Roundabout Alternative is projected to improve the design year intersection LOS from a E to a B and reduces the projected queues.

7. Safety Considerations

Safety is a key evaluation factor brought forth in the Directive, and one of the goals of the ICE process is to identify projects that will ensure a reasonable level of safety and operational performance for all users.

7.1 Historic Collision Data

Historical collision data for a five-year interval (2011 through 2016) was obtained from the Statewide Integrated Traffic Records System (SWITRS). Table 16 provides the summary of the type of collisions that happened in that time period at the study intersections.

**TABLE 16
COLLISION DATA**

| Intersections | Property Damage Only | Fatal | Injury (Severe) | Injury (Other visible) | Injury (Complaint of Pain) |
|---------------------------------------|----------------------------|-------|--------------------|------------------------------|----------------------------------|
| Lake Street/4th Street/Central Avenue | 9 | 0 | 0 | 0 | 1 |

As shown in Table 12, there were no fatal or severe injury collisions at the study intersection within the five-year interval. Most collisions resulted in property damage only, but there was one reported injury collision. Of the total 10 collisions, 4 were broadside or head-on collisions.

7.2 Safety Analysis

7.2.1 Crash Modification Factors

The technical report publication titled “Desktop Reference for Crash Reduction Factor” by the Federal Highway Administration (FHWA) documents Crash Modification Factors (CMF). The publication contains CMF values for conversion of an all-way stop control to a roundabout or traffic signal or a traffic signal to a roundabout. The CMF factors for both Total Collisions and Fatal/Severe Injury Collisions are reproduced below:

Total Collisions

- CMF for converting all-way stop control to a roundabout: 72% with +/- 6% standard error
- CMF for converting all-way stop control to a traffic signal: -17%

Fatal/Severe Injury Collisions

- CMF for converting all-way stop control to a roundabout: 88% with +/- 8% standard error.
- CMF for converting all-way stop control to a traffic signal: -23% with +/- 22% standard error.

As can be seen, statistics have shown that, in general, the conversion of a stop-controlled intersection to a signal results in a negative CMF (increase in crashes) for both total number and fatal/severe injury collisions. Conversely, roundabouts have proven to result in fewer total collisions and fewer injury collisions compared to the stop-controlled and signalized intersections they replace.

7.2.2 Number of Conflicting Points

CMF factors do not account for the 5-legged intersection, which needs a detailed examination of conflict point parameters for both the Signal Alternative and Roundabout Alternatives the number of conflicting points within an intersection directly correlates to the risk of an incident, especially at intersections. Conflicting points are locations at which a roadway user can cross, merge, diverge, etc. with another roadway user. A diagram of conflict locations at typical 4-legged intersections are provided in Figure 6.

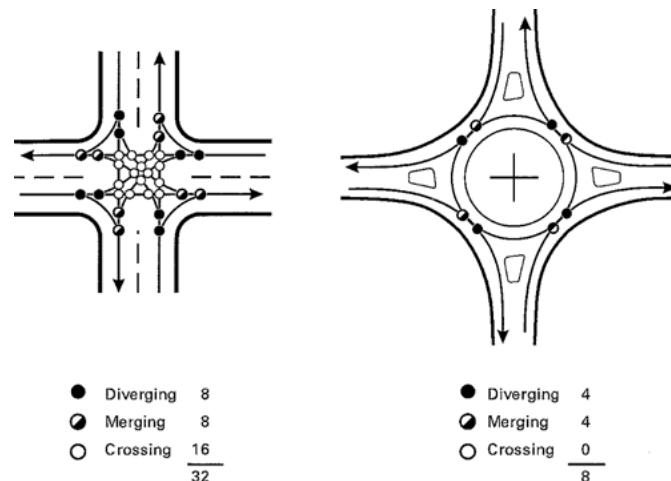


Figure 6 – Typical Conflict Points at Typical Intersections

The number of conflicting points for each of the proposed alternatives are provided below:

Traffic Signal Alternative= **32** Conflicts

Roundabout Alternative=**8** Conflicts

The analysis above illustrates the advantages that the Roundabout Alternative provides by significantly reducing the number of conflict points between vehicles and further justifies the higher CMF values as the exposure to risk is significantly reduced at roundabout intersections.

7.2.3 Reduced Speed Potential and Crash Severity Potential

Typically, the roundabout geometric design requires the driver to reduce the speed in the intersection to 15-25 MPH. Conversely, drivers can travel through a signalized intersection at speeds higher than posted speed limits due to lack of geometric constraints. Due to reduced travel speeds through the intersection and expected reduction in crashes, the Roundabout Alternative is likely to eliminate most severe crash types.

7.2.4 Pedestrian and Bike Safety

Bicycle and pedestrian safety features have been incorporated into the design of both alternatives. The Traffic Signal Alternative includes high-visibility crosswalks and a reconstructed curb ramp. According to the City's Bike Plan, all entering legs to this intersection are identified as Class 3 shared roadways. For this reason, no bike lanes were shown on either concept.

The Roundabout Alternative includes several safety enhancements for both pedestrians and

cyclists. Cyclists have two options when using a roundabout: they can exit the roadway via a bike ramp to use the shared use path with pedestrians, or they can take the lane and ride through the roundabout with the vehicles. Cyclists may feel more comfortable taking the lane due to the slower speeds that a roundabout provides; the average vehicle speed is nearly the same speed as a cyclist. The shared-use path is separated from the circulatory roadway with a landscaped buffer. This buffer screens pedestrians from the moving vehicles and also directs pedestrians to the correct crossing location. The crosswalks are split into two stages with the provision of pedestrian refuges in the splitter island. This means pedestrians only need to cross one direction of traffic at a time and they reduce the amount of sustained time a pedestrian is in potential conflict with motorized vehicles by limiting the length of each crossing.

Compared to the Roundabout Alternative, where a pedestrian only has to cross one lane of traffic at a time, with the Traffic Signal Alternative pedestrians will need to cross up to four lanes of traffic at a time.

8. Alternatives Comparison

8.1 Traffic Signal Alternative

Based on the geometric concept shown on Figure 3 and also provided in Appendix B, the Traffic Signal Alternative has the following potential impacts and considerations:

- The intersection improvements under this alternative would encroach into the adjacent property at the northwest corner of the intersection. Partial or full acquisition of this parcel would be required.
- Reconstructed curb return with ADA compliant pedestrian ramps will be provided on the northwest return.
- The northeast leg of 4th Street will be terminated at the alley and will no longer be part of the intersection. A sidewalk connection will be provided between Lake Street and the existing sidewalk on this leg of 4th Street.
- Approximately 29 on-street parking spaces will be eliminated on the approach roadways to accommodate the additional turn lanes. Eleven of these spaces are part of the northeast leg of 4th Street that will be removed.
- The intersection will be converted from all-way stop control, and a traffic signal will be installed.

8.2 Roundabout Alternative

Based on the geometric concept shown on Figure 4 and also provided in Appendix C, Roundabout Alternative has the following potential impacts and considerations:

- The intersection improvements under this alternative would encroach into the adjacent properties at the corners of the intersection. Partial or full acquisition of each parcel would be required.
- The northeast leg of 4th Street will be terminated at the alley and will no longer be part of the intersection. A sidewalk connection will be provided between Lake Street and the existing sidewalk on this leg of 4th Street.
- Shared-use paths (10') are proposed to be provided on each corner of the intersection with landscaped buffers.
- Approximately 40 on-street parking spaces will be eliminated on the approach roadways

to accommodate the proposed curb alignments. Eleven of these spaces are part of the northeast leg of 4th Street that will be removed.

9. Life-Cycle Analysis

9.1 Collision Costs

Costs associated with each crash type have been quantified using the expected crash reduction (CMF) for the intersection type as noted in the previous section and the number of accidents shown in the Collision history section. Transportation Planning Department of Caltrans provides the costs associated with accident types in Life-Cycle Benefit-Cost Analysis Economic Parameter 2016 webpage (www.dot.ca.gov/hq/tpp/offices/eab/benefit_cost/LCBCAeconomic_parameters.html). The costs are as follows:

- Fatal Accident \$10,800,000
- Injury Accident: \$148,800
- Property Damage (PDO) Accidents: \$9,700
- Average Cost per Accident: \$185,600

At the study intersection, there were a total of 10 reported collisions in the 5 year (2011- 2016) period. Out of those 10 collisions, one (1) collision was an injury collision and the remaining collisions were property damage collisions. As such, the total collision cost is calculated to be \$236,100 [(\$148,800 x 1) + (\$9,700 x 9)]. The annual collision cost is calculated to be \$47,220.

- Using the CRF reduction of 17%, the cost reduction for the Signal Alternative is approximately \$8,000/year.
- Using the CRF reduction of 56%, the cost reduction for the Roundabout Alternative is \$26,400/year.

Therefore, the Roundabout Alternative will result in lower collision costs when compared to the Signal Alternative.

9.2 Fuel Costs

To calculate the fuel cost for the alternatives, the vehicle operating costs were quantified for the project. The fuel costs (vehicle operating costs) were computed using the delay for the AM and PM peak hour periods for both the Signal and Roundabout alternatives. The output files showing the cost for all alternatives can be found in Appendix D.

The vehicle operating cost parameters were obtained from Life-Cycle Benefit-Cost Analysis Economic Parameters 2016 published by Caltrans. The cost of average fuel price was documented as \$3.18 for regular unleaded which was utilized for analysis purpose.

- The average fuel cost for the Signal Alternative is \$21,000/year.
- The average fuel cost for the Roundabout Alternative is \$20,000/year.

Therefore, it can be concluded that the Roundabout Alternative will result in slightly lower fuel costs when compared to the Traffic Signal Alternative.

9.3 Environmental Costs

To calculate the environmental cost for the alternatives, the greenhouse gas emissions costs were quantified for the project. The fuel costs (vehicle operating costs) were computed using the delay for the AM and PM peak hour periods for both the Signal and Roundabout alternatives. The output files showing the cost for the alternatives can be found in Appendix C. The vehicle operating cost parameters were obtained from Life-Cycle Benefit-Cost Analysis Economic Parameters 2016 published by Caltrans. The cost of Carbon Monoxide (CO) in California urban area was stated to be \$80/ton. The cost of Nitrogen Oxide (NOx) in California urban area was stated to be \$18,700/ton.

- The average environmental cost for the Signal Alternative is \$1,505/year.
- The total environmental cost for the Roundabout Alternative is \$1,505/year.

Therefore, it can be concluded that both alternatives will result in the same greenhouse emission costs.

9.4 Capital Costs

9.4.1 Construction Costs

Preliminary estimated construction costs have been developed for both the Traffic Signal Alternative and the Roundabout Alternative with copies of these preliminary cost estimates provided in Appendix B and C. The estimated construction costs for each alternative are provided below.

- **\$1.05 Million** for Traffic Signal Alternative
- **\$1.62 Million** for Roundabout Alternative

As shown, the construction costs, which represent an initial project capital investment, will be lower for the Traffic Signal Alternative when compared to the Roundabout Alternative.

9.4.2 Right-of-Way Costs

Preliminary ball-park costs for right-of-way were estimated and are provided in Table 17. For this study, \$10 per square foot was assumed for partial right of way takes. For the Roundabout Alternative, there are three properties identified in Table 17 as full takes. These full takes are per discussions with the City and are based on property impacts due to both roundabout geometric and sight line impacts. It was also agreed that \$250,000 per full take was a reasonable ball-park cost estimate for this study.

TABLE 17
PRELIMINARY RIGHT-OF-WAY IMPACTS AND COSTS

| Property | Traffic Signal Alternative (SQFT/COST) | Roundabout Alternative (SQFT/COST) |
|--|---|---|
| NW Corner of Lake Street and Central Avenue | 160 / \$1,600 | Full Take / \$250,000 |
| SW Corner of Central Avenue and 4 th Street | - | Full Take / \$250,000 |
| North Side Central Avenue West of Lake Street | - | 149 / \$1,490 |
| SE Corner of 4 th Street and Lake Street | - | 392 / \$3,920 |
| NE Corner of 4 th Street and Lake Street | - | Full Take / \$250,000 |
| Estimated Right-of-Way Costs | \$1,600 | \$755,410 |

As shown in Table 17, the Roundabout Alternative has a much larger impact on the adjacent properties and results in much greater right-of-way impacts and costs when compared to the Traffic Signal Alternative. These costs also represent an initial project capital investment.

9.5 Other Costs

Besides the collision, environmental and mobility cost, a significant portion of cost associated with both alternatives will be related to its operation & maintenance and pavement rehabilitation costs.

9.5.1 Operation & Maintenance Cost

The maintenance and operation cost for a traffic signal includes providing power service to the signal and street lighting (\$1,500 annually), signal retiming (\$3,000 every three years), and signal maintenance for power outages/new detector loops/etc. (\$1,500 annually) for a total annual cost of \$4,000 per year.

The roundabout alternative would incur much lower operation and maintenance costs limited to the cost to power street lighting, which is estimated at \$750 annually.

9.5.2 Landscape Maintenance Cost

It is difficult to quantify the landscape maintenance cost at this level since the cost is directly proportional to the area covered by the landscape. Roundabouts typically have a central island covered by landscaping, as well as other landscaping features not typical for a signal.

The landscape maintenance cost is projected to be \$1,500 per year for the Roundabout Alternative. The Traffic Signal Alternative is assumed to have no landscaping that will need to be maintained; therefore, a cost of \$0 per year per signal was used for landscape maintenance cost.

9.5.3 Pavement Rehabilitation

It is necessary for the function of a roadway to keep the pavement in good condition and maintain roadway striping and markings to assist motorists to navigate through an intersection/corridor safely and efficiently.

Intersections with traffic signals experience a lot of differential loading and pavement heaving

perpendicular to the direction of travel. This is caused by frequent stopping and starting of vehicles at the intersection.

Roundabout intersections experience less severe pavement heaving due to the lack of differential loading, but when heaving does occur at roundabouts, it is typically parallel to the direction of travel and occurs near the outer edge of the roadway, along the curb line. This is caused by the constant angular forces experienced in and near the circulatory roadway. As a result, roundabout intersection do not typically require structural section reconstruction just resurfacing.

Proper maintenance of the roadway profiles and cross slopes also ensure proper drainage flow and friction levels with a vehicle's tires and a roadway is typically resurfaced every 5-10 years. For the purpose of this report pavement rehabilitation is expected to occur in the study area every 8 years.

The costs associated with pavement rehabilitation include removing and reconstructing the roadway structural section, resurfacing, and pavement delineation. Traffic signal rehabilitation projects typically require more structural section reconstruction than roundabout intersections, but roundabout intersections require more labor intensive control when replacing the pavement delineation (striping and markings).

9.6 Service Life

The roundabout and traffic signal alternatives proposed for the ultimate design year are projected to provide equal levels of service for the Design Year 2040; however, the roundabout alternative is projected to operate with lower delays and shorter queues for the Ultimate Design Year than the Traffic Signal Alternative.

It can be concluded that the Roundabout Alternative will provide increased benefit with regards to service life, when compared to the Traffic Signal Alternative.

10. Summary of Findings

The traffic forecast volumes for the Lake Street/4th Street/Central Avenue intersection show growth in this area. The No Build Alternative analysis shows congestion and delay in the design year (2040) indicating that significant improvements would need to be made to the study intersection. Table 18 summarizes and compares the performance for both the Traffic Signal Alternative and the Roundabout Alternative.

**TABLE 18
ALTERNATIVE PERFORMANCE COMPARISON**

| Performance Measure | Traffic Signal Alternative | Roundabout Alternative |
|--|----------------------------|-----------------------------------|
| Cumulative Condition | | |
| Delay - All approaches LOS "D" or better LOS A rated at 5 and E rated at 1. | 2.4 ✓ | 4.8 ✓✓ |
| 95 th % Queue - Adequate queue storage | ✓ | ✓✓ |
| Future Investment Needs | | |
| Service Life – function past the design year | D ✓ | B ✓✓ |
| Costs | | |
| Operations & Maintenance - Annualized | \$3,000 | \$1,700 ✓ |
| Collision Costs - Annualized | \$150,100 | \$100,800 ✓ |
| Delay Costs - Annualized | \$36,000 | \$11,000 ✓ |
| Fuel Costs - Annualized | \$21,000 | \$20,000 ✓ |
| Environmental Costs - Annualized | \$1,505 | \$1,505 |
| Capital Costs - Annualized | \$48,000 ✓ | \$119,000 |
| Truck Accommodations | | |
| Serves design vehicle for all movements | ✓ | ✓ |
| Safety | | |
| Predictive Measures - Greatest crash reduction potential for expected fatal and injury crashes | 17% | 56% ✓ |
| Vehicle Conflicts - The number of potential conflict points that may occur at the intersection based on layout geometry | 32 | 8 ✓ |
| Pedestrian Safety - Exposure to traffic in terms of number of lanes, conflict points, crossing times, and expected vehicular speeds. | 4 35-45 mph | 1 15-25mph ✓✓ |
| Bicycle Safety - Exposure to traffic in terms of number of lanes, conflict points, and speed differential | | ✓ |
| Property Impacts | | |
| Property Impacts | ✓✓ | |
| Local Access | | |
| Maintains local access and circulation | ✓ | ✓ |
| Total Performance Measures Met | 8 | 17 |

Table 19 provides a summary of the life cycle costs for the two alternatives.

TABLE 19
LIFE CYCLE COST SUMMARY PERFORMANCE COMPARISON

| Life Cycle Costs (20 year design) | Traffic Signal Alternative | Roundabout Alternative |
|---|-----------------------------------|-------------------------------|
| Collision and Mobility Costs | | |
| Collision Costs of predicted crashes | \$3,002,000 | \$2,016,000 |
| Delay Costs | \$860,000 | \$260,000 |
| Fuel and GHG Costs | \$537,000 | \$506,000 |
| Project Costs including design, construction and maintenance | | |
| Operations and Maintenance Costs | \$60,000 | \$34,000 |
| Project Costs (including R/W) | \$1,172,299 | \$2,609,802 |
| | | |
| Total Life Cycle Costs (Opening Year \$ - Net Present Value) | \$5,631,299 | \$5,425,802 |

11. Conclusions

As shown in Table 18, 17 performance measure points were assigned to the Roundabout Alternative, as compared to 8 for the Traffic Signal Alternative. As shown in Table 19, when compared to the Traffic Signal Alternative, implementation of the Roundabout Alternative will result in lower life cycle costs. Based on these results, the Roundabout Alternative would provide superior performance at a lower overall cost than the Traffic Signal Alternative for the Lake Street/4th Street/Central Avenue intersection.

Appendix

APPENDIX A – CAPACITY ASSESSMENT/ANALYSIS EXISTING 5-LEG INTERSECTION

NO BUILD ANALYSIS

SIGNAL ANALYSIS

ROUNDBOUT ANALYSIS

APPENDIX B – TRAFFIC SIGNAL ALTERNATIVE

SIGNAL LAYOUT & TRUCK TURN EXHIBITS

SYNCHRO/SIMTRAFFIC ANALYSIS

CONSTRUCTION COST ESTIMATE

APPENDIX C – ROUNDBOUT ALTERNATIVE

ROUNDBOUT LAYOUT, FASTEST PATH, & TRUCK TURN EXHIBITS

SIDRA 7 ANALYSIS

CONSTRUCTION COST ESTIMATE

APPENDIX D – BENEFIT/COST RATIO BACK-UP

APPENDIX E – ALTERNATIVES COMPARISON BACK-UP

APPENDIX A – CAPACITY ASSESSMENT/ANALYSIS EXISTING 5-LEG INTERSECTION

NO BUILD ANALYSIS

SIGNAL ANALYSIS

ROUNDBOUT ANALYSIS

APPENDIX A – NO BUILD ANALYSIS

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 153 | 157 | 163 | 161 | 161 | 159 |
| Vehs Exited | 158 | 156 | 151 | 162 | 160 | 157 |
| Starting Vehs | 10 | 8 | 6 | 11 | 12 | 8 |
| Ending Vehs | 5 | 9 | 18 | 10 | 13 | 9 |
| Travel Distance (mi) | 27 | 27 | 27 | 28 | 28 | 28 |
| Travel Time (hr) | 1.9 | 1.7 | 1.7 | 1.7 | 1.8 | 1.8 |
| Total Delay (hr) | 0.7 | 0.5 | 0.6 | 0.5 | 0.6 | 0.6 |
| Total Stops | 155 | 157 | 163 | 160 | 161 | 159 |
| Fuel Used (gal) | 1.5 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 153 | 157 | 163 | 161 | 161 | 159 |
| Vehs Exited | 158 | 156 | 151 | 162 | 160 | 157 |
| Starting Vehs | 10 | 8 | 6 | 11 | 12 | 8 |
| Ending Vehs | 5 | 9 | 18 | 10 | 13 | 9 |
| Travel Distance (mi) | 27 | 27 | 27 | 28 | 28 | 28 |
| Travel Time (hr) | 1.9 | 1.7 | 1.7 | 1.7 | 1.8 | 1.8 |
| Total Delay (hr) | 0.7 | 0.5 | 0.6 | 0.5 | 0.6 | 0.6 |
| Total Stops | 155 | 157 | 163 | 160 | 161 | 159 |
| Fuel Used (gal) | 1.5 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | EBL | EBT | EBR | WBT | WBR2 | NBL2 | NBL | NBT | NBR | SBT | SBR | SBR2 |
|--------------------|-----|-----|-----|-----|------|------|-----|-----|-----|------|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Denied Del/Veh (s) | 3.8 | 0.1 | 3.8 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 | | 0.4 | 0.5 | 2.7 |
| Total Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 |
| Total Del/Veh (s) | 7.4 | 4.6 | 5.3 | 8.4 | 1.4 | 8.6 | 9.9 | 9.0 | | 15.9 | 12.2 | 3.0 |
| Stop Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 |
| Stop Del/Veh (s) | 5.8 | 2.7 | 5.7 | 5.1 | 1.4 | 5.5 | 7.7 | 5.1 | | 11.6 | 11.3 | 3.0 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | SEL2 | SEL | SER | All |
|--------------------|------|-----|-----|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 0.2 | | 0.1 | 1.3 |
| Total Delay (hr) | 0.0 | 0.0 | 0.0 | 0.5 |
| Total Del/Veh (s) | 11.5 | | 7.8 | 10.2 |
| Stop Delay (hr) | 0.0 | 0.0 | 0.0 | 0.4 |
| Stop Del/Veh (s) | 9.0 | | 7.3 | 8.3 |

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | EB | WB | NB | SB | SB | SE |
|-----------------------|----|-----|----|------|------|-----|----|-----|
| Directions Served | <L | T | R | LTR> | <LTR | LTR | > | <LR |
| Maximum Queue (ft) | 47 | 7 | 38 | 26 | 69 | 162 | 16 | 58 |
| Average Queue (ft) | 32 | 2 | 20 | 7 | 42 | 99 | 6 | 40 |
| 95th Queue (ft) | 50 | 10 | 42 | 25 | 76 | 189 | 20 | 70 |
| Link Distance (ft) | | 362 | | 330 | 430 | 406 | | 473 |
| Upstream Blk Time (%) | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | |
| Storage Bay Dist (ft) | 60 | | 75 | | | | 65 | |
| Storage Blk Time (%) | 0 | | 0 | | | 20 | | |
| Queuing Penalty (veh) | 0 | | 0 | | | 5 | | |

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 193 | 199 | 215 | 191 | 191 | 197 |
| Vehs Exited | 199 | 186 | 196 | 194 | 194 | 193 |
| Starting Vehs | 12 | 6 | 7 | 14 | 18 | 12 |
| Ending Vehs | 6 | 19 | 26 | 11 | 15 | 13 |
| Travel Distance (mi) | 34 | 34 | 36 | 34 | 34 | 35 |
| Travel Time (hr) | 2.3 | 2.6 | 2.6 | 2.1 | 2.4 | 2.4 |
| Total Delay (hr) | 0.9 | 1.2 | 1.2 | 0.7 | 1.0 | 1.0 |
| Total Stops | 198 | 199 | 216 | 187 | 193 | 198 |
| Fuel Used (gal) | 1.8 | 1.8 | 1.9 | 1.7 | 1.8 | 1.8 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 193 | 199 | 215 | 191 | 191 | 197 |
| Vehs Exited | 199 | 186 | 196 | 194 | 194 | 193 |
| Starting Vehs | 12 | 6 | 7 | 14 | 18 | 12 |
| Ending Vehs | 6 | 19 | 26 | 11 | 15 | 13 |
| Travel Distance (mi) | 34 | 34 | 36 | 34 | 34 | 35 |
| Travel Time (hr) | 2.3 | 2.6 | 2.6 | 2.1 | 2.4 | 2.4 |
| Total Delay (hr) | 0.9 | 1.2 | 1.2 | 0.7 | 1.0 | 1.0 |
| Total Stops | 198 | 199 | 216 | 187 | 193 | 198 |
| Fuel Used (gal) | 1.8 | 1.8 | 1.9 | 1.7 | 1.8 | 1.8 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | WBR2 | NBL2 | NBL | NBT | NBR | SBT |
|--------------------|------|-----|-----|-----|-----|-----|------|------|------|------|-----|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Denied Del/Veh (s) | 3.5 | 0.1 | 3.7 | | 0.1 | | | 0.2 | 0.3 | 0.2 | 0.1 | 0.4 |
| Total Delay (hr) | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.2 |
| Total Del/Veh (s) | 12.5 | 9.0 | 4.4 | | 5.8 | | | 17.4 | 17.6 | 18.2 | 9.5 | 20.1 |
| Stop Delay (hr) | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.2 |
| Stop Del/Veh (s) | 10.9 | 6.4 | 4.8 | | 4.0 | | | 15.2 | 15.5 | 14.1 | 9.2 | 16.1 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | SBR | SBR2 | SEL2 | SEL | SER | SER2 | All |
|--------------------|------|------|------|-----|-----|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 0.6 | 3.1 | 0.2 | | 0.1 | | 1.3 |
| Total Delay (hr) | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 |
| Total Del/Veh (s) | 15.8 | 3.8 | 13.2 | 5.6 | 9.5 | | 14.8 |
| Stop Delay (hr) | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.7 |
| Stop Del/Veh (s) | 15.4 | 3.6 | 10.8 | 4.7 | 9.0 | | 12.6 |

Total Network Performance

| Denied Delay (hr) | 0.1 |
|--------------------|------|
| Denied Del/Veh (s) | 1.3 |
| Total Delay (hr) | 0.9 |
| Total Del/Veh (s) | 16.3 |
| Stop Delay (hr) | 0.7 |
| Stop Del/Veh (s) | 13.1 |

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | EB | WB | NB | SB | SB | SE |
|-----------------------|----|-----|----|------|------|-----|----|------|
| Directions Served | <L | T | R | LTR> | <LTR | LTR | > | <LR> |
| Maximum Queue (ft) | 71 | 18 | 35 | 26 | 143 | 147 | 16 | 64 |
| Average Queue (ft) | 43 | 4 | 10 | 7 | 89 | 91 | 7 | 39 |
| 95th Queue (ft) | 77 | 22 | 33 | 32 | 169 | 177 | 18 | 75 |
| Link Distance (ft) | | 351 | | 330 | 430 | 406 | | 462 |
| Upstream Blk Time (%) | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | |
| Storage Bay Dist (ft) | 60 | | 75 | | | | 65 | |
| Storage Blk Time (%) | 5 | 0 | | | | 26 | | |
| Queuing Penalty (veh) | 5 | 0 | | | | 11 | | |

Network Summary

Network wide Queuing Penalty: 17

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 200 | 211 | 220 | 202 | 203 | 207 |
| Vehs Exited | 193 | 196 | 200 | 204 | 195 | 198 |
| Starting Vehs | 11 | 8 | 9 | 16 | 12 | 12 |
| Ending Vehs | 18 | 23 | 29 | 14 | 20 | 19 |
| Travel Distance (mi) | 34 | 36 | 36 | 35 | 35 | 35 |
| Travel Time (hr) | 3.4 | 2.9 | 3.6 | 2.4 | 2.6 | 3.0 |
| Total Delay (hr) | 1.9 | 1.5 | 2.1 | 0.9 | 1.1 | 1.5 |
| Total Stops | 196 | 212 | 219 | 198 | 205 | 205 |
| Fuel Used (gal) | 2.0 | 1.9 | 2.0 | 1.8 | 1.8 | 1.9 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 200 | 211 | 220 | 202 | 203 | 207 |
| Vehs Exited | 193 | 196 | 200 | 204 | 195 | 198 |
| Starting Vehs | 11 | 8 | 9 | 16 | 12 | 12 |
| Ending Vehs | 18 | 23 | 29 | 14 | 20 | 19 |
| Travel Distance (mi) | 34 | 36 | 36 | 35 | 35 | 35 |
| Travel Time (hr) | 3.4 | 2.9 | 3.6 | 2.4 | 2.6 | 3.0 |
| Total Delay (hr) | 1.9 | 1.5 | 2.1 | 0.9 | 1.1 | 1.5 |
| Total Stops | 196 | 212 | 219 | 198 | 205 | 205 |
| Fuel Used (gal) | 2.0 | 1.9 | 2.0 | 1.8 | 1.8 | 1.9 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | EBL | EBT | EBR | WBT | WBR2 | NBL2 | NBL | NBT | NBR | SBT | SBR | SBR2 |
|--------------------|------|-----|-----|-----|------|------|------|------|-----|------|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Denied Del/Veh (s) | 3.6 | 0.1 | 3.7 | 0.1 | | 0.3 | 0.2 | 0.2 | 0.1 | 0.7 | 0.7 | 3.1 |
| Total Delay (hr) | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.5 | 0.5 | 0.0 |
| Total Del/Veh (s) | 10.6 | 3.8 | 7.1 | 8.0 | | 15.1 | 12.6 | 13.7 | 2.0 | 42.3 | 37.5 | 5.0 |
| Stop Delay (hr) | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.4 | 0.5 | 0.0 |
| Stop Del/Veh (s) | 8.9 | 2.6 | 7.3 | 5.1 | | 12.6 | 9.9 | 9.5 | 2.1 | 40.2 | 38.5 | 4.1 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | SEL2 | SEL | SER | All |
|--------------------|------|-----|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 0.2 | 0.1 | 0.2 | 1.3 |
| Total Delay (hr) | 0.0 | 0.0 | 0.1 | 1.4 |
| Total Del/Veh (s) | 12.4 | 6.6 | 12.7 | 23.0 |
| Stop Delay (hr) | 0.0 | 0.0 | 0.1 | 1.3 |
| Stop Del/Veh (s) | 10.4 | 5.6 | 12.1 | 21.6 |

Queuing and Blocking Report
2040 AM

4/19/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | EB | WB | NB | SB | SB | SE |
|-----------------------|----|-----|----|------|------|-----|-----|-----|
| Directions Served | <L | T | R | LTR> | <LTR | LTR | > | <LR |
| Maximum Queue (ft) | 61 | 14 | 46 | 16 | 125 | 347 | 83 | 71 |
| Average Queue (ft) | 43 | 3 | 22 | 4 | 68 | 219 | 34 | 49 |
| 95th Queue (ft) | 70 | 22 | 48 | 20 | 123 | 421 | 195 | 90 |
| Link Distance (ft) | | 362 | | 330 | 430 | 406 | | 473 |
| Upstream Blk Time (%) | | | | | | 2 | | |
| Queuing Penalty (veh) | | | | | | 0 | | |
| Storage Bay Dist (ft) | 60 | | 75 | | | | 65 | |
| Storage Blk Time (%) | 3 | 0 | | | | 62 | | |
| Queuing Penalty (veh) | 3 | 0 | | | | 21 | | |

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 231 | 245 | 249 | 237 | 230 | 237 |
| Vehs Exited | 225 | 225 | 210 | 222 | 232 | 222 |
| Starting Vehs | 20 | 17 | 20 | 16 | 25 | 18 |
| Ending Vehs | 26 | 37 | 59 | 31 | 23 | 33 |
| Travel Distance (mi) | 39 | 41 | 39 | 40 | 41 | 40 |
| Travel Time (hr) | 5.4 | 4.4 | 5.3 | 4.0 | 4.9 | 4.8 |
| Total Delay (hr) | 3.8 | 2.8 | 3.7 | 2.4 | 3.3 | 3.2 |
| Total Stops | 235 | 244 | 242 | 230 | 234 | 237 |
| Fuel Used (gal) | 2.7 | 2.4 | 2.6 | 2.3 | 2.6 | 2.5 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 231 | 245 | 249 | 237 | 230 | 237 |
| Vehs Exited | 225 | 225 | 210 | 222 | 232 | 222 |
| Starting Vehs | 20 | 17 | 20 | 16 | 25 | 18 |
| Ending Vehs | 26 | 37 | 59 | 31 | 23 | 33 |
| Travel Distance (mi) | 39 | 41 | 39 | 40 | 41 | 40 |
| Travel Time (hr) | 5.4 | 4.4 | 5.3 | 4.0 | 4.9 | 4.8 |
| Total Delay (hr) | 3.8 | 2.8 | 3.7 | 2.4 | 3.3 | 3.2 |
| Total Stops | 235 | 244 | 242 | 230 | 234 | 237 |
| Fuel Used (gal) | 2.7 | 2.4 | 2.6 | 2.3 | 2.6 | 2.5 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | WBR2 | NBL2 | NBL | NBT | NBR | SBL |
|--------------------|------|------|------|-----|------|-----|------|------|------|------|------|-----|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Denied Del/Veh (s) | 3.9 | 0.5 | 3.7 | 0.1 | 0.1 | | | 0.5 | 0.4 | 0.4 | 0.1 | |
| Total Delay (hr) | 0.5 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.8 | 0.0 | 0.0 |
| Total Del/Veh (s) | 39.7 | 19.3 | 11.1 | 5.6 | 14.0 | | | 52.7 | 50.4 | 53.4 | 27.0 | |
| Stop Delay (hr) | 0.5 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.8 | 0.0 | 0.0 |
| Stop Del/Veh (s) | 38.9 | 17.0 | 10.8 | 4.7 | 10.6 | | | 52.0 | 50.2 | 51.6 | 27.3 | |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | SBT | SBR | SBR2 | SEL2 | SEL | SER | SER2 | All |
|--------------------|------|------|------|------|------|------|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 0.7 | 0.8 | 3.6 | 0.2 | 0.1 | 0.2 | | 1.6 |
| Total Delay (hr) | 0.7 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.0 |
| Total Del/Veh (s) | 59.6 | 51.6 | 6.2 | 14.7 | 15.2 | 13.5 | | 43.4 |
| Stop Delay (hr) | 0.7 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.9 |
| Stop Del/Veh (s) | 58.2 | 53.2 | 5.2 | 12.4 | 13.8 | 12.7 | | 42.5 |

Total Network Performance

| Denied Delay (hr) | 0.1 |
|--------------------|------|
| Denied Del/Veh (s) | 1.6 |
| Total Delay (hr) | 3.1 |
| Total Del/Veh (s) | 43.5 |
| Stop Delay (hr) | 3.0 |
| Stop Del/Veh (s) | 41.9 |

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | EB | WB | NB | SB | SB | SE |
|-----------------------|-----|-----|-----|------|------|-----|-----|------|
| Directions Served | <L | T | R | LTR> | <LTR | LTR | > | <LR> |
| Maximum Queue (ft) | 99 | 159 | 72 | 30 | 312 | 327 | 154 | 56 |
| Average Queue (ft) | 82 | 76 | 33 | 9 | 217 | 235 | 49 | 43 |
| 95th Queue (ft) | 127 | 262 | 135 | 32 | 380 | 417 | 242 | 69 |
| Link Distance (ft) | | 351 | | 330 | 430 | 406 | | 462 |
| Upstream Blk Time (%) | | 2 | | | 1 | 2 | | |
| Queuing Penalty (veh) | | 0 | | | 0 | 0 | | |
| Storage Bay Dist (ft) | 60 | | 75 | | | | 65 | |
| Storage Blk Time (%) | 44 | 1 | | | | 78 | | |
| Queuing Penalty (veh) | 55 | 3 | | | | 42 | | |

Network Summary

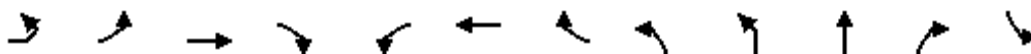
Network wide Queuing Penalty: 99

APPENDIX A – TRAFFIC SIGNAL ANALYSIS

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017

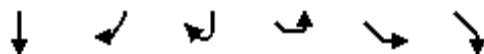


| Movement | EBL2 | EBL | EBT | EBR | WBL | WBT | WBR2 | NBL2 | NBL | NBT | NBR | SBL |
|-----------------------------------|------|------|-------|------|---------------------------|------|------|------|------|------|------|------|
| Lane Configurations | | RT | LT | | RT | LT | | | RT | LT | | RT |
| Traffic Volume (vph) | 1 | 145 | 2 | 94 | 2 | 3 | 1 | 37 | 25 | 140 | 2 | 1 |
| Future Volume (vph) | 1 | 145 | 2 | 94 | 2 | 3 | 1 | 37 | 25 | 140 | 2 | 1 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 13 | 13 | 12 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | 4.5 | 4.5 | | 4.5 |
| Lane Util. Factor | | 0.97 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 0.99 | 1.00 | | | 1.00 | 1.00 | | 0.99 |
| Frt | | 1.00 | 0.85 | | 1.00 | 0.97 | | | 1.00 | 1.00 | | 1.00 |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.95 | 1.00 | | 0.95 |
| Satd. Flow (prot) | | 3156 | 1444 | | 1622 | 1896 | | | 1699 | 1785 | | 1621 |
| Flt Permitted | | 0.75 | 1.00 | | 0.68 | 1.00 | | | 0.95 | 1.00 | | 0.95 |
| Satd. Flow (perm) | | 2506 | 1444 | | 1163 | 1896 | | | 1699 | 1785 | | 1621 |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 1 | 179 | 2 | 116 | 2 | 4 | 1 | 46 | 31 | 173 | 2 | 1 |
| RTOR Reduction (vph) | 0 | 0 | 95 | 0 | 0 | 4 | 0 | 0 | 0 | 1 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 180 | 23 | 0 | 2 | 1 | 0 | 0 | 77 | 174 | 0 | 1 |
| Confl. Peds. (#/hr) | 6 | | | | 9 | | | 3 | | | | 1 |
| Confl. Bikes (#/hr) | | | | 1 | | | 5 | | | | 2 | |
| Turn Type | Perm | Perm | NA | | Perm | NA | | Prot | Prot | NA | | Prot |
| Protected Phases | | | 2 | | | 6 | | 3 | 3 | 8 | | 7 |
| Permitted Phases | 2 | 2 | | | 6 | | | | | | | |
| Actuated Green, G (s) | | 11.8 | 11.8 | | 11.8 | 11.8 | | | 6.8 | 25.5 | | 0.7 |
| Effective Green, g (s) | | 11.8 | 11.8 | | 11.8 | 11.8 | | | 6.8 | 25.5 | | 0.7 |
| Actuated g/C Ratio | | 0.18 | 0.18 | | 0.18 | 0.18 | | | 0.11 | 0.40 | | 0.01 |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | 4.5 | 4.5 | | 4.5 |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | | 462 | 266 | | 214 | 349 | | | 180 | 711 | | 17 |
| v/s Ratio Prot | | | 0.02 | | | 0.00 | | | 0.05 | 0.10 | | 0.00 |
| v/s Ratio Perm | | 0.07 | | | 0.00 | | | | | | | |
| v/c Ratio | | 0.39 | 0.09 | | 0.01 | 0.00 | | | 0.43 | 0.25 | | 0.06 |
| Uniform Delay, d1 | | 22.9 | 21.6 | | 21.3 | 21.3 | | | 26.8 | 12.8 | | 31.3 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 |
| Incremental Delay, d2 | | 0.5 | 0.1 | | 0.0 | 0.0 | | | 1.6 | 0.2 | | 1.5 |
| Delay (s) | | 23.5 | 21.8 | | 21.3 | 21.3 | | | 28.4 | 13.0 | | 32.8 |
| Level of Service | | C | C | | C | C | | | C | B | | C |
| Approach Delay (s) | | | 22.8 | | | 21.3 | | | | 17.7 | | |
| Approach LOS | | | C | | | C | | | | B | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 20.4 | | HCM 2000 Level of Service | | | | C | | | |
| HCM 2000 Volume to Capacity ratio | | | 0.46 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 64.0 | | Sum of lost time (s) | | | | 18.0 | | | |
| Intersection Capacity Utilization | | | 45.3% | | ICU Level of Service | | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017



| Movement | SBT | SBR | SBR2 | SEL2 | SEL | SER |
|------------------------|------|-------|------|------|-------|------|
| Lane Configurations | ↑ | ↘ | | | ↙ | ↘ |
| Traffic Volume (vph) | 178 | 216 | 27 | 14 | 2 | 65 |
| Future Volume (vph) | 178 | 216 | 27 | 14 | 2 | 65 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | 4.5 | 4.5 | | | 4.5 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 0.98 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.85 | | | 0.89 | |
| Flt Protected | 1.00 | 1.00 | | | 0.99 | |
| Satd. Flow (prot) | 1731 | 1440 | | | 1527 | |
| Flt Permitted | 1.00 | 1.00 | | | 0.99 | |
| Satd. Flow (perm) | 1731 | 1440 | | | 1527 | |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 220 | 267 | 33 | 17 | 2 | 80 |
| RTOR Reduction (vph) | 0 | 88 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 220 | 212 | 0 | 0 | 99 | 0 |
| Confl. Peds. (#/hr) | | | | 8 | | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Turn Type | NA | Perm | | Prot | Prot | |
| Protected Phases | 4 | | | 9 | 9 | |
| Permitted Phases | | 4 | | | | |
| Actuated Green, G (s) | 19.4 | 19.4 | | | 8.0 | |
| Effective Green, g (s) | 19.4 | 19.4 | | | 8.0 | |
| Actuated g/C Ratio | 0.30 | 0.30 | | | 0.12 | |
| Clearance Time (s) | 4.5 | 4.5 | | | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 524 | 436 | | | 190 | |
| v/s Ratio Prot | 0.13 | | | | c0.06 | |
| v/s Ratio Perm | | c0.15 | | | | |
| v/c Ratio | 0.42 | 0.49 | | | 0.52 | |
| Uniform Delay, d1 | 17.8 | 18.2 | | | 26.2 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.5 | 0.9 | | | 2.6 | |
| Delay (s) | 18.4 | 19.1 | | | 28.8 | |
| Level of Service | B | B | | | C | |
| Approach Delay (s) | 18.8 | | | | 28.8 | |
| Approach LOS | B | | | | C | |

Intersection Summary

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 178 | 169 | 150 | 150 | 150 | 158 |
| Vehs Exited | 167 | 175 | 153 | 153 | 148 | 159 |
| Starting Vehs | 6 | 18 | 14 | 12 | 5 | 11 |
| Ending Vehs | 17 | 12 | 11 | 9 | 7 | 10 |
| Travel Distance (mi) | 30 | 31 | 27 | 26 | 26 | 28 |
| Travel Time (hr) | 2.1 | 2.1 | 1.9 | 1.7 | 1.8 | 1.9 |
| Total Delay (hr) | 1.0 | 1.0 | 0.9 | 0.8 | 0.8 | 0.9 |
| Total Stops | 123 | 124 | 111 | 106 | 115 | 115 |
| Fuel Used (gal) | 1.8 | 1.8 | 1.5 | 1.5 | 1.5 | 1.6 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 178 | 169 | 150 | 150 | 150 | 158 |
| Vehs Exited | 167 | 175 | 153 | 153 | 148 | 159 |
| Starting Vehs | 6 | 18 | 14 | 12 | 5 | 11 |
| Ending Vehs | 17 | 12 | 11 | 9 | 7 | 10 |
| Travel Distance (mi) | 30 | 31 | 27 | 26 | 26 | 28 |
| Travel Time (hr) | 2.1 | 2.1 | 1.9 | 1.7 | 1.8 | 1.9 |
| Total Delay (hr) | 1.0 | 1.0 | 0.9 | 0.8 | 0.8 | 0.9 |
| Total Stops | 123 | 124 | 111 | 106 | 115 | 115 |
| Fuel Used (gal) | 1.8 | 1.8 | 1.5 | 1.5 | 1.5 | 1.6 |

2: N Lake St & E 4th St & Central Ave Performance by approach

| Approach | EB | WB | NB | SB | SE | All |
|--------------------|------|-----|------|------|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 0.2 | 0.1 | 1.5 | 2.5 | 0.2 | 1.5 |
| Total Delay (hr) | 0.2 | 0.0 | 0.2 | 0.3 | 0.1 | 0.8 |
| Total Del/Veh (s) | 13.8 | 6.9 | 21.2 | 16.0 | 22.6 | 16.9 |
| Stop Delay (hr) | 0.2 | 0.0 | 0.2 | 0.3 | 0.1 | 0.6 |
| Stop Del/Veh (s) | 12.1 | 5.4 | 17.2 | 12.7 | 21.0 | 14.0 |

Queuing and Blocking Report
Signal 2017 AM

4/20/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | WB | NB | NB | SB | SB | SB | SE |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | L | TR | TR> | <L | TR | L | T | R> | <LR |
| Maximum Queue (ft) | 87 | 23 | 13 | 47 | 100 | 1 | 76 | 92 | 74 |
| Average Queue (ft) | 52 | 9 | 3 | 29 | 62 | 0 | 40 | 44 | 42 |
| 95th Queue (ft) | 105 | 28 | 15 | 52 | 105 | 2 | 86 | 106 | 82 |
| Link Distance (ft) | 352 | 352 | 307 | | 436 | | 387 | | 452 |
| Upstream Blk Time (%) | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | |
| Storage Bay Dist (ft) | | | | 200 | | 100 | | 200 | |
| Storage Blk Time (%) | | | | | | | 0 | | |
| Queuing Penalty (veh) | | | | | | | 1 | | |

Actuated Signals, Observed Splits
Signal 2017 AM

4/20/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Phase | 2 | 3 | 4 | 6 | 7 | 8 | 9 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Movement(s) Served | EBTL | NBL | SBT | WBTL | SBL | NBT | SEL |
| Maximum Green (s) | 31.4 | 18.5 | 41.5 | 31.4 | 5.0 | 55.0 | 20.6 |
| Minimum Green (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Recall | None | None | None | None | None | None | None |
| Avg. Green (s) | 12.0 | 6.9 | 14.7 | 12.0 | 0.0 | 20.6 | 10.5 |
| g/C Ratio | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 | -0.01 |
| Cycles Skipped (%) | 15 | 42 | 8 | 15 | 100 | 42 | 42 |
| Cycles @ Minimum (%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cycles Maxed Out (%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cycles with Peds (%) | 8 | 0 | 0 | 0 | 0 | 0 | 8 |

Controller Summary

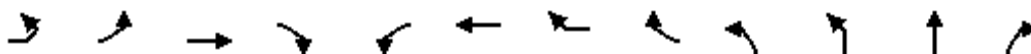
Average Cycle Length (s): NA

Number of Complete Cycles : 0

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017



| Movement | EBL2 | EBL | EBT | EBR | WBL | WBT | WBR | WBR2 | NBL2 | NBL | NBT | NBR |
|-----------------------------------|------|-------|-------|------|------|---------------------------|------|------|------|-------|-------|------|
| Lane Configurations | | EBL | EBT | | WBL | WBT | | | NBL2 | NBL | NBT | NBR |
| Traffic Volume (vph) | 1 | 221 | 4 | 96 | 3 | 2 | 1 | 1 | 48 | 43 | 262 | 5 |
| Future Volume (vph) | 1 | 221 | 4 | 96 | 3 | 2 | 1 | 1 | 48 | 43 | 262 | 5 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 12 | 13 | 13 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.97 | 1.00 | | 1.00 | 1.00 | | | | 1.00 | 1.00 | |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 0.99 | | | | 1.00 | 1.00 | |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 0.99 | 1.00 | | | | 1.00 | 1.00 | |
| Frt | | 1.00 | 0.86 | | 1.00 | 0.93 | | | | 1.00 | 1.00 | |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | | | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3250 | 1493 | | 1670 | 1852 | | | | 1750 | 1836 | |
| Flt Permitted | | 0.76 | 1.00 | | 0.69 | 1.00 | | | | 0.95 | 1.00 | |
| Satd. Flow (perm) | | 2583 | 1493 | | 1215 | 1852 | | | | 1750 | 1836 | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 1 | 226 | 4 | 98 | 3 | 2 | 1 | 1 | 49 | 44 | 267 | 5 |
| RTOR Reduction (vph) | 0 | 0 | 78 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 0 | 227 | 24 | 0 | 3 | 3 | 0 | 0 | 0 | 93 | 271 | 0 |
| Confl. Peds. (#/hr) | 6 | | | | 9 | | | | 3 | | | |
| Confl. Bikes (#/hr) | | | | 1 | | | | 5 | | | | 2 |
| Turn Type | Perm | Perm | NA | | Perm | NA | | | Prot | Prot | NA | |
| Protected Phases | | | 2 | | | 6 | | | 3 | 3 | 8 | |
| Permitted Phases | 2 | 2 | | | 6 | | | | | | | |
| Actuated Green, G (s) | | 12.8 | 12.8 | | 12.8 | 12.8 | | | | 7.3 | 24.4 | |
| Effective Green, g (s) | | 12.8 | 12.8 | | 12.8 | 12.8 | | | | 7.3 | 24.4 | |
| Actuated g/C Ratio | | 0.20 | 0.20 | | 0.20 | 0.20 | | | | 0.11 | 0.38 | |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | | | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 519 | 300 | | 244 | 372 | | | | 200 | 704 | |
| v/s Ratio Prot | | | 0.02 | | | 0.00 | | | | c0.05 | c0.15 | |
| v/s Ratio Perm | | c0.09 | | | 0.00 | | | | | | | |
| v/c Ratio | | 0.44 | 0.08 | | 0.01 | 0.01 | | | | 0.47 | 0.39 | |
| Uniform Delay, d1 | | 22.2 | 20.6 | | 20.3 | 20.3 | | | | 26.3 | 14.2 | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | | | | 1.00 | 1.00 | |
| Incremental Delay, d2 | | 0.6 | 0.1 | | 0.0 | 0.0 | | | | 1.7 | 0.4 | |
| Delay (s) | | 22.8 | 20.7 | | 20.4 | 20.3 | | | | 28.0 | 14.5 | |
| Level of Service | | C | C | | C | C | | | | C | B | |
| Approach Delay (s) | | | 22.2 | | | 20.3 | | | | | 18.0 | |
| Approach LOS | | | C | | | C | | | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 20.2 | | | HCM 2000 Level of Service | | | | C | | |
| HCM 2000 Volume to Capacity ratio | | | 0.45 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 63.6 | | | Sum of lost time (s) | | | 18.0 | | | |
| Intersection Capacity Utilization | | | 53.3% | | | ICU Level of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017



| Movement | SBL | SBT | SBR | SBR2 | SEL2 | SEL | SER | SER2 |
|------------------------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | |
| Traffic Volume (vph) | 2 | 213 | 150 | 42 | 32 | 2 | 58 | 2 |
| Future Volume (vph) | 2 | 213 | 150 | 42 | 32 | 2 | 58 | 2 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | 4.5 | 4.5 | 4.5 | | | 4.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | | 1.00 | | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | | | 0.99 | | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | | | 1.00 | | |
| Frt | 1.00 | 1.00 | 0.85 | | | 0.91 | | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | | 0.98 | | |
| Satd. Flow (prot) | 1672 | 1782 | 1483 | | | 1586 | | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | | 0.98 | | |
| Satd. Flow (perm) | 1672 | 1782 | 1483 | | | 1586 | | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 2 | 217 | 153 | 43 | 33 | 2 | 59 | 2 |
| RTOR Reduction (vph) | 0 | 0 | 91 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 2 | 217 | 105 | 0 | 0 | 96 | 0 | 0 |
| Confl. Peds. (#/hr) | 1 | | | | 8 | | | |
| Confl. Bikes (#/hr) | | | | 1 | | | | 1 |
| Turn Type | Prot | NA | Perm | | Prot | Prot | | |
| Protected Phases | 7 | 4 | | | 9 | 9 | | |
| Permitted Phases | | | 4 | | | | | |
| Actuated Green, G (s) | 0.7 | 17.8 | 17.8 | | | 7.7 | | |
| Effective Green, g (s) | 0.7 | 17.8 | 17.8 | | | 7.7 | | |
| Actuated g/C Ratio | 0.01 | 0.28 | 0.28 | | | 0.12 | | |
| Clearance Time (s) | 4.5 | 4.5 | 4.5 | | | 4.5 | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 18 | 498 | 415 | | | 192 | | |
| v/s Ratio Prot | 0.00 | 0.12 | | | | c0.06 | | |
| v/s Ratio Perm | | | 0.07 | | | | | |
| v/c Ratio | 0.11 | 0.44 | 0.25 | | | 0.50 | | |
| Uniform Delay, d1 | 31.1 | 18.8 | 17.8 | | | 26.1 | | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 2.7 | 0.6 | 0.3 | | | 2.0 | | |
| Delay (s) | 33.9 | 19.4 | 18.1 | | | 28.2 | | |
| Level of Service | C | B | B | | | C | | |
| Approach Delay (s) | | 18.8 | | | | 28.2 | | |
| Approach LOS | | B | | | | C | | |
| Intersection Summary | | | | | | | | |

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 212 | 211 | 200 | 217 | 199 | 205 |
| Vehs Exited | 207 | 206 | 190 | 207 | 199 | 202 |
| Starting Vehs | 19 | 13 | 11 | 17 | 8 | 12 |
| Ending Vehs | 24 | 18 | 21 | 27 | 8 | 20 |
| Travel Distance (mi) | 37 | 37 | 34 | 37 | 35 | 36 |
| Travel Time (hr) | 2.7 | 3.0 | 2.6 | 2.9 | 2.4 | 2.7 |
| Total Delay (hr) | 1.3 | 1.6 | 1.3 | 1.5 | 1.2 | 1.4 |
| Total Stops | 148 | 163 | 153 | 165 | 140 | 154 |
| Fuel Used (gal) | 2.2 | 2.2 | 2.0 | 2.2 | 2.0 | 2.1 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 212 | 211 | 200 | 217 | 199 | 205 |
| Vehs Exited | 207 | 206 | 190 | 207 | 199 | 202 |
| Starting Vehs | 19 | 13 | 11 | 17 | 8 | 12 |
| Ending Vehs | 24 | 18 | 21 | 27 | 8 | 20 |
| Travel Distance (mi) | 37 | 37 | 34 | 37 | 35 | 36 |
| Travel Time (hr) | 2.7 | 3.0 | 2.6 | 2.9 | 2.4 | 2.7 |
| Total Delay (hr) | 1.3 | 1.6 | 1.3 | 1.5 | 1.2 | 1.4 |
| Total Stops | 148 | 163 | 153 | 165 | 140 | 154 |
| Fuel Used (gal) | 2.2 | 2.2 | 2.0 | 2.2 | 2.0 | 2.1 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | WBR2 | NBL2 | NBL | NBT | NBR | SBL |
|--------------------|------|------|-----|-----|-----|-----|------|------|------|------|------|-----|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Denied Del/Veh (s) | 0.2 | 0.5 | 0.2 | | | | | 3.4 | 3.6 | 0.6 | 0.8 | |
| Total Delay (hr) | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.3 | 0.0 | 0.0 |
| Total Del/Veh (s) | 25.1 | 19.9 | 5.0 | | | | | 25.0 | 25.6 | 21.6 | 10.4 | |
| Stop Delay (hr) | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.2 | 0.0 | 0.0 |
| Stop Del/Veh (s) | 21.6 | 13.7 | 5.1 | | | | | 22.2 | 22.6 | 16.3 | 8.5 | |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | SBT | SBR | SBR2 | SEL2 | SER | SER2 | All |
|--------------------|------|------|------|------|------|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 1.0 | 3.5 | 3.4 | 0.2 | 0.2 | | 1.2 |
| Total Delay (hr) | 0.2 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 1.2 |
| Total Del/Veh (s) | 20.4 | 18.0 | 11.8 | 24.8 | 26.2 | | 20.8 |
| Stop Delay (hr) | 0.2 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 1.0 |
| Stop Del/Veh (s) | 15.3 | 15.7 | 10.9 | 22.1 | 24.9 | | 17.3 |

Queuing and Blocking Report
Signal 2017 PM

4/20/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB | SE |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| Directions Served | <L | L | TR | L | TR> | <L | TR | L | T | R> | <LR> |
| Maximum Queue (ft) | 22 | 123 | 32 | 3 | 16 | 63 | 200 | 1 | 110 | 78 | 91 |
| Average Queue (ft) | 6 | 79 | 9 | 1 | 4 | 42 | 116 | 0 | 54 | 41 | 53 |
| 95th Queue (ft) | 38 | 137 | 38 | 5 | 16 | 72 | 218 | 2 | 121 | 88 | 98 |
| Link Distance (ft) | | 341 | 341 | | 307 | | 436 | | 387 | | 438 |
| Upstream Blk Time (%) | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | |
| Storage Bay Dist (ft) | 150 | | | 100 | | 200 | | 100 | | 200 | |
| Storage Blk Time (%) | | 0 | | | | | 3 | | 2 | | |
| Queuing Penalty (veh) | | 0 | | | | | 2 | | 4 | | |

Intersection: 2: N Lake St & E 4th St & Central Ave

| Phase | 2 | 3 | 4 | 6 | 7 | 8 | 9 |
|----------------------|------|-------|------|------|-------|-------|-------|
| Movement(s) Served | EBTL | NBL | SBT | WBTL | SBL | NBT | SEL |
| Maximum Green (s) | 31.4 | 18.5 | 41.5 | 31.4 | 5.0 | 55.0 | 20.6 |
| Minimum Green (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Recall | None | None | None | None | None | None | None |
| Avg. Green (s) | 18.0 | 8.7 | 16.6 | 18.0 | 0.0 | 31.4 | 10.0 |
| g/C Ratio | NA | -0.01 | NA | NA | -0.01 | -0.01 | -0.01 |
| Cycles Skipped (%) | 0 | 13 | 0 | 0 | 100 | 25 | 11 |
| Cycles @ Minimum (%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cycles Maxed Out (%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cycles with Peds (%) | 13 | 0 | 11 | 13 | 0 | 0 | 0 |

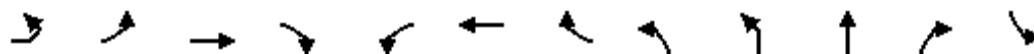
Controller Summary

Average Cycle Length (s): NA
Number of Complete Cycles : 0

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017



| Movement | EBL2 | EBL | EBT | EBR | WBL | WBT | WBR2 | NBL2 | NBL | NBT | NBR | SBL |
|------------------------|------|-------|------|------|------|------|------|------|-------|------|------|------|
| Lane Configurations | | EBL | EBT | | WBL | WBT | | NBL2 | NBL | NBT | NBR | SBL |
| Traffic Volume (vph) | 1 | 182 | 3 | 118 | 3 | 4 | 1 | 47 | 31 | 176 | 3 | 1 |
| Future Volume (vph) | 1 | 182 | 3 | 118 | 3 | 4 | 1 | 47 | 31 | 176 | 3 | 1 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 13 | 13 | 12 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | 4.5 | 4.5 | | 4.5 |
| Lane Util. Factor | | 0.97 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 0.98 | 1.00 | | | 1.00 | 1.00 | | 0.98 |
| Frt | | 1.00 | 0.85 | | 1.00 | 0.97 | | | 1.00 | 1.00 | | 1.00 |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | | | 0.95 | 1.00 | | 0.95 |
| Satd. Flow (prot) | | 3148 | 1446 | | 1619 | 1907 | | | 1699 | 1783 | | 1617 |
| Flt Permitted | | 0.75 | 1.00 | | 0.59 | 1.00 | | | 0.95 | 1.00 | | 0.95 |
| Satd. Flow (perm) | | 2498 | 1446 | | 1012 | 1907 | | | 1699 | 1783 | | 1617 |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 1 | 225 | 4 | 146 | 4 | 5 | 1 | 58 | 38 | 217 | 4 | 1 |
| RTOR Reduction (vph) | 0 | 0 | 120 | 0 | 0 | 5 | 0 | 0 | 0 | 1 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 226 | 30 | 0 | 4 | 1 | 0 | 0 | 96 | 220 | 0 | 1 |
| Confl. Peds. (#/hr) | 6 | | | | 9 | | | 3 | | | | 1 |
| Confl. Bikes (#/hr) | | | | 1 | | | 5 | | | | 2 | |
| Turn Type | Perm | Perm | NA | | Perm | NA | | Prot | Prot | NA | | Prot |
| Protected Phases | | | 2 | | | 6 | | 3 | 3 | 8 | | 7 |
| Permitted Phases | 2 | 2 | | | 6 | | | | | | | |
| Actuated Green, G (s) | | 14.2 | 14.2 | | 14.2 | 14.2 | | | 8.5 | 33.6 | | 0.7 |
| Effective Green, g (s) | | 14.2 | 14.2 | | 14.2 | 14.2 | | | 8.5 | 33.6 | | 0.7 |
| Actuated g/C Ratio | | 0.18 | 0.18 | | 0.18 | 0.18 | | | 0.11 | 0.42 | | 0.01 |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | 4.5 | 4.5 | | 4.5 |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | | 445 | 257 | | 180 | 339 | | | 181 | 751 | | 14 |
| v/s Ratio Prot | | | 0.02 | | | 0.00 | | | c0.06 | 0.12 | | 0.00 |
| v/s Ratio Perm | | c0.09 | | | 0.00 | | | | | | | |
| v/c Ratio | | 0.51 | 0.12 | | 0.02 | 0.00 | | | 0.53 | 0.29 | | 0.07 |
| Uniform Delay, d1 | | 29.6 | 27.5 | | 27.0 | 26.9 | | | 33.7 | 15.2 | | 39.2 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 | | 1.00 |
| Incremental Delay, d2 | | 0.9 | 0.2 | | 0.0 | 0.0 | | | 3.0 | 0.2 | | 2.2 |
| Delay (s) | | 30.5 | 27.7 | | 27.1 | 26.9 | | | 36.7 | 15.4 | | 41.3 |
| Level of Service | | C | C | | C | C | | | D | B | | D |
| Approach Delay (s) | | | 29.4 | | | 27.0 | | | | 21.9 | | |
| Approach LOS | | | C | | | C | | | | C | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 25.7 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.56 | | |
| Actuated Cycle Length (s) | 79.7 | Sum of lost time (s) | 18.0 |
| Intersection Capacity Utilization | 50.7% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017



| Movement | SBT | SBR | SBR2 | SEL2 | SEL | SER |
|------------------------|------|-------|------|------|-------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 224 | 272 | 34 | 18 | 3 | 82 |
| Future Volume (vph) | 224 | 272 | 34 | 18 | 3 | 82 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | 4.5 | 4.5 | | | 4.5 | |
| Lane Util. Factor | 1.00 | 1.00 | | | 1.00 | |
| Frpb, ped/bikes | 1.00 | 0.98 | | | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | | 1.00 | |
| Frt | 1.00 | 0.85 | | | 0.89 | |
| Flt Protected | 1.00 | 1.00 | | | 0.99 | |
| Satd. Flow (prot) | 1731 | 1440 | | | 1529 | |
| Flt Permitted | 1.00 | 1.00 | | | 0.99 | |
| Satd. Flow (perm) | 1731 | 1440 | | | 1529 | |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 277 | 336 | 42 | 22 | 4 | 101 |
| RTOR Reduction (vph) | 0 | 85 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 277 | 293 | 0 | 0 | 127 | 0 |
| Confl. Peds. (#/hr) | | | | 8 | | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Turn Type | NA | Perm | | Prot | Prot | |
| Protected Phases | 4 | | | 9 | 9 | |
| Permitted Phases | | 4 | | | | |
| Actuated Green, G (s) | 25.8 | 25.8 | | | 13.2 | |
| Effective Green, g (s) | 25.8 | 25.8 | | | 13.2 | |
| Actuated g/C Ratio | 0.32 | 0.32 | | | 0.17 | |
| Clearance Time (s) | 4.5 | 4.5 | | | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 560 | 466 | | | 253 | |
| v/s Ratio Prot | 0.16 | | | | c0.08 | |
| v/s Ratio Perm | | c0.20 | | | | |
| v/c Ratio | 0.49 | 0.63 | | | 0.50 | |
| Uniform Delay, d1 | 21.7 | 22.9 | | | 30.3 | |
| Progression Factor | 1.00 | 1.00 | | | 1.00 | |
| Incremental Delay, d2 | 0.7 | 2.6 | | | 1.6 | |
| Delay (s) | 22.4 | 25.5 | | | 31.8 | |
| Level of Service | C | C | | | C | |
| Approach Delay (s) | 24.2 | | | | 31.8 | |
| Approach LOS | C | | | | C | |
| Intersection Summary | | | | | | |

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 210 | 205 | 199 | 199 | 178 | 199 |
| Vehs Exited | 209 | 209 | 204 | 209 | 180 | 202 |
| Starting Vehs | 19 | 19 | 19 | 17 | 16 | 18 |
| Ending Vehs | 20 | 15 | 14 | 7 | 14 | 13 |
| Travel Distance (mi) | 37 | 37 | 35 | 36 | 31 | 35 |
| Travel Time (hr) | 2.6 | 2.9 | 2.5 | 2.4 | 2.2 | 2.5 |
| Total Delay (hr) | 1.3 | 1.5 | 1.2 | 1.1 | 1.1 | 1.2 |
| Total Stops | 136 | 147 | 143 | 143 | 137 | 140 |
| Fuel Used (gal) | 2.1 | 2.2 | 2.0 | 2.1 | 1.8 | 2.0 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 210 | 205 | 199 | 199 | 178 | 199 |
| Vehs Exited | 209 | 209 | 204 | 209 | 180 | 202 |
| Starting Vehs | 19 | 19 | 19 | 17 | 16 | 18 |
| Ending Vehs | 20 | 15 | 14 | 7 | 14 | 13 |
| Travel Distance (mi) | 37 | 37 | 35 | 36 | 31 | 35 |
| Travel Time (hr) | 2.6 | 2.9 | 2.5 | 2.4 | 2.2 | 2.5 |
| Total Delay (hr) | 1.3 | 1.5 | 1.2 | 1.1 | 1.1 | 1.2 |
| Total Stops | 136 | 147 | 143 | 143 | 137 | 140 |
| Fuel Used (gal) | 2.1 | 2.2 | 2.0 | 2.1 | 1.8 | 2.0 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR2 | NBL2 | NBL | NBT | NBR | SBT | SBR |
|--------------------|------|-----|-----|-----|------|------|------|------|------|-----|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Denied Del/Veh (s) | 0.2 | | 0.3 | | 0.1 | | 3.8 | 3.5 | 0.4 | 0.3 | 1.2 | 3.3 |
| Total Delay (hr) | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 0.2 | 0.3 |
| Total Del/Veh (s) | 21.8 | | 4.6 | | 14.0 | | 29.3 | 27.6 | 15.1 | 2.6 | 18.5 | 19.2 |
| Stop Delay (hr) | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 0.2 | 0.2 |
| Stop Del/Veh (s) | 18.3 | | 4.4 | | 11.4 | | 26.3 | 25.1 | 11.3 | 1.3 | 13.7 | 16.1 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | SBR2 | SEL2 | SEL | SER | All |
|--------------------|------|------|-----|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 3.5 | 0.3 | | 0.2 | 1.4 |
| Total Delay (hr) | 0.0 | 0.0 | 0.0 | 0.1 | 1.1 |
| Total Del/Veh (s) | 11.7 | 32.0 | | 25.3 | 18.4 |
| Stop Delay (hr) | 0.0 | 0.0 | 0.0 | 0.1 | 0.9 |
| Stop Del/Veh (s) | 10.4 | 28.5 | | 23.9 | 15.2 |

Queuing and Blocking Report
Signal 2040 AM

4/20/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SE |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Directions Served | <L | L | TR | L | TR> | <L | TR | T | R> | <LR |
| Maximum Queue (ft) | 6 | 89 | 59 | 3 | 14 | 72 | 121 | 113 | 138 | 87 |
| Average Queue (ft) | 1 | 58 | 17 | 1 | 3 | 44 | 74 | 69 | 83 | 53 |
| 95th Queue (ft) | 8 | 106 | 63 | 5 | 16 | 76 | 132 | 135 | 174 | 96 |
| Link Distance (ft) | | 352 | 352 | | 307 | | 436 | 387 | | 452 |
| Upstream Blk Time (%) | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | |
| Storage Bay Dist (ft) | 150 | | | 100 | | 200 | | | 200 | |
| Storage Blk Time (%) | | | | | | | | 2 | 1 | |
| Queuing Penalty (veh) | | | | | | | | 7 | 2 | |

Actuated Signals, Observed Splits
Signal 2040 AM

4/20/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Phase | 2 | 3 | 4 | 6 | 7 | 8 | 9 |
|----------------------|------|-------|------|------|-------|-------|-------|
| Movement(s) Served | EBTL | NBL | SBT | WBTL | SBL | NBT | SEL |
| Maximum Green (s) | 31.4 | 18.5 | 41.5 | 31.4 | 5.0 | 55.0 | 20.6 |
| Minimum Green (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Recall | None | None | None | None | None | None | None |
| Avg. Green (s) | 15.8 | 8.7 | 18.4 | 15.8 | 0.0 | 27.7 | 12.6 |
| g/C Ratio | NA | -0.01 | NA | NA | -0.01 | -0.01 | -0.01 |
| Cycles Skipped (%) | 0 | 33 | 0 | 0 | 100 | 22 | 25 |
| Cycles @ Minimum (%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cycles Maxed Out (%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cycles with Peds (%) | 11 | 0 | 0 | 11 | 0 | 0 | 13 |

Controller Summary

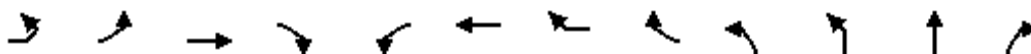
Average Cycle Length (s): NA

Number of Complete Cycles : 0

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017



| Movement | EBL2 | EBL | EBT | EBR | WBL | WBT | WBR | WBR2 | NBL2 | NBL | NBT | NBR |
|------------------------|------|-------|------|------|------|------|------|------|------|-------|------|------|
| Lane Configurations | | EBL | EBT | | WBL | WBT | | | NBL2 | NBL | NBT | NBR |
| Traffic Volume (vph) | 1 | 278 | 5 | 121 | 4 | 3 | 1 | 1 | 60 | 54 | 329 | 6 |
| Future Volume (vph) | 1 | 278 | 5 | 121 | 4 | 3 | 1 | 1 | 60 | 54 | 329 | 6 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 16 | 12 | 12 | 12 | 13 | 13 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | | 4.5 | 4.5 | |
| Lane Util. Factor | | 0.97 | 1.00 | | 1.00 | 1.00 | | | | 1.00 | 1.00 | |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 0.99 | | | | 1.00 | 1.00 | |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 0.98 | 1.00 | | | | 1.00 | 1.00 | |
| Frt | | 1.00 | 0.86 | | 1.00 | 0.94 | | | | 1.00 | 1.00 | |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | | | | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 3240 | 1493 | | 1665 | 1885 | | | | 1750 | 1837 | |
| Flt Permitted | | 0.75 | 1.00 | | 0.63 | 1.00 | | | | 0.95 | 1.00 | |
| Satd. Flow (perm) | | 2573 | 1493 | | 1109 | 1885 | | | | 1750 | 1837 | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 1 | 299 | 5 | 130 | 4 | 3 | 1 | 1 | 65 | 58 | 354 | 6 |
| RTOR Reduction (vph) | 0 | 0 | 105 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 0 | 300 | 30 | 0 | 4 | 4 | 0 | 0 | 0 | 123 | 359 | 0 |
| Confl. Peds. (#/hr) | 6 | | | | 9 | | | | 3 | | | |
| Confl. Bikes (#/hr) | | | | 1 | | | | 5 | | | | 2 |
| Turn Type | Perm | Perm | NA | | Perm | NA | | | Prot | Prot | NA | |
| Protected Phases | | | 2 | | | 6 | | | 3 | 3 | 8 | |
| Permitted Phases | 2 | 2 | | | 6 | | | | | | | |
| Actuated Green, G (s) | | 16.0 | 16.0 | | 16.0 | 16.0 | | | | 11.8 | 35.3 | |
| Effective Green, g (s) | | 16.0 | 16.0 | | 16.0 | 16.0 | | | | 11.8 | 35.3 | |
| Actuated g/C Ratio | | 0.19 | 0.19 | | 0.19 | 0.19 | | | | 0.14 | 0.43 | |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | | | | 4.5 | 4.5 | |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | | | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | | 497 | 288 | | 214 | 364 | | | | 249 | 784 | |
| v/s Ratio Prot | | | 0.02 | | | 0.00 | | | | c0.07 | 0.20 | |
| v/s Ratio Perm | | c0.12 | | | 0.00 | | | | | | | |
| v/c Ratio | | 0.60 | 0.10 | | 0.02 | 0.01 | | | | 0.49 | 0.46 | |
| Uniform Delay, d1 | | 30.5 | 27.5 | | 27.0 | 27.0 | | | | 32.7 | 16.9 | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | | | | 1.00 | 1.00 | |
| Incremental Delay, d2 | | 2.1 | 0.2 | | 0.0 | 0.0 | | | | 1.5 | 0.4 | |
| Delay (s) | | 32.5 | 27.6 | | 27.0 | 27.0 | | | | 34.2 | 17.3 | |
| Level of Service | | C | C | | C | C | | | | C | B | |
| Approach Delay (s) | | | 31.0 | | | 27.0 | | | | | 21.6 | |
| Approach LOS | | | C | | | C | | | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 26.4 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.55 | | |
| Actuated Cycle Length (s) | 82.7 | Sum of lost time (s) | 18.0 |
| Intersection Capacity Utilization | 60.3% | ICU Level of Service | B |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4/19/2017



| Movement | SBL | SBT | SBR | SBR2 | SEL2 | SEL | SER | SER2 |
|------------------------|------|-------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | |
| Traffic Volume (vph) | 3 | 268 | 189 | 53 | 40 | 3 | 73 | 3 |
| Future Volume (vph) | 3 | 268 | 189 | 53 | 40 | 3 | 73 | 3 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | 4.5 | 4.5 | 4.5 | | | 4.5 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | | | 1.00 | | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | | | 0.99 | | |
| Flpb, ped/bikes | 0.99 | 1.00 | 1.00 | | | 1.00 | | |
| Frt | 1.00 | 1.00 | 0.85 | | | 0.91 | | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | | 0.98 | | |
| Satd. Flow (prot) | 1669 | 1782 | 1483 | | | 1586 | | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | | 0.98 | | |
| Satd. Flow (perm) | 1669 | 1782 | 1483 | | | 1586 | | |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 3 | 288 | 203 | 57 | 43 | 3 | 78 | 3 |
| RTOR Reduction (vph) | 0 | 0 | 89 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 3 | 288 | 171 | 0 | 0 | 127 | 0 | 0 |
| Confl. Peds. (#/hr) | 1 | | | | 8 | | | |
| Confl. Bikes (#/hr) | | | | 1 | | | | 1 |
| Turn Type | Prot | NA | Perm | | Prot | Prot | | |
| Protected Phases | 7 | 4 | | | 9 | 9 | | |
| Permitted Phases | | | 4 | | | | | |
| Actuated Green, G (s) | 0.7 | 24.2 | 24.2 | | | 12.7 | | |
| Effective Green, g (s) | 0.7 | 24.2 | 24.2 | | | 12.7 | | |
| Actuated g/C Ratio | 0.01 | 0.29 | 0.29 | | | 0.15 | | |
| Clearance Time (s) | 4.5 | 4.5 | 4.5 | | | 4.5 | | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | | 3.0 | | |
| Lane Grp Cap (vph) | 14 | 521 | 433 | | | 243 | | |
| v/s Ratio Prot | 0.00 | c0.16 | | | | c0.08 | | |
| v/s Ratio Perm | | | 0.12 | | | | | |
| v/c Ratio | 0.21 | 0.55 | 0.39 | | | 0.52 | | |
| Uniform Delay, d1 | 40.7 | 24.7 | 23.4 | | | 32.2 | | |
| Progression Factor | 1.00 | 1.00 | 1.00 | | | 1.00 | | |
| Incremental Delay, d2 | 7.6 | 1.3 | 0.6 | | | 2.0 | | |
| Delay (s) | 48.3 | 26.0 | 24.0 | | | 34.2 | | |
| Level of Service | D | C | C | | | C | | |
| Approach Delay (s) | | 25.1 | | | | 34.2 | | |
| Approach LOS | | C | | | | C | | |
| Intersection Summary | | | | | | | | |

Summary of All Intervals

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|-------------------------|------|------|------|------|------|------|
| Start Time | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 | 6:57 |
| End Time | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 | 7:10 |
| Total Time (min) | 13 | 13 | 13 | 13 | 13 | 13 |
| Time Recorded (min) | 10 | 10 | 10 | 10 | 10 | 10 |
| # of Intervals | 2 | 2 | 2 | 2 | 2 | 2 |
| # of Recorded Intervals | 1 | 1 | 1 | 1 | 1 | 1 |
| Vehs Entered | 270 | 255 | 256 | 243 | 259 | 256 |
| Vehs Exited | 261 | 247 | 250 | 235 | 276 | 254 |
| Starting Vehs | 15 | 22 | 18 | 14 | 28 | 19 |
| Ending Vehs | 24 | 30 | 24 | 22 | 11 | 21 |
| Travel Distance (mi) | 47 | 44 | 44 | 42 | 47 | 45 |
| Travel Time (hr) | 3.9 | 3.3 | 3.3 | 3.1 | 4.3 | 3.6 |
| Total Delay (hr) | 2.2 | 1.7 | 1.7 | 1.6 | 2.5 | 1.9 |
| Total Stops | 202 | 180 | 181 | 168 | 194 | 183 |
| Fuel Used (gal) | 2.8 | 2.5 | 2.6 | 2.4 | 3.0 | 2.7 |

Interval #0 Information Seeding

| | |
|-------------------------------------|------|
| Start Time | 6:57 |
| End Time | 7:00 |
| Total Time (min) | 3 |
| Volumes adjusted by Growth Factors. | |
| No data recorded this interval. | |

Interval #1 Information Recording

| | |
|-------------------------------------|------|
| Start Time | 7:00 |
| End Time | 7:10 |
| Total Time (min) | 10 |
| Volumes adjusted by Growth Factors. | |

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
|----------------------|-----|-----|-----|-----|-----|-----|
| Vehs Entered | 270 | 255 | 256 | 243 | 259 | 256 |
| Vehs Exited | 261 | 247 | 250 | 235 | 276 | 254 |
| Starting Vehs | 15 | 22 | 18 | 14 | 28 | 19 |
| Ending Vehs | 24 | 30 | 24 | 22 | 11 | 21 |
| Travel Distance (mi) | 47 | 44 | 44 | 42 | 47 | 45 |
| Travel Time (hr) | 3.9 | 3.3 | 3.3 | 3.1 | 4.3 | 3.6 |
| Total Delay (hr) | 2.2 | 1.7 | 1.7 | 1.6 | 2.5 | 1.9 |
| Total Stops | 202 | 180 | 181 | 168 | 194 | 183 |
| Fuel Used (gal) | 2.8 | 2.5 | 2.6 | 2.4 | 3.0 | 2.7 |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | WBR2 | NBL2 | NBL | NBT | NBR | SBL |
|--------------------|------|------|-----|-----|-----|-----|------|------|------|------|------|-----|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Denied Del/Veh (s) | 0.3 | 0.1 | 0.2 | 2.5 | | | | 3.6 | 3.0 | 0.7 | 0.5 | |
| Total Delay (hr) | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.3 | 0.0 | 0.0 |
| Total Del/Veh (s) | 35.2 | 22.9 | 6.7 | 5.7 | | | | 34.6 | 34.2 | 17.4 | 25.3 | |
| Stop Delay (hr) | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.2 | 0.0 | 0.0 |
| Stop Del/Veh (s) | 30.8 | 20.3 | 6.5 | 4.9 | | | | 31.4 | 30.9 | 13.0 | 23.5 | |

2: N Lake St & E 4th St & Central Ave Performance by movement

| Movement | SBT | SBR | SBR2 | SEL2 | SEL | SER | SER2 | All |
|--------------------|------|------|------|------|------|------|------|------|
| Denied Delay (hr) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Denied Del/Veh (s) | 1.1 | 3.4 | 3.4 | 0.1 | 0.2 | 0.2 | | 1.2 |
| Total Delay (hr) | 0.3 | 0.2 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 1.8 |
| Total Del/Veh (s) | 20.0 | 21.2 | 14.0 | 33.0 | 59.8 | 30.6 | | 23.4 |
| Stop Delay (hr) | 0.2 | 0.2 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 1.5 |
| Stop Del/Veh (s) | 14.9 | 18.6 | 12.4 | 29.1 | 56.4 | 28.5 | | 19.7 |

Queuing and Blocking Report
Signal 2040 PM

4/20/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB | SE |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| Directions Served | <L | L | TR | L | TR> | <L | TR | L | T | R> | <LR> |
| Maximum Queue (ft) | 118 | 173 | 27 | 5 | 9 | 102 | 188 | 2 | 129 | 130 | 124 |
| Average Queue (ft) | 42 | 117 | 10 | 1 | 2 | 67 | 124 | 0 | 78 | 64 | 77 |
| 95th Queue (ft) | 149 | 198 | 32 | 6 | 11 | 122 | 235 | 3 | 136 | 142 | 136 |
| Link Distance (ft) | | 341 | 341 | | 307 | | 436 | | 387 | | 438 |
| Upstream Blk Time (%) | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | |
| Storage Bay Dist (ft) | 150 | | | 100 | | 200 | | 100 | | 200 | |
| Storage Blk Time (%) | 0 | 4 | | | | | 3 | | 4 | | |
| Queuing Penalty (veh) | 0 | 6 | | | | | 4 | | 9 | | |

Actuated Signals, Observed Splits
Signal 2040 PM

4/20/2017

Intersection: 2: N Lake St & E 4th St & Central Ave

| Phase | 2 | 3 | 4 | 6 | 7 | 8 | 9 |
|----------------------|------|-------|------|------|-------|------|------|
| Movement(s) Served | EBTL | NBL | SBT | WBTL | SBL | NBT | SEL |
| Maximum Green (s) | 31.4 | 18.5 | 41.5 | 31.4 | 5.0 | 55.0 | 20.6 |
| Minimum Green (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Recall | None | None | None | None | None | None | None |
| Avg. Green (s) | 20.9 | 10.8 | 25.8 | 20.9 | 0.0 | 39.6 | 13.3 |
| g/C Ratio | NA | -0.01 | NA | NA | -0.01 | NA | NA |
| Cycles Skipped (%) | 0 | 17 | 0 | 0 | 100 | 0 | 0 |
| Cycles @ Minimum (%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cycles Maxed Out (%) | 14 | 0 | 0 | 14 | 0 | 0 | 0 |
| Cycles with Peds (%) | 0 | 0 | 14 | 14 | 0 | 0 | 0 |

Controller Summary

Average Cycle Length (s): NA
Number of Complete Cycles : 0

APPENDIX A – ROUNDABOUT ANALYSIS

LANE SUMMARY

 **Site: 1 [2017 AM Peak Hour]**

4th Street/Lake Street/Central Avenue
2017 AM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|--------------------------|------------------|---------------|---------------------|--------------------|-------------------------|---------------------|--------------------|---------------------|----------------|----------------------|-------------------|----------------------|
| | Demand Total veh/h | Flows HV % | Cap. veh/h | Deg. Satn v/c | Lane Util. % | Average Delay sec | Level of Service | 95% Back of Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. Adj. % | Prob. Block. % |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 252 | 4.0 | 1092 | 0.231 | 100 | 5.4 | LOS A | 1.4 | 36.1 | Full | 360 | 0.0 | 0.0 |
| Approach | 252 | 4.0 | | 0.231 | | 5.4 | LOS A | 1.4 | 36.1 | | | | |
| NorthEast: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 9 | 4.0 | 907 | 0.010 | 100 | 4.1 | LOS A | 0.0 | 1.3 | Full | 325 | 0.0 | 0.0 |
| Approach | 9 | 4.0 | | 0.010 | | 4.1 | LOS A | 0.0 | 1.3 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 521 | 4.0 | 1056 | 0.493 | 100 | 9.1 | LOS A | 3.9 | 99.6 | Full | 730 | 0.0 | 0.0 |
| Approach | 521 | 4.0 | | 0.493 | | 9.1 | LOS A | 3.9 | 99.6 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 101 | 4.0 | 770 | 0.131 | 100 | 6.0 | LOS A | 0.8 | 20.9 | Full | 450 | 0.0 | 0.0 |
| Approach | 101 | 4.0 | | 0.131 | | 6.0 | LOS A | 0.8 | 20.9 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 299 | 4.0 | 987 | 0.303 | 100 | 6.7 | LOS A | 1.9 | 49.1 | Full | 320 | 0.0 | 0.0 |
| Approach | 299 | 4.0 | | 0.303 | | 6.7 | LOS A | 1.9 | 49.1 | | | | |
| Intersection | 1181 | 4.0 | | 0.493 | | 7.4 | LOS A | 3.9 | 99.6 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 **Site: 1 [2017 PM Peak Hour]**

4th Street/Lake Street/Central Avenue
2017 PM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|--------------------------|------------------|---------------|---------------------|--------------------|-------------------------|---------------------|--------------------|---------------------|----------------|----------------------|-------------------|----------------------|
| | Demand Total veh/h | Flows HV % | Cap. veh/h | Deg. Satn v/c | Lane Util. % | Average Delay sec | Level of Service | 95% Back of Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. Adj. % | Prob. Block. % |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 385 | 1.0 | 1063 | 0.362 | 100 | 7.1 | LOS A | 2.5 | 61.8 | Full | 360 | 0.0 | 0.0 |
| Approach | 385 | 1.0 | | 0.362 | | 7.1 | LOS A | 2.5 | 61.8 | | | | |
| NorthEast: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 8 | 1.0 | 792 | 0.010 | 100 | 4.6 | LOS A | 0.1 | 1.3 | Full | 325 | 0.0 | 0.0 |
| Approach | 8 | 1.0 | | 0.010 | | 4.6 | LOS A | 0.1 | 1.3 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 438 | 1.0 | 1003 | 0.436 | 100 | 8.5 | LOS A | 3.2 | 80.4 | Full | 730 | 0.0 | 0.0 |
| Approach | 438 | 1.0 | | 0.436 | | 8.5 | LOS A | 3.2 | 80.4 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 101 | 1.0 | 891 | 0.113 | 100 | 5.1 | LOS A | 0.7 | 17.3 | Full | 450 | 0.0 | 0.0 |
| Approach | 101 | 1.0 | | 0.113 | | 5.1 | LOS A | 0.7 | 17.3 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 346 | 1.0 | 1022 | 0.339 | 100 | 7.0 | LOS A | 2.2 | 55.9 | Full | 320 | 0.0 | 0.0 |
| Approach | 346 | 1.0 | | 0.339 | | 7.0 | LOS A | 2.2 | 55.9 | | | | |
| Intersection | 1277 | 1.0 | | 0.436 | | 7.4 | LOS A | 3.2 | 80.4 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 **Site: 1 [2040 AM Peak Hour]**

4th Street/Lake Street/Central Avenue
2040 AM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|--------------------------|------------------|---------------|---------------------|--------------------|-------------------------|---------------------|--------------------|---------------------|----------------|----------------------|-------------------|----------------------|
| | Demand Total veh/h | Flows HV % | Cap. veh/h | Deg. Satn v/c | Lane Util. % | Average Delay sec | Level of Service | 95% Back of Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. Adj. % | Prob. Block. % |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 317 | 4.0 | 1032 | 0.307 | 100 | 6.6 | LOS A | 2.0 | 52.0 | Full | 360 | 0.0 | 0.0 |
| Approach | 317 | 4.0 | | 0.307 | | 6.6 | LOS A | 2.0 | 52.0 | | | | |
| NorthEast: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 11 | 4.0 | 816 | 0.014 | 100 | 4.5 | LOS A | 0.1 | 1.9 | Full | 325 | 0.0 | 0.0 |
| Approach | 11 | 4.0 | | 0.014 | | 4.5 | LOS A | 0.1 | 1.9 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 656 | 4.0 | 984 | 0.666 | 100 | 14.0 | LOS B | 7.5 | 194.1 | Full | 730 | 0.0 | 0.0 |
| Approach | 656 | 4.0 | | 0.666 | | 14.0 | LOS B | 7.5 | 194.1 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 128 | 4.0 | 629 | 0.204 | 100 | 8.2 | LOS A | 1.4 | 35.7 | Full | 450 | 0.0 | 0.0 |
| Approach | 128 | 4.0 | | 0.204 | | 8.2 | LOS A | 1.4 | 35.7 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 375 | 4.0 | 902 | 0.416 | 100 | 8.9 | LOS A | 2.9 | 74.8 | Full | 320 | 0.0 | 0.0 |
| Approach | 375 | 4.0 | | 0.416 | | 8.9 | LOS A | 2.9 | 74.8 | | | | |
| Intersection | 1488 | 4.0 | | 0.666 | | 10.5 | LOS B | 7.5 | 194.1 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 **Site: 1 [2040 PM Peak Hour]**

4th Street/Lake Street/Central Avenue
2040 PM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|--------------------------|------------------|---------------|---------------------|--------------------|-------------------------|---------------------|--------------------|---------------------|----------------|----------------------|-------------------|----------------------|
| | Demand Total veh/h | Flows HV % | Cap. veh/h | Deg. Satn v/c | Lane Util. % | Average Delay sec | Level of Service | 95% Back of Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. Adj. % | Prob. Block. % |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 483 | 1.0 | 988 | 0.489 | 100 | 9.5 | LOS A | 3.7 | 93.8 | Full | 360 | 0.0 | 0.0 |
| Approach | 483 | 1.0 | | 0.489 | | 9.5 | LOS A | 3.7 | 93.8 | | | | |
| NorthEast: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 10 | 1.0 | 656 | 0.015 | 100 | 5.6 | LOS A | 0.1 | 2.2 | Full | 325 | 0.0 | 0.0 |
| Approach | 10 | 1.0 | | 0.015 | | 5.6 | LOS A | 0.1 | 2.2 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 552 | 1.0 | 918 | 0.601 | 100 | 12.6 | LOS B | 6.0 | 150.0 | Full | 730 | 0.0 | 0.0 |
| Approach | 552 | 1.0 | | 0.601 | | 12.6 | LOS B | 6.0 | 150.0 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 128 | 1.0 | 773 | 0.166 | 100 | 6.4 | LOS A | 1.1 | 27.2 | Full | 450 | 0.0 | 0.0 |
| Approach | 128 | 1.0 | | 0.166 | | 6.4 | LOS A | 1.1 | 27.2 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 435 | 1.0 | 937 | 0.465 | 100 | 9.5 | LOS A | 3.4 | 86.0 | Full | 320 | 0.0 | 0.0 |
| Approach | 435 | 1.0 | | 0.465 | | 9.5 | LOS A | 3.4 | 86.0 | | | | |
| Intersection | 1608 | 1.0 | | 0.601 | | 10.3 | LOS B | 6.0 | 150.0 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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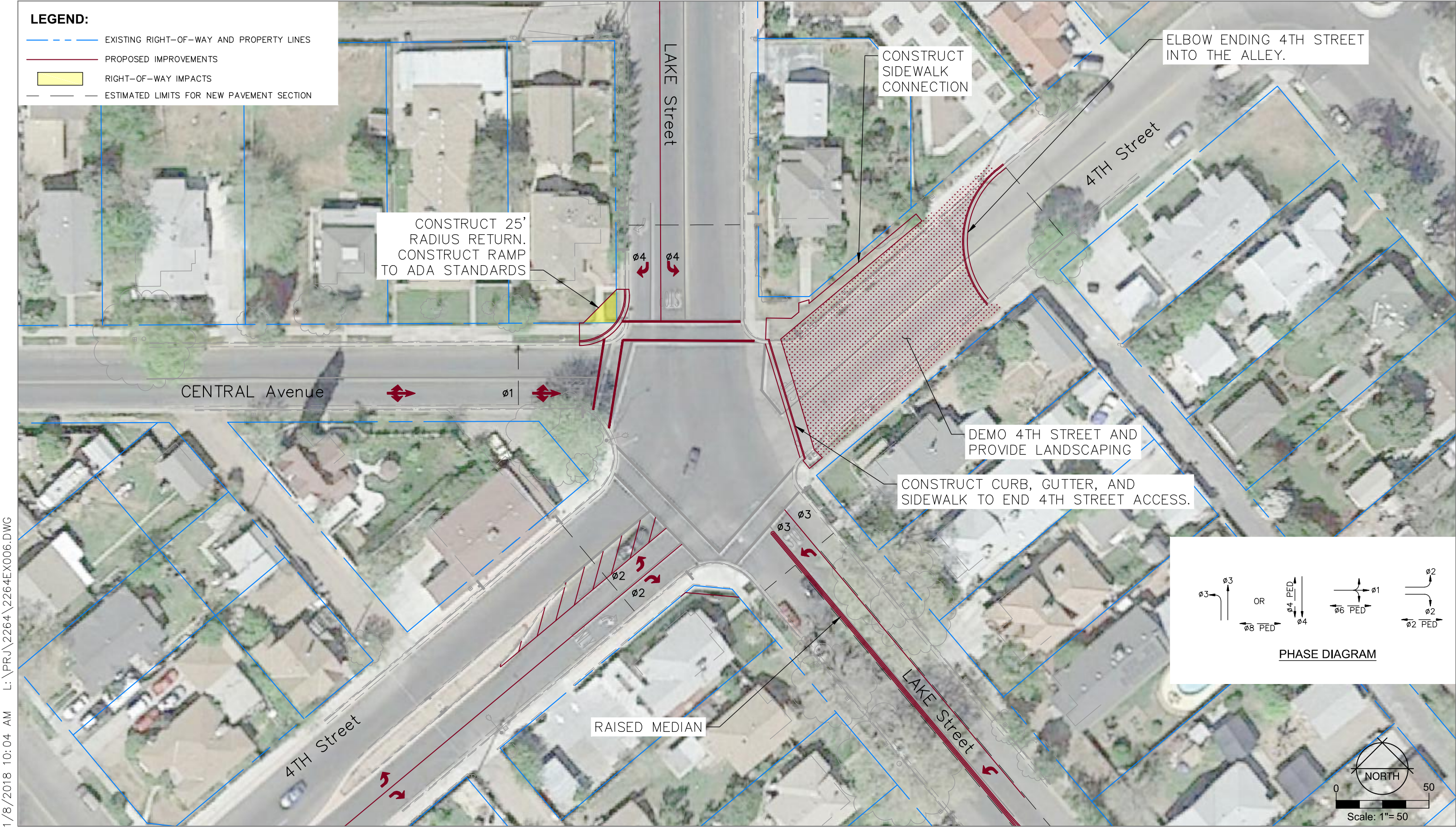
APPENDIX B – TRAFFIC SIGNAL ALTERNATIVE

SIGNAL LAYOUT & TRUCK TURN EXHIBITS

SYNCHRO/SIMTRAFFIC ANALYSIS

CONSTRUCTION COST ESTIMATE

Traffic Signal Alternative: Preliminary Layout



1/8/2018 10:04 AM L:\PRJ\2264\2264EX006.DWG

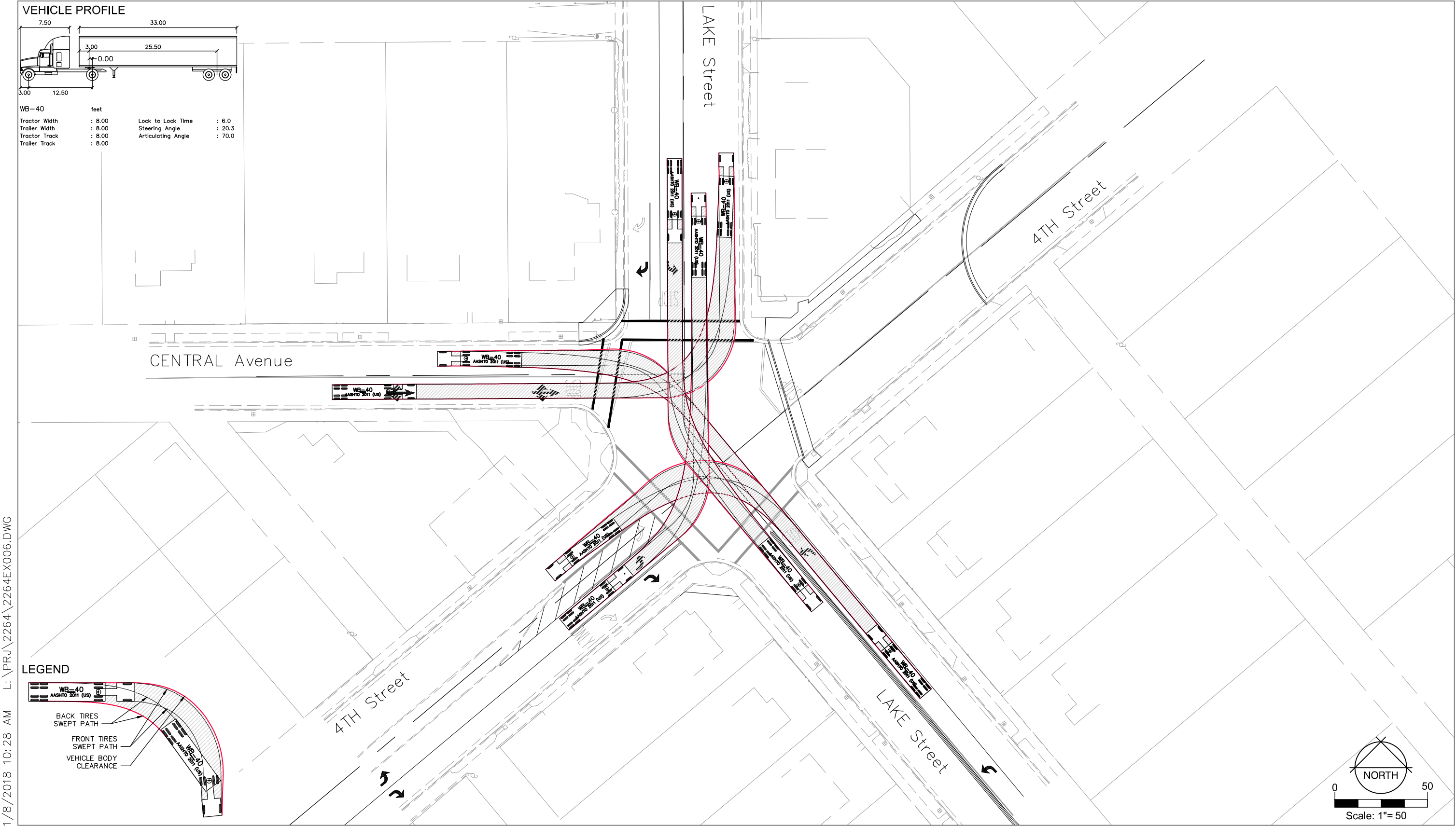
LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Madera, California

Figure B1

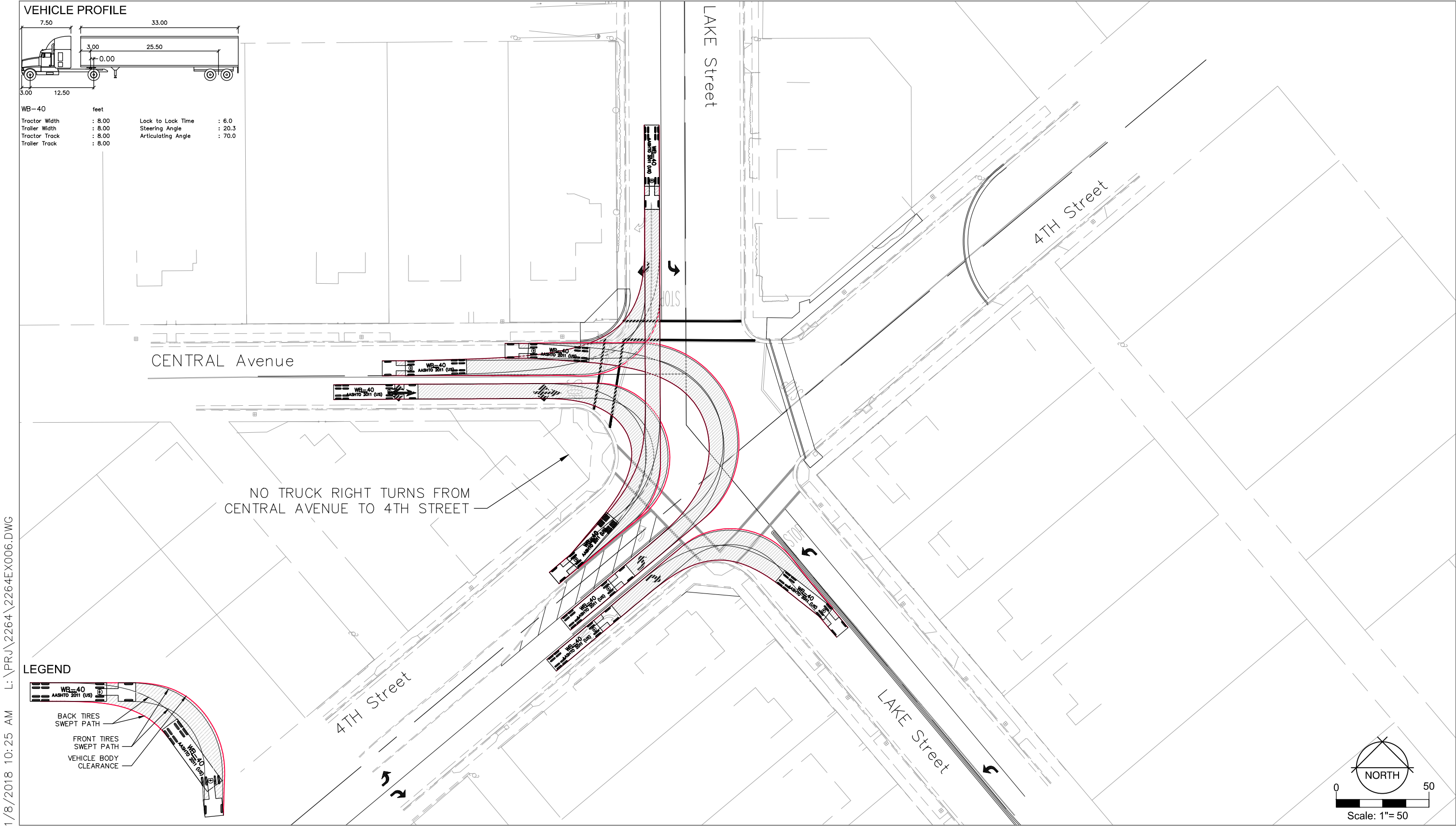


WB-40 Truck Turn (Left-Turn Movement Only)



1/8/2018 10:28 AM L:\PRJ\2264\2264EX006.DWG

WB-40 Truck Turn (Right-Turn Movement Only)



LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Madera, California

Figure B3



Queues
2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative 2040 (AM)



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | SEL |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 199 | 128 | 85 | 191 | 243 | 333 | 112 |
| v/c Ratio | 0.56 | 0.28 | 0.28 | 0.60 | 0.60 | 0.69 | 0.43 |
| Control Delay | 31.0 | 2.9 | 29.6 | 38.0 | 30.1 | 19.6 | 31.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 31.0 | 2.9 | 29.6 | 38.0 | 30.1 | 19.6 | 31.3 |
| Queue Length 50th (ft) | 67 | 0 | 28 | 66 | 79 | 44 | 39 |
| Queue Length 95th (ft) | 158 | 15 | 85 | #220 | 189 | #182 | 95 |
| Internal Link Dist (ft) | 442 | | | 427 | 397 | | 458 |
| Turn Bay Length (ft) | 200 | | 200 | | | 200 | |
| Base Capacity (vph) | 425 | 517 | 344 | 362 | 517 | 563 | 280 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.47 | 0.25 | 0.25 | 0.53 | 0.47 | 0.59 | 0.40 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative 2040 (AM)



| Movement | EBL2 | EBL | EBR | NBL2 | NBL | NBT | SBT | SBR | SBR2 | SEL | SER | SER2 |
|------------------------|------|-------|------|-------|-------|-------|-------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 1 | 182 | 118 | 47 | 31 | 176 | 224 | 272 | 34 | 18 | 82 | 3 |
| Future Volume (vph) | 1 | 182 | 118 | 47 | 31 | 176 | 224 | 272 | 34 | 18 | 82 | 3 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 13 | 13 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | 1.00 | 0.98 | | 0.99 | | |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frt | | 1.00 | 0.85 | | 1.00 | 1.00 | 1.00 | 0.85 | | 0.89 | | |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.99 | | |
| Satd. Flow (prot) | | 1629 | 1439 | | 1699 | 1788 | 1731 | 1439 | | 1508 | | |
| Flt Permitted | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.99 | | |
| Satd. Flow (perm) | | 1629 | 1439 | | 1699 | 1788 | 1731 | 1439 | | 1508 | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 1 | 198 | 128 | 51 | 34 | 191 | 243 | 296 | 37 | 20 | 89 | 3 |
| RTOR Reduction (vph) | 0 | 0 | 101 | 0 | 0 | 0 | 0 | 147 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 199 | 27 | 0 | 85 | 191 | 243 | 186 | 0 | 112 | 0 | 0 |
| Confl. Peds. (#/hr) | 6 | | | 3 | | | | | | 8 | | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | 1 |
| Heavy Vehicles (%) | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% |
| Turn Type | Perm | Perm | Perm | Split | Split | NA | NA | Perm | | Prot | | |
| Protected Phases | | | | 3 | 3 | 3 | 4 | | | 1 | | |
| Permitted Phases | 2 | 2 | 2 | | | | | 4 | | | | |
| Actuated Green, G (s) | | 12.2 | 12.2 | | 6.8 | 6.8 | 13.3 | 13.3 | | 6.8 | | |
| Effective Green, g (s) | | 12.2 | 12.2 | | 6.8 | 6.8 | 13.3 | 13.3 | | 6.8 | | |
| Actuated g/C Ratio | | 0.21 | 0.21 | | 0.12 | 0.12 | 0.23 | 0.23 | | 0.12 | | |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | | |
| Lane Grp Cap (vph) | | 348 | 307 | | 202 | 212 | 403 | 335 | | 179 | | |
| v/s Ratio Prot | | | | | 0.05 | c0.11 | c0.14 | | | c0.07 | | |
| v/s Ratio Perm | | c0.12 | 0.02 | | | | | 0.13 | | | | |
| v/c Ratio | | 0.57 | 0.09 | | 0.42 | 0.90 | 0.60 | 0.56 | | 0.63 | | |
| Uniform Delay, d1 | | 20.1 | 18.0 | | 23.3 | 24.8 | 19.5 | 19.3 | | 23.9 | | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Incremental Delay, d2 | | 2.3 | 0.1 | | 1.4 | 35.9 | 2.5 | 2.0 | | 6.7 | | |
| Delay (s) | | 22.4 | 18.1 | | 24.7 | 60.7 | 22.1 | 21.3 | | 30.6 | | |
| Level of Service | | C | B | | C | E | C | C | | C | | |
| Approach Delay (s) | | 20.7 | | | | 49.7 | 21.6 | | | 30.6 | | |
| Approach LOS | | C | | | | D | C | | | C | | |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 28.2 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.65 | | |
| Actuated Cycle Length (s) | 57.1 | Sum of lost time (s) | 18.0 |
| Intersection Capacity Utilization | 49.3% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

Queues
2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative (AM)



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | SEL |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 180 | 116 | 77 | 173 | 220 | 300 | 99 |
| v/c Ratio | 0.48 | 0.23 | 0.25 | 0.53 | 0.59 | 0.61 | 0.35 |
| Control Delay | 24.8 | 1.0 | 25.9 | 33.8 | 32.6 | 14.7 | 25.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 24.8 | 1.0 | 25.9 | 33.8 | 32.6 | 14.7 | 25.2 |
| Queue Length 50th (ft) | 49 | 0 | 20 | 49 | 60 | 18 | 28 |
| Queue Length 95th (ft) | 107 | 0 | 64 | #159 | #189 | #100 | 65 |
| Internal Link Dist (ft) | 442 | | | 427 | 397 | | 458 |
| Turn Bay Length (ft) | 200 | | 200 | | | 200 | |
| Base Capacity (vph) | 442 | 557 | 337 | 355 | 436 | 533 | 279 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.41 | 0.21 | 0.23 | 0.49 | 0.50 | 0.56 | 0.35 |

Intersection Summary




















95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative (AM)

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL2 | EBL | EBR | NBL2 | NBL | NBT | SBT | SBR | SBR2 | SEL | SER | SER2 |
| Lane Configurations | |  |  | |  |  |  |  | |  | | |
| Traffic Volume (vph) | 1 | 145 | 94 | 37 | 25 | 140 | 178 | 216 | 27 | 14 | 65 | 2 |
| Future Volume (vph) | 1 | 145 | 94 | 37 | 25 | 140 | 178 | 216 | 27 | 14 | 65 | 2 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 13 | 13 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | 1.00 | 0.98 | | 0.99 | | |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frt | | 1.00 | 0.85 | | 1.00 | 1.00 | 1.00 | 0.85 | | 0.89 | | |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.99 | | |
| Satd. Flow (prot) | | 1631 | 1438 | | 1699 | 1788 | 1731 | 1439 | | 1507 | | |
| Flt Permitted | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.99 | | |
| Satd. Flow (perm) | | 1631 | 1438 | | 1699 | 1788 | 1731 | 1439 | | 1507 | | |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 1 | 179 | 116 | 46 | 31 | 173 | 220 | 267 | 33 | 17 | 80 | 2 |
| RTOR Reduction (vph) | 0 | 0 | 97 | 0 | 0 | 0 | 0 | 179 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 180 | 19 | 0 | 77 | 173 | 220 | 121 | 0 | 99 | 0 | 0 |
| Confl. Peds. (#/hr) | 6 | | | 3 | | | | | | 8 | | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | 1 |
| Heavy Vehicles (%) | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% | 4% |
| Turn Type | Perm | Perm | Perm | Split | Split | NA | NA | Perm | | Prot | | |
| Protected Phases | | | | 3 | 3 | 3 | 4 | | | 1 | | |
| Permitted Phases | 2 | 2 | 2 | | | | | 4 | | | | |
| Actuated Green, G (s) | | 7.7 | 7.7 | | 5.3 | 5.3 | 10.2 | 10.2 | | 5.7 | | |
| Effective Green, g (s) | | 7.7 | 7.7 | | 5.3 | 5.3 | 10.2 | 10.2 | | 5.7 | | |
| Actuated g/C Ratio | | 0.16 | 0.16 | | 0.11 | 0.11 | 0.22 | 0.22 | | 0.12 | | |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | | |
| Lane Grp Cap (vph) | | 267 | 236 | | 191 | 202 | 376 | 312 | | 183 | | |
| v/s Ratio Prot | | | | | 0.05 | c0.10 | c0.13 | | | c0.07 | | |
| v/s Ratio Perm | | c0.11 | 0.01 | | | | | 0.08 | | | | |
| v/c Ratio | | 0.67 | 0.08 | | 0.40 | 0.86 | 0.59 | 0.39 | | 0.54 | | |
| Uniform Delay, d1 | | 18.4 | 16.6 | | 19.3 | 20.4 | 16.5 | 15.7 | | 19.4 | | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Incremental Delay, d2 | | 6.6 | 0.1 | | 1.4 | 28.1 | 2.3 | 0.8 | | 3.2 | | |
| Delay (s) | | 25.0 | 16.7 | | 20.7 | 48.6 | 18.8 | 16.5 | | 22.6 | | |
| Level of Service | | C | B | | C | D | B | B | | C | | |
| Approach Delay (s) | | 21.8 | | | | 40.0 | 17.4 | | | 22.6 | | |
| Approach LOS | | C | | | | D | B | | | C | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 23.8 | | | HCM 2000 Level of Service | | | | C | | |
| HCM 2000 Volume to Capacity ratio | | | 0.65 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 46.9 | | | Sum of lost time (s) | | | | 18.0 | | |
| Intersection Capacity Utilization | | | 42.8% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Queues
2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative 2040 (PM)



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | SEL |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 303 | 132 | 124 | 358 | 291 | 263 | 125 |
| v/c Ratio | 0.85 | 0.30 | 0.32 | 0.87 | 0.84 | 0.64 | 0.63 |
| Control Delay | 52.8 | 6.0 | 28.8 | 52.1 | 53.4 | 21.0 | 47.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 52.8 | 6.0 | 28.8 | 52.1 | 53.4 | 21.0 | 47.9 |
| Queue Length 50th (ft) | 134 | 0 | 47 | 158 | 132 | 45 | 58 |
| Queue Length 95th (ft) | #321 | 36 | 113 | #377 | #290 | 138 | 115 |
| Internal Link Dist (ft) | 442 | | | 427 | 397 | | 458 |
| Turn Bay Length (ft) | 200 | | 200 | | | 150 | |
| Base Capacity (vph) | 387 | 461 | 425 | 447 | 362 | 423 | 197 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.78 | 0.29 | 0.29 | 0.80 | 0.80 | 0.62 | 0.63 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative 2040 (PM)



| Movement | EBL2 | EBL | EBR | NBL2 | NBL | NBT | SBT | SBR | SBR2 | SEL | SER | SER2 |
|-----------------------------------|------|-------|-------|-------|-------|---------------------------|-------|------|------|-------|------|------|
| Lane Configurations | | ↰ | ↱ | | ↰ | ↱ | ↱ | ↱ | | ↰ | ↱ | ↱ |
| Traffic Volume (vph) | 1 | 278 | 121 | 60 | 54 | 329 | 268 | 189 | 53 | 40 | 73 | 3 |
| Future Volume (vph) | 1 | 278 | 121 | 60 | 54 | 329 | 268 | 189 | 53 | 40 | 73 | 3 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 13 | 13 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | 1.00 | 0.98 | | 0.99 | | |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frt | | 1.00 | 0.85 | | 1.00 | 1.00 | 1.00 | 0.85 | | 0.91 | | |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.98 | | |
| Satd. Flow (prot) | | 1672 | 1482 | | 1750 | 1842 | 1782 | 1482 | | 1582 | | |
| Flt Permitted | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.98 | | |
| Satd. Flow (perm) | | 1672 | 1482 | | 1750 | 1842 | 1782 | 1482 | | 1582 | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 1 | 302 | 132 | 65 | 59 | 358 | 291 | 205 | 58 | 43 | 79 | 3 |
| RTOR Reduction (vph) | 0 | 0 | 104 | 0 | 0 | 0 | 0 | 123 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 303 | 28 | 0 | 124 | 358 | 291 | 140 | 0 | 125 | 0 | 0 |
| Confl. Peds. (#/hr) | 6 | | | 3 | | | | | | 8 | | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | 1 |
| Turn Type | Perm | Perm | Perm | Split | Split | NA | NA | Perm | | Prot | | |
| Protected Phases | | | | 3 | 3 | 3 | 4 | | | 1 | | |
| Permitted Phases | 2 | 2 | 2 | | | | | 4 | | | | |
| Actuated Green, G (s) | | 16.1 | 16.1 | | 16.9 | 16.9 | 14.6 | 14.6 | | 9.4 | | |
| Effective Green, g (s) | | 16.1 | 16.1 | | 16.9 | 16.9 | 14.6 | 14.6 | | 9.4 | | |
| Actuated g/C Ratio | | 0.21 | 0.21 | | 0.23 | 0.23 | 0.19 | 0.19 | | 0.13 | | |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | | |
| Lane Grp Cap (vph) | | 358 | 318 | | 394 | 415 | 346 | 288 | | 198 | | |
| v/s Ratio Prot | | | | | 0.07 | c0.19 | c0.16 | | | c0.08 | | |
| v/s Ratio Perm | | c0.18 | 0.02 | | | | | 0.09 | | | | |
| v/c Ratio | | 0.85 | 0.09 | | 0.31 | 0.86 | 0.84 | 0.49 | | 0.63 | | |
| Uniform Delay, d1 | | 28.3 | 23.6 | | 24.2 | 27.9 | 29.1 | 26.9 | | 31.2 | | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Incremental Delay, d2 | | 16.6 | 0.1 | | 0.5 | 16.7 | 16.6 | 1.3 | | 6.4 | | |
| Delay (s) | | 44.9 | 23.7 | | 24.7 | 44.6 | 45.7 | 28.1 | | 37.6 | | |
| Level of Service | | D | C | | C | D | D | C | | D | | |
| Approach Delay (s) | | 38.5 | | | | 39.5 | 37.4 | | | 37.6 | | |
| Approach LOS | | D | | | | D | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 38.3 | | | HCM 2000 Level of Service | | | | D | | |
| HCM 2000 Volume to Capacity ratio | | | 0.81 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 75.0 | | | Sum of lost time (s) | | | | 18.0 | | |
| Intersection Capacity Utilization | | | 60.1% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Queues
2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative (PM)



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | SEL |
|-------------------------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 227 | 98 | 93 | 267 | 182 | 196 | 94 |
| v/c Ratio | 0.66 | 0.21 | 0.27 | 0.74 | 0.58 | 0.45 | 0.44 |
| Control Delay | 33.5 | 1.0 | 26.4 | 40.3 | 32.3 | 7.5 | 32.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.5 | 1.0 | 26.4 | 40.3 | 32.3 | 7.5 | 32.0 |
| Queue Length 50th (ft) | 69 | 0 | 26 | 81 | 57 | 0 | 30 |
| Queue Length 95th (ft) | 183 | 0 | 90 | #301 | 146 | 46 | 83 |
| Internal Link Dist (ft) | 442 | | | 427 | 397 | | 458 |
| Turn Bay Length (ft) | 200 | | 200 | | | 200 | |
| Base Capacity (vph) | 385 | 500 | 383 | 403 | 335 | 453 | 216 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.59 | 0.20 | 0.24 | 0.66 | 0.54 | 0.43 | 0.44 |

Intersection Summary




















95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis

2: N Lake St & E 4th St & Central Ave

4th/Lake/Central Intersection Improvement

B-Traffic Signal Alternative (PM)

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL2 | EBL | EBR | NBL2 | NBL | NBT | SBT | SBR | SBR2 | SEL | SER | SER2 |
| Lane Configurations | |  |  | |  |  |  |  | |  | | |
| Traffic Volume (vph) | 1 | 221 | 96 | 48 | 43 | 262 | 178 | 150 | 42 | 32 | 58 | 2 |
| Future Volume (vph) | 1 | 221 | 96 | 48 | 43 | 262 | 178 | 150 | 42 | 32 | 58 | 2 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 12 | 12 | 12 | 12 | 13 | 13 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | 1.00 | 1.00 | | 0.99 | | |
| Flpb, ped/bikes | | 0.99 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Frt | | 1.00 | 0.85 | | 1.00 | 1.00 | 1.00 | 0.85 | | 0.91 | | |
| Flt Protected | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.98 | | |
| Satd. Flow (prot) | | 1677 | 1482 | | 1750 | 1842 | 1782 | 1515 | | 1583 | | |
| Flt Permitted | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 1.00 | | 0.98 | | |
| Satd. Flow (perm) | | 1677 | 1482 | | 1750 | 1842 | 1782 | 1515 | | 1583 | | |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 1 | 226 | 98 | 49 | 44 | 267 | 182 | 153 | 43 | 33 | 59 | 2 |
| RTOR Reduction (vph) | 0 | 0 | 78 | 0 | 0 | 0 | 0 | 161 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 227 | 20 | 0 | 93 | 267 | 182 | 35 | 0 | 94 | 0 | 0 |
| Confl. Peds. (#/hr) | 6 | | | 3 | | | | | | 8 | | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 1 | | | 1 |
| Turn Type | Perm | Perm | Perm | Split | Split | NA | NA | Prot | | Prot | | |
| Protected Phases | | | | 3 | 3 | 3 | 4 | 4 | | 1 | | |
| Permitted Phases | 2 | 2 | 2 | | | | | | | | | |
| Actuated Green, G (s) | | 11.6 | 11.6 | | 11.1 | 11.1 | 10.0 | 10.0 | | 5.9 | | |
| Effective Green, g (s) | | 11.6 | 11.6 | | 11.1 | 11.1 | 10.0 | 10.0 | | 5.9 | | |
| Actuated g/C Ratio | | 0.20 | 0.20 | | 0.20 | 0.20 | 0.18 | 0.18 | | 0.10 | | |
| Clearance Time (s) | | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.5 | | 4.5 | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | | |
| Lane Grp Cap (vph) | | 343 | 303 | | 343 | 361 | 314 | 267 | | 165 | | |
| v/s Ratio Prot | | | | | 0.05 | c0.14 | c0.10 | 0.02 | | c0.06 | | |
| v/s Ratio Perm | | c0.14 | 0.01 | | | | | | | | | |
| v/c Ratio | | 0.66 | 0.07 | | 0.27 | 0.74 | 0.58 | 0.13 | | 0.57 | | |
| Uniform Delay, d1 | | 20.7 | 18.1 | | 19.3 | 21.4 | 21.4 | 19.6 | | 24.1 | | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | | |
| Incremental Delay, d2 | | 4.7 | 0.1 | | 0.4 | 7.7 | 2.6 | 0.2 | | 4.5 | | |
| Delay (s) | | 25.4 | 18.2 | | 19.7 | 29.1 | 24.0 | 19.9 | | 28.6 | | |
| Level of Service | | C | B | | B | C | C | B | | C | | |
| Approach Delay (s) | | 23.3 | | | | 26.7 | 21.8 | | | 28.6 | | |
| Approach LOS | | C | | | | C | C | | | C | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 24.3 | | | HCM 2000 Level of Service | | | | C | | |
| HCM 2000 Volume to Capacity ratio | | | 0.65 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 56.6 | | | Sum of lost time (s) | | | | 18.0 | | |
| Intersection Capacity Utilization | | | 49.0% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Preliminary Opinion of Costs (Construction Costs Only)

4th Street/Lake Street/Central Avenue Intersection - **Signal Alternative**

City of Madera

1/12/2018

55-4549-03/2264

| No. | Item Description | Units | Quantity | Unit Cost | Total |
|-----|---------------------------------------|-------|----------|--------------|------------------------|
| 1 | Traffic Control System | LS | 1 | \$60,000.00 | \$60,000.00 |
| 2 | Remove Thermoplastic Traffic Stripe | LF | 200 | \$4.25 | \$850.00 |
| 3 | Remove Thermoplastic Pavement Marking | SQFT | 50 | \$12.50 | \$625.00 |
| 4 | Remove Roadside Sign | EA | 10 | \$155.00 | \$1,550.00 |
| 5 | Remove Concrete Sidewalk | SQYD | 30 | \$31.50 | \$945.00 |
| 6 | Remove Concrete (Curb & Gutter) | LF | 340 | \$12.50 | \$4,250.00 |
| 7 | Roadway Excavation | CY | 560 | \$32.00 | \$17,920.00 |
| 8 | Class 2 Aggregate Base | CY | 150 | \$53.00 | \$7,950.00 |
| 9 | Hot Mix Asphalt (Type B) | TON | 140 | \$90.00 | \$12,600.00 |
| 10 | Minor Concrete (Median Curb) | CY | 20 | \$770.00 | \$15,400.00 |
| 11 | Minor Concrete (Curb and Gutter) | CY | 10 | \$355.00 | \$3,550.00 |
| 12 | Minor Concrete (Medians) | SQFT | 150 | \$6.00 | \$900.00 |
| 13 | Minor Concrete (Sidewalk) | CY | 20 | \$540.00 | \$10,800.00 |
| 14 | Thermoplastic Traffic Stripe | LF | 1000 | \$2.00 | \$2,000.00 |
| 15 | Thermoplastic Pavement Marking | SQFT | 840 | \$7.00 | \$5,880.00 |
| 16 | Landscape | SQFT | 7800 | \$5.00 | \$39,000.00 |
| 17 | Signs | EA | 20 | \$380.00 | \$7,600.00 |
| 18 | Signals and Lighting | LS | 1 | \$350,000.00 | \$350,000.00 |
| 19 | Storm Drain System | LS | 1 | \$50,000.00 | \$50,000.00 |
| 20 | Mobilization | LS | 1 | \$53,200.00 | \$53,200.00 |
| | Subtotal (Construction Costs) | | | | \$ 645,020.00 |
| | Minor/ Supplemental Items | | | 30% | \$ 194,000.00 |
| | Construction Contingency | | | 25% | \$ 210,000.00 |
| | Total Construction Costs | | | | \$ 1,049,020.00 |
| | Rounded | | | | \$ 1,050,000.00 |

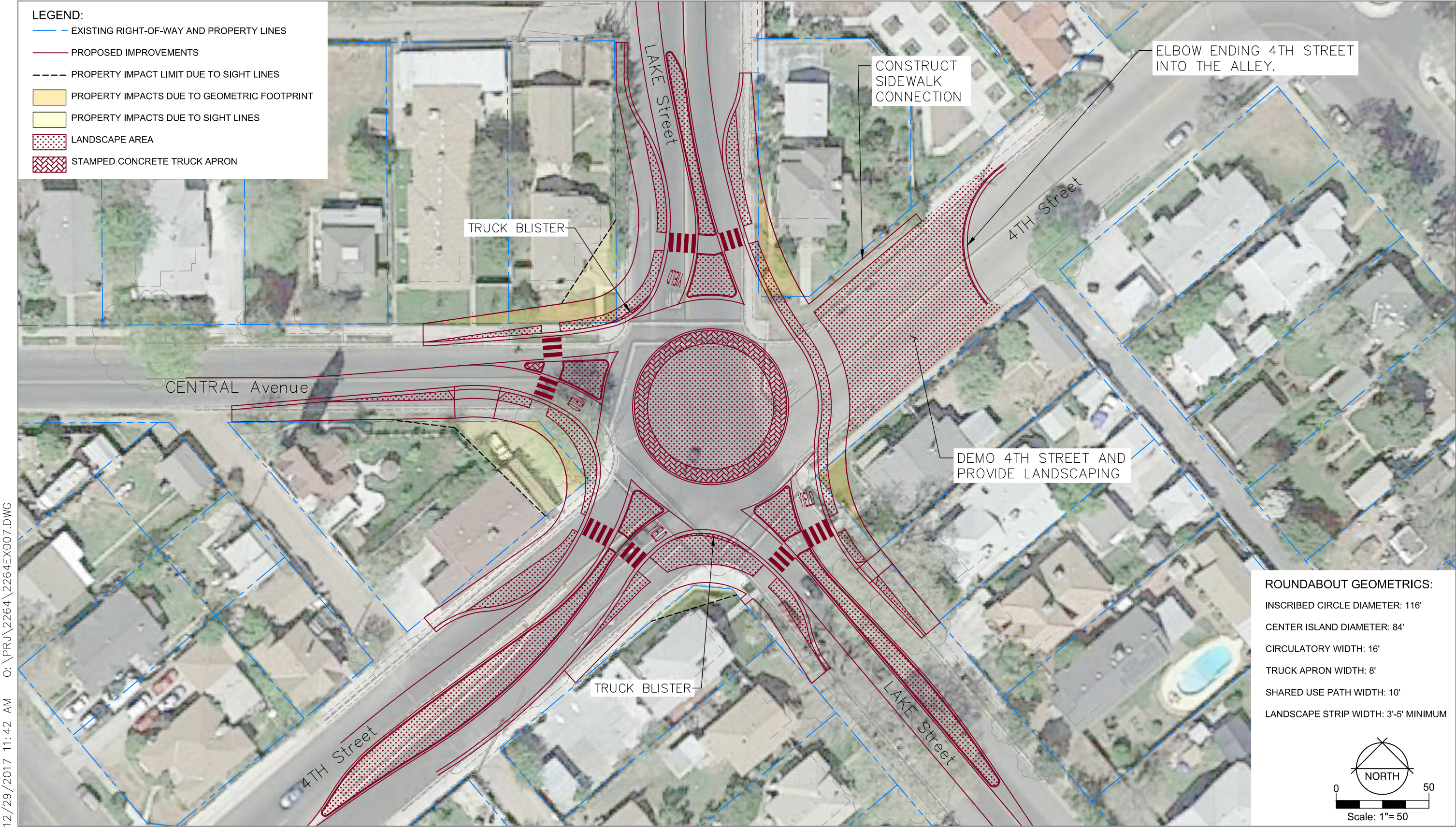
APPENDIX C – ROUNDABOUT ALTERNATIVE

ROUNDABOUT LAYOUT, FASTEST PATH, & TRUCK TURN EXHIBITS

SIDRA 7 ANALYSIS

CONSTRUCTION COST ESTIMATE

Roundabout Alternative: Preliminary Layout



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LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

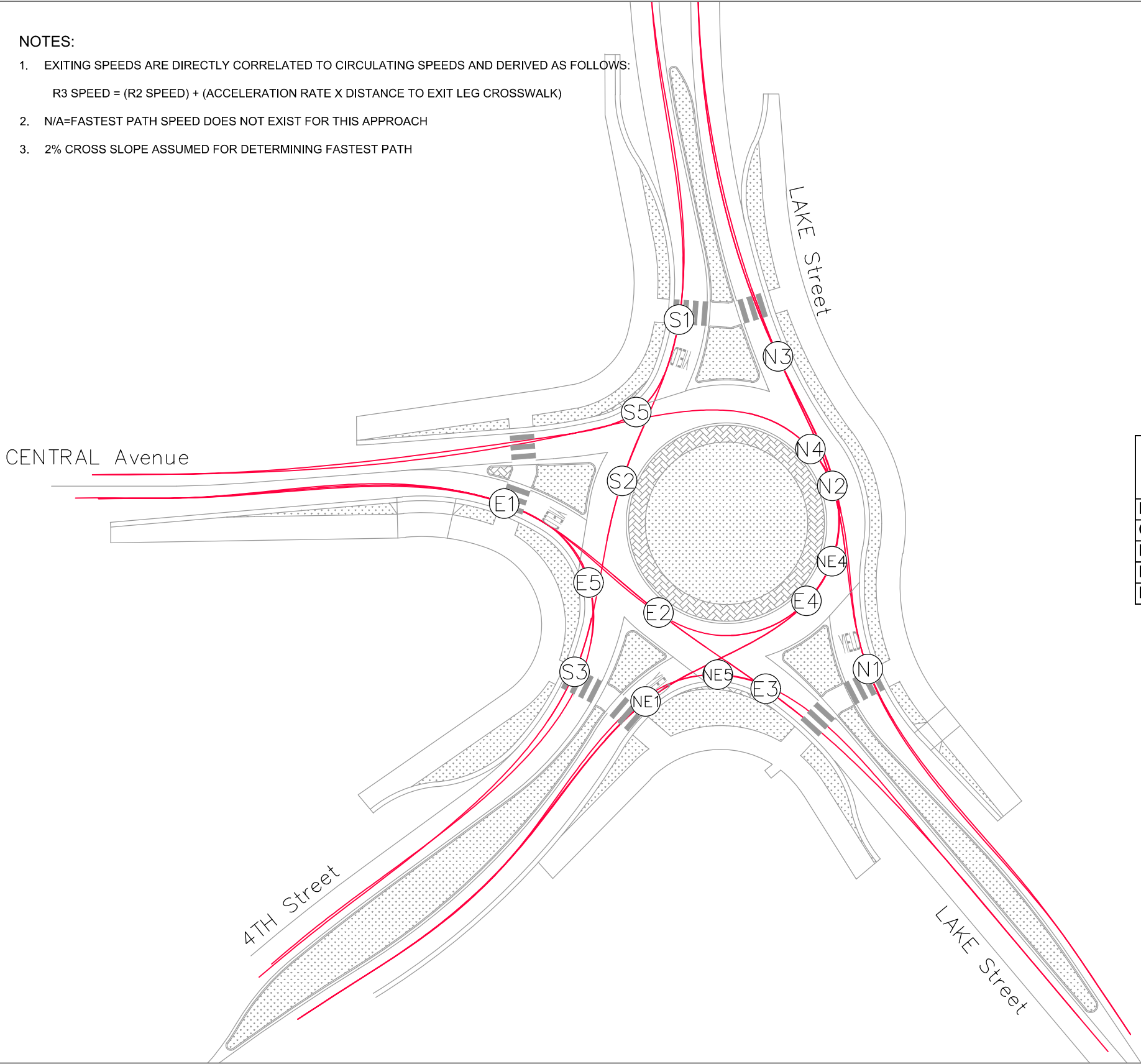
Madera, California

Figure C1



NOTES:

- 1. EXITING SPEEDS ARE DIRECTLY CORRELATED TO CIRCULATING SPEEDS AND DERIVED AS FOLLOWS:
R3 SPEED = (R2 SPEED) + (ACCELERATION RATE X DISTANCE TO EXIT LEG CROSSWALK)
- 2. N/A=FASTEST PATH SPEED DOES NOT EXIST FOR THIS APPROACH
- 3. 2% CROSS SLOPE ASSUMED FOR DETERMINING FASTEST PATH

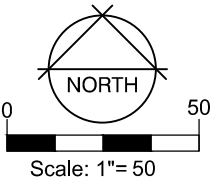


FASTEST PATH RADIUS (FT)

| MOVEMENT | NB LAKE STREET (N#) | SB LAKE STREET (S#) | NEB 4TH STREET (NE#) | EB CENTRAL AVENUE (E#) |
|------------------|---------------------|---------------------|----------------------|------------------------|
| ENTERING (R1) | 120.7 | 128.4 | 119.1 | 105.0 |
| CIRCULATING (R2) | 162.7 | 202.7 | | 399.4 |
| EXITING (R3) | 543.7 | 118.0 | | 505.0 |
| LEFT TURN (R4) | 50.2 | | 51.8 | 45.2 |
| RIGHT TURN (R5) | | 33.5 | 51.3 | 48.5 |

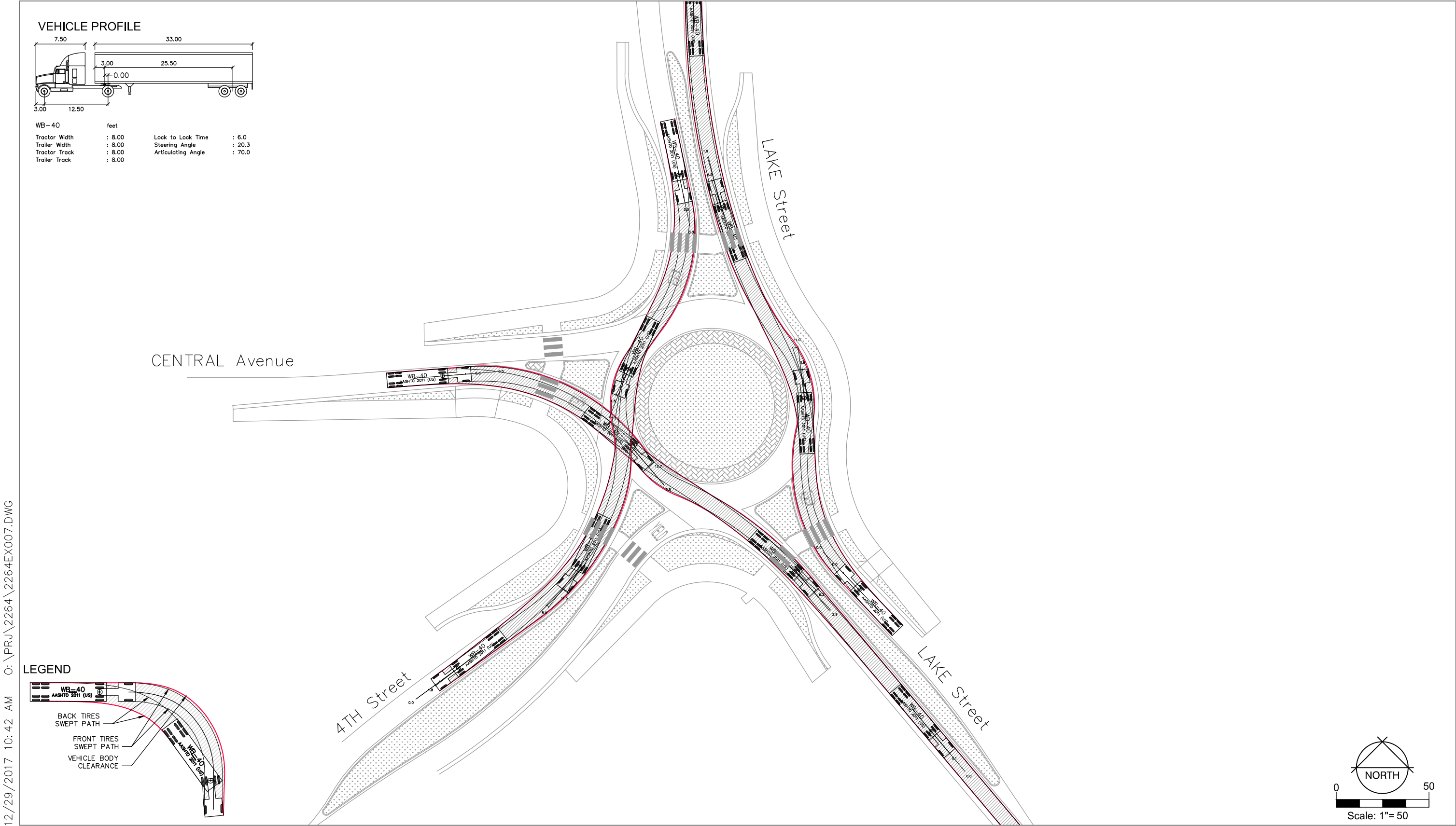
FASTEST PATH SPEED (MPH)

| MOVEMENT | NB LAKE STREET (N#) | SB LAKE STREET (S#) | NEB 4TH STREET (NE#) | EB CENTRAL AVENUE (E#) |
|------------------|---------------------|---------------------|----------------------|------------------------|
| ENTERING (R1) | 21.9 | 22.4 | 21.8 | 20.8 |
| CIRCULATING (R2) | 22.5 | 24.4 | | 31.2 |
| EXITING (R3) | 31.4 | 21.7 | | 38.1 |
| LEFT TURN (R4) | 14.6 | | 14.8 | 14.0 |
| RIGHT TURN (R5) | | 13.4 | 15.7 | 15.4 |



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WB-40 Truck Turn (Through Movement Only)



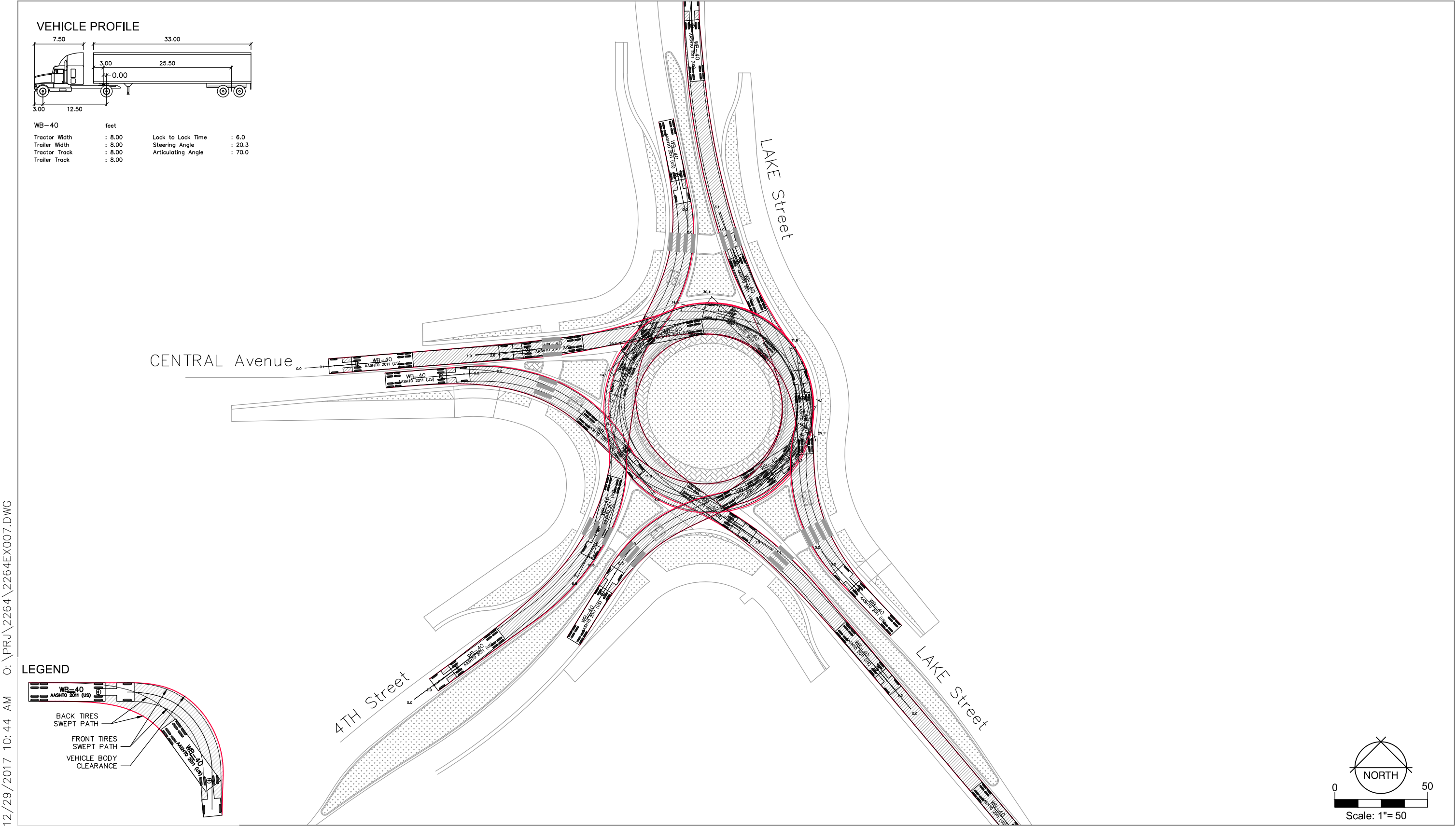
LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Figure C3

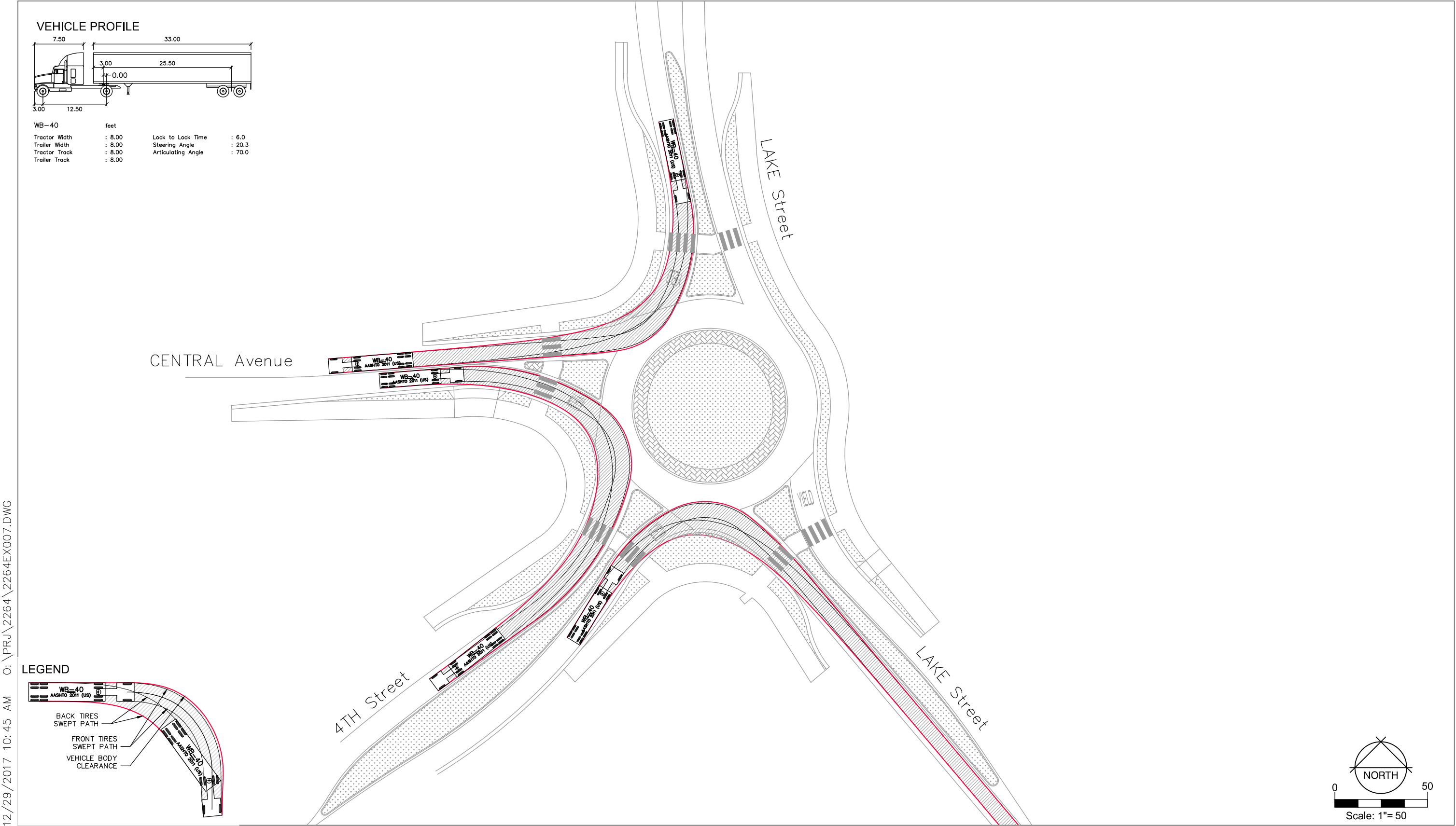


Madera, California

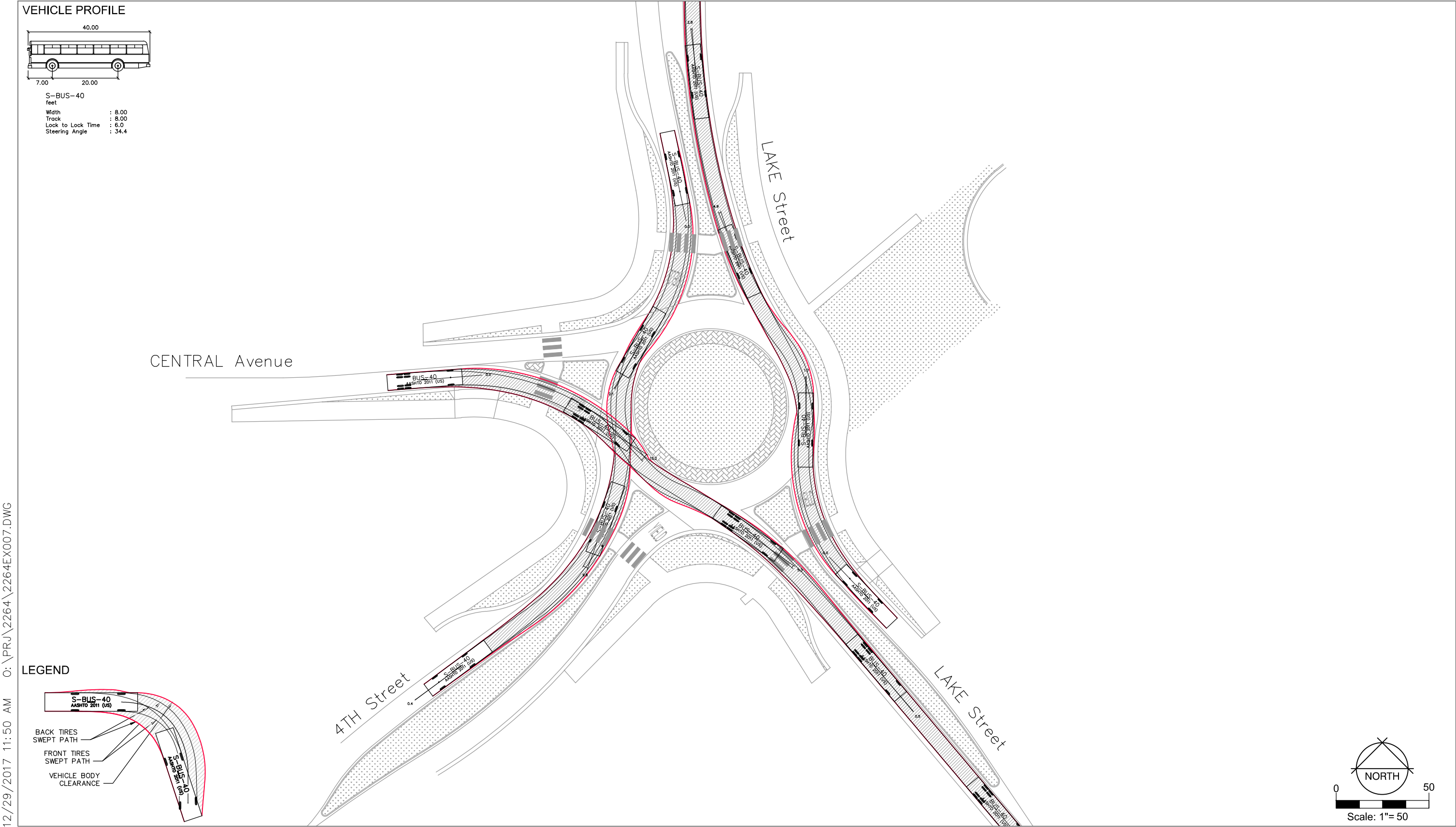
WB-40 Truck Turn (Left-Turn Movement Only)



WB-40 Truck Turn (Right-Turn Movement Only)



Bus 40 VehicleTurn (Through Movement Only)



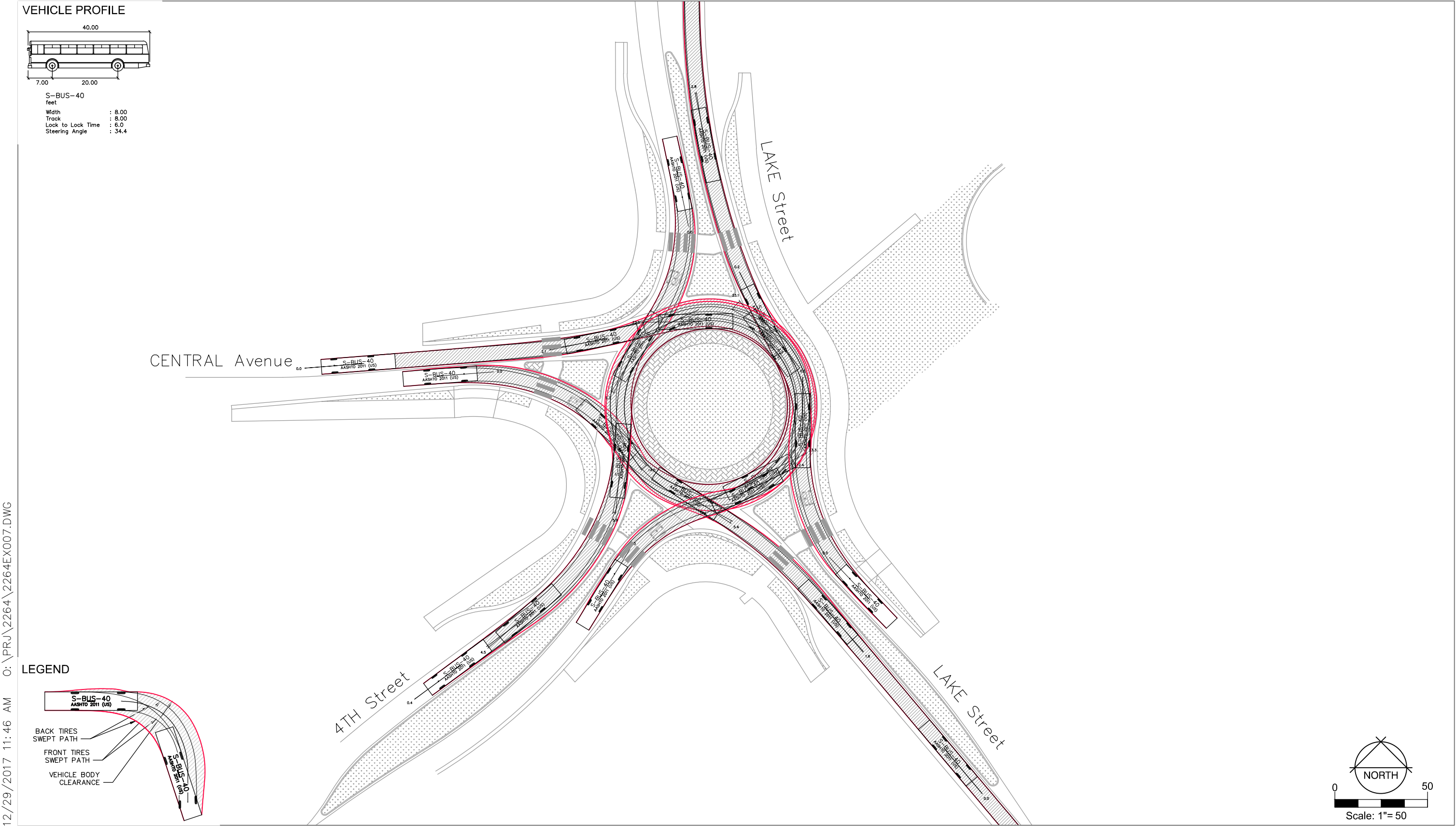
LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Madera, California

Figure C6



Bus 40 VehicleTurn (Left-Turn Movement Only)



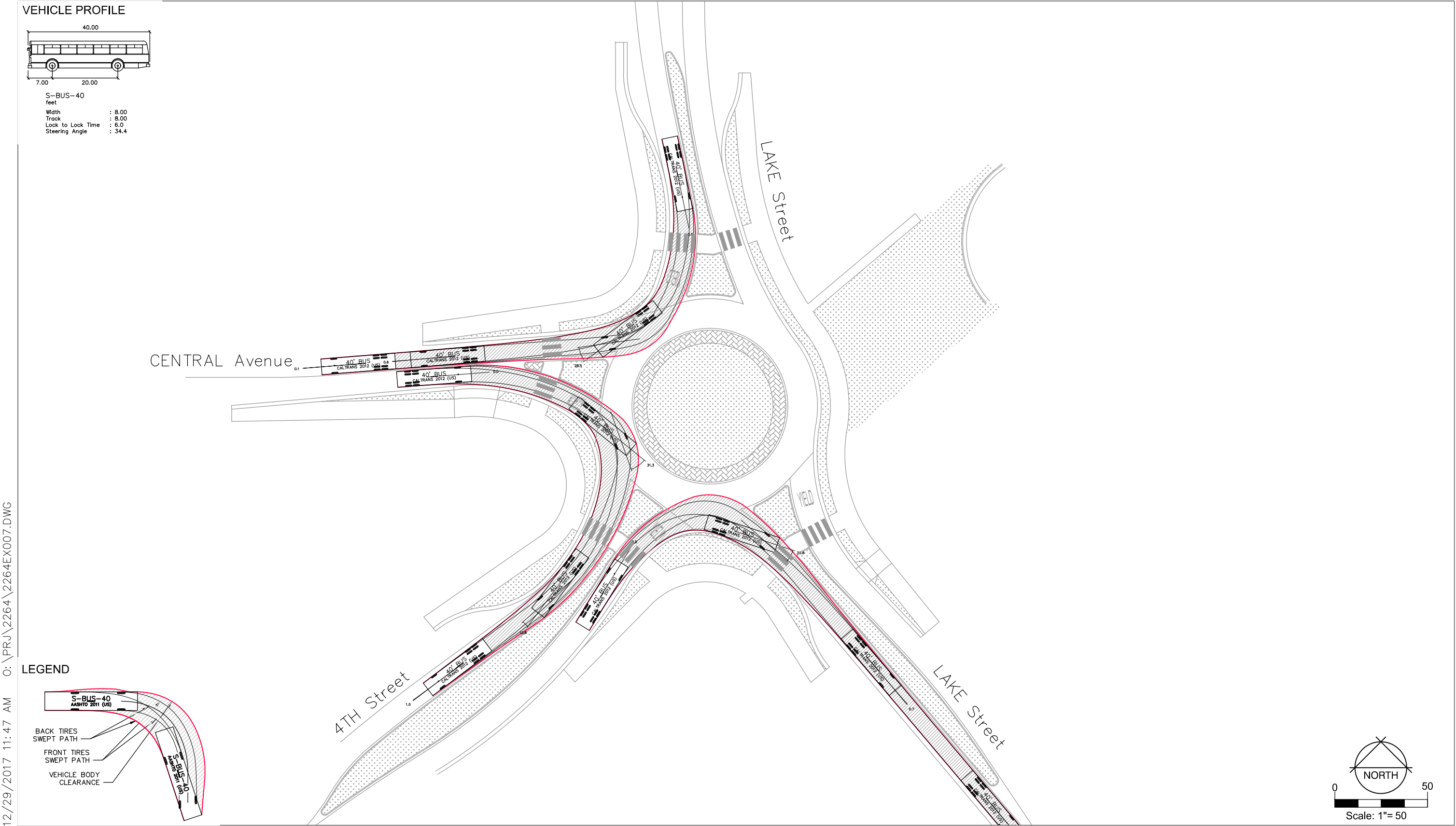
LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Madera, California

Figure C7



Bus 40 VehicleTurn (Right-Turn Movement Only)



Stopping Sight Distance

- NOTES:
- 1. STOPPING SIGHT DISTANCE CRITERIA OBTAINED FROM NCHRP REPORT 672
 - 2. STOPPING SIGHT DISTANCE IS MEASURED USING AN ASSUMED DRIVER'S EYE HEIGHT OF 3.5 FT AND AN ASSUMED OBJECT HEIGHT OF 6 INCHES.

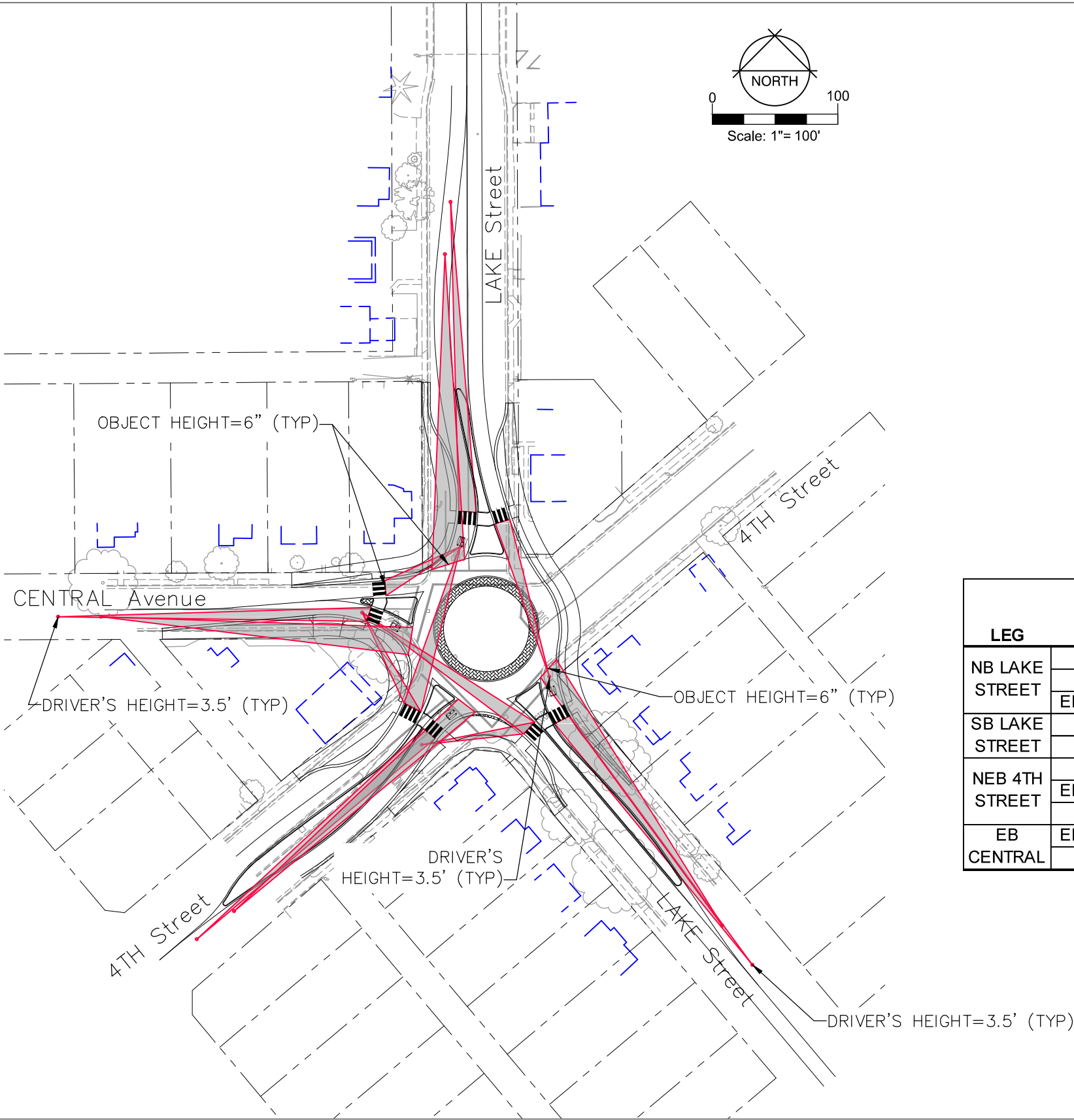
SSD - ENTRY

| APPROACH | INITIAL SPEED (MPH) | STOPPING SIGHT DISTANCE (FT) |
|-------------------|---------------------|------------------------------|
| NB LAKE STREET | 35.0 | 247.3 |
| SB LAKE STREET | 35.0 | 247.3 |
| NEB 4TH STREET | 35.0 | 247.3 |
| EB CENTRAL AVENUE | 35.0 | 247.3 |

SSD - PEDESTRIAN CROSSING

| LEG | APPROACH | CONFLICTING SPEED (MPH) | SIGHT TRIANGLE LENGTH (FT) |
|----------------|--|-------------------------|----------------------------|
| NB LAKE STREET | NB LAKE STREET INITIAL SPEED | 35.0 | 247.3 |
| | NEB 4TH STREET RIGHT TURN (V5) | 15.7 | 81.8 |
| | EB CENTRAL AVENUE CIRCULATING SPEED (V2) | 26.0 | 161.0 |
| SB LAKE STREET | SB LAKE STREET INITIAL SPEED | 35.0 | 247.3 |
| | NB LAKE STREET CIRCULATING SPEED (V2) | 22.2 | 129.2 |
| NEB 4TH STREET | NEB 4TH STREET INITIAL SPEED | 35.0 | 247.3 |
| | EB CENTRAL AVENUE RIGHT TURN (V5) | 15.4 | 79.6 |
| | SB LAKE STREET CIRCULATING SPEED (V2) | 23.4 | 139.0 |
| EB CENTRAL | EB CENTRAL AVENUE INITIAL SPEED | 35.0 | 247.3 |
| | SB LAKE STREET RIGHT TURN (V5) | 13.4 | 66.3 |

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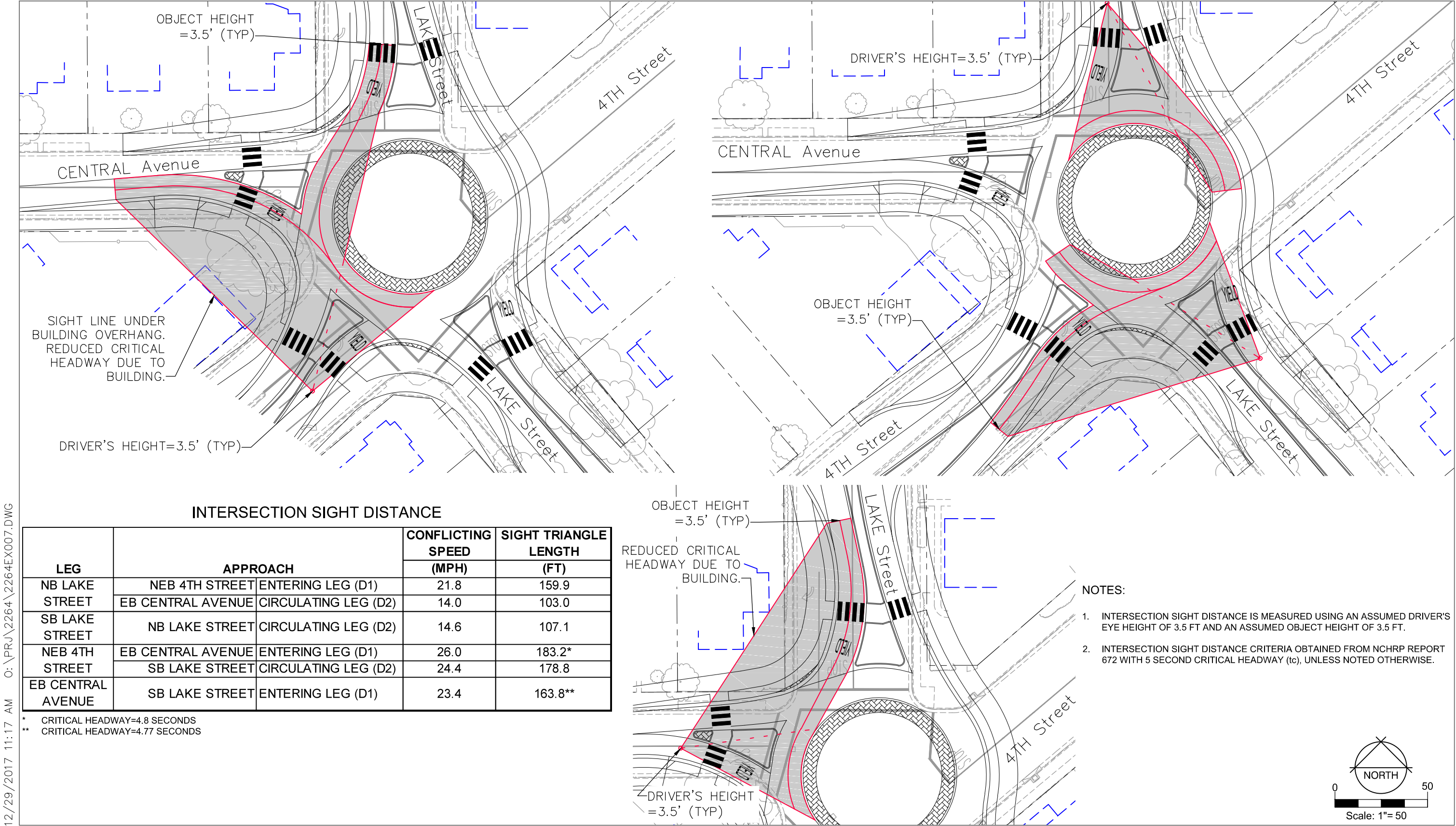
LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Madera, California

Figure C9

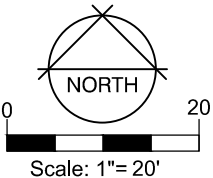
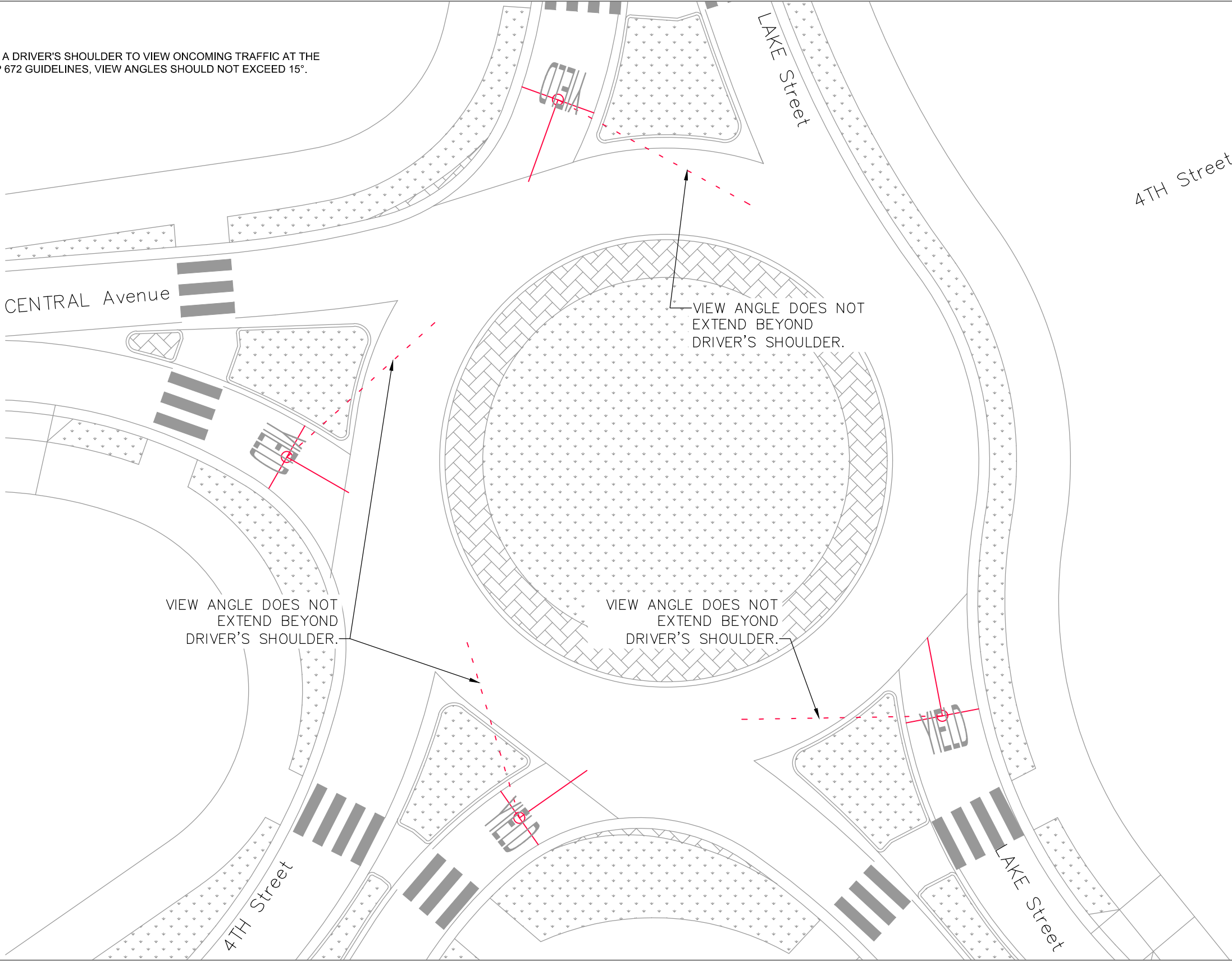


Intersection Sight Distance



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NOTE
VALUE SHOWN IS THE ANGLE BEYOND A DRIVER'S SHOULDER TO VIEW ONCOMING TRAFFIC AT THE
ROUNDAABOUT ENTRANCE. PER NCHRP 672 GUIDELINES, VIEW ANGLES SHOULD NOT EXCEED 15°.



LAKE St/4TH St/CENTRAL Ave INTX IMPROVEMENTS

Figure C11



Madera, California

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LANE SUMMARY

 **Site: 1 [2017 AM Peak Hour]**

4th Street/Lake Street/Central Avenue
2017 AM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|-----------------------------------|---------|---------------|---------------------|--------------------|-------------------------|---------------------|-------------------|------------|----------------|----------------------|-------------------|----------------------|
| | Demand Flows Total veh/h | HV % | Cap. veh/h | Deg. Satn v/c | Lane Util. % | Average Delay sec | Level of Service | 95% Back of Queue | | Lane Config | Lane Length ft | Cap. Adj. % | Prob. Block. % |
| | | | | | | | | Veh | Dist ft | | | | |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 249 | 4.0 | 1098 | 0.227 | 100 | 5.4 | LOS A | 1.4 | 35.5 | Full | 360 | 0.0 | 0.0 |
| Approach | 249 | 4.0 | | 0.227 | | 5.4 | LOS A | 1.4 | 35.5 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 520 | 4.0 | 1064 | 0.488 | 100 | 9.0 | LOS A | 3.8 | 98.6 | Full | 730 | 0.0 | 0.0 |
| Approach | 520 | 4.0 | | 0.488 | | 9.0 | LOS A | 3.8 | 98.6 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 99 | 4.0 | 777 | 0.127 | 100 | 5.9 | LOS A | 0.8 | 20.1 | Full | 450 | 0.0 | 0.0 |
| Approach | 99 | 4.0 | | 0.127 | | 5.9 | LOS A | 0.8 | 20.1 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 296 | 4.0 | 992 | 0.299 | 100 | 6.7 | LOS A | 1.9 | 48.3 | Full | 320 | 0.0 | 0.0 |
| Approach | 296 | 4.0 | | 0.299 | | 6.7 | LOS A | 1.9 | 48.3 | | | | |
| Intersection | 1164 | 4.0 | | 0.488 | | 7.4 | LOS A | 3.8 | 98.6 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 **Site: 1 [2017 PM Peak Hour]**

4th Street/Lake Street/Central Avenue
2017 PM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|--------------|-----|-------|-----------|------------|---------------|------------------|-------------------|------|-------------|-------------|-----------|--------------|
| | Demand Flows | | Cap. | Deg. Satn | Lane Util. | Average Delay | Level of Service | 95% Back of Queue | | Lane Config | Lane Length | Cap. Adj. | Prob. Block. |
| | Total | HV | | | | | | Veh | Dist | | | | |
| | veh/h | % | veh/h | v/c | % | sec | | | | | ft | % | % |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 380 | 1.0 | 1071 | 0.354 | 100 | 7.0 | LOS A | 2.4 | 60.1 | Full | 360 | 0.0 | 0.0 |
| Approach | 380 | 1.0 | | 0.354 | | 7.0 | LOS A | 2.4 | 60.1 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 435 | 1.0 | 1010 | 0.431 | 100 | 8.4 | LOS A | 3.1 | 79.3 | Full | 730 | 0.0 | 0.0 |
| Approach | 435 | 1.0 | | 0.431 | | 8.4 | LOS A | 3.1 | 79.3 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 99 | 1.0 | 897 | 0.110 | 100 | 5.1 | LOS A | 0.7 | 16.7 | Full | 450 | 0.0 | 0.0 |
| Approach | 99 | 1.0 | | 0.110 | | 5.1 | LOS A | 0.7 | 16.7 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 342 | 1.0 | 1028 | 0.333 | 100 | 6.9 | LOS A | 2.2 | 54.6 | Full | 320 | 0.0 | 0.0 |
| Approach | 342 | 1.0 | | 0.333 | | 6.9 | LOS A | 2.2 | 54.6 | | | | |
| Intersection | 1256 | 1.0 | | 0.431 | | 7.3 | LOS A | 3.1 | 79.3 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 **Site: 1 [2040 AM Peak Hour]**

4th Street/Lake Street/Central Avenue
2040 AM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|-----------------------------------|---------|---------------|---------------------|--------------------|-------------------------|---------------------|-------------------|------------|----------------|----------------------|-------------------|----------------------|
| | Demand Flows Total veh/h | HV % | Cap. veh/h | Deg. Satn v/c | Lane Util. % | Average Delay sec | Level of Service | 95% Back of Queue | | Lane Config | Lane Length ft | Cap. Adj. % | Prob. Block. % |
| | | | | | | | | Veh | Dist ft | | | | |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 314 | 4.0 | 1040 | 0.301 | 100 | 6.5 | LOS A | 2.0 | 50.8 | Full | 360 | 0.0 | 0.0 |
| Approach | 314 | 4.0 | | 0.301 | | 6.5 | LOS A | 2.0 | 50.8 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 654 | 4.0 | 994 | 0.658 | 100 | 13.6 | LOS B | 7.3 | 188.0 | Full | 730 | 0.0 | 0.0 |
| Approach | 654 | 4.0 | | 0.658 | | 13.6 | LOS B | 7.3 | 188.0 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 125 | 4.0 | 638 | 0.196 | 100 | 8.0 | LOS A | 1.3 | 34.0 | Full | 450 | 0.0 | 0.0 |
| Approach | 125 | 4.0 | | 0.196 | | 8.0 | LOS A | 1.3 | 34.0 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 372 | 4.0 | 909 | 0.409 | 100 | 8.7 | LOS A | 2.8 | 73.2 | Full | 320 | 0.0 | 0.0 |
| Approach | 372 | 4.0 | | 0.409 | | 8.7 | LOS A | 2.8 | 73.2 | | | | |
| Intersectio n | 1464 | 4.0 | | 0.658 | | 10.3 | LOS B | 7.3 | 188.0 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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LANE SUMMARY

 **Site: 1 [2040 PM Peak Hour]**

4th Street/Lake Street/Central Avenue
2040 PM Peak Hour
Roundabout

| Lane Use and Performance | | | | | | | | | | | | | |
|------------------------------|--------------|-----|-------|-----------|------------|---------------|------------------|-------------------|-------|-------------|-------------|-----------|--------------|
| | Demand Flows | | Cap. | Deg. Satn | Lane Util. | Average Delay | Level of Service | 95% Back of Queue | | Lane Config | Lane Length | Cap. Adj. | Prob. Block. |
| | Total | HV | | | | | | Veh | Dist | | | | |
| | veh/h | % | veh/h | v/c | % | sec | | | | | ft | % | % |
| SouthEast: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 476 | 1.0 | 998 | 0.477 | 100 | 9.2 | LOS A | 3.6 | 90.9 | Full | 360 | 0.0 | 0.0 |
| Approach | 476 | 1.0 | | 0.477 | | 9.2 | LOS A | 3.6 | 90.9 | | | | |
| North: North Lake Street | | | | | | | | | | | | | |
| Lane 1 ^d | 548 | 1.0 | 926 | 0.592 | 100 | 12.3 | LOS B | 5.8 | 145.2 | Full | 730 | 0.0 | 0.0 |
| Approach | 548 | 1.0 | | 0.592 | | 12.3 | LOS B | 5.8 | 145.2 | | | | |
| West: East Central Avenue | | | | | | | | | | | | | |
| Lane 1 ^d | 125 | 1.0 | 782 | 0.160 | 100 | 6.3 | LOS A | 1.0 | 26.1 | Full | 450 | 0.0 | 0.0 |
| Approach | 125 | 1.0 | | 0.160 | | 6.3 | LOS A | 1.0 | 26.1 | | | | |
| SouthWest: 4th Street | | | | | | | | | | | | | |
| Lane 1 ^d | 430 | 1.0 | 946 | 0.455 | 100 | 9.2 | LOS A | 3.3 | 83.5 | Full | 320 | 0.0 | 0.0 |
| Approach | 430 | 1.0 | | 0.455 | | 9.2 | LOS A | 3.3 | 83.5 | | | | |
| Intersection | 1580 | 1.0 | | 0.592 | | 10.1 | LOS B | 5.8 | 145.2 | | | | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

^d Dominant lane on roundabout approach

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Preliminary Opinion of Costs (Construction Costs Only)

4th Street/Lake Street/Central Avenue Intersection Improvements - **Roundabout Alternative**

City of Madera

1/2/2018

55-4549-03/2264

| No. | Item Description | Units | Quantity | Unit Cost | Total |
|-----|--|-------|----------|--------------|------------------------|
| 1 | Traffic Control System | LS | 1 | \$90,000.00 | \$90,000.00 |
| 2 | Remove Tree | EA | 5 | \$800.00 | \$4,000.00 |
| 3 | Remove Fence | LF | 220 | \$20.00 | \$4,400.00 |
| 4 | Remove Thermoplastic Traffic Stripe | LF | 570 | \$4.25 | \$2,422.50 |
| 5 | Remove Thermoplastic Pavement Marking | SQFT | 50 | \$12.50 | \$625.00 |
| 6 | Remove Roadside Sign | EA | 20 | \$155.00 | \$3,100.00 |
| 7 | Remove Concrete Curb | LF | 500 | \$19.50 | \$9,750.00 |
| 8 | Remove Concrete Sidewalk | SQYD | 560 | \$31.50 | \$17,640.00 |
| 9 | Remove Concrete (Curb & Gutter) | LF | 1900 | \$12.50 | \$23,750.00 |
| 10 | Roadway Excavation | CY | 2400 | \$32.00 | \$76,800.00 |
| 11 | Class 2 Aggregate Base | CY | 770 | \$53.00 | \$40,810.00 |
| 12 | Hot Mix Asphalt (Type B) | TON | 720 | \$90.00 | \$64,800.00 |
| 13 | Minor Concrete (Stamped Concrete -Truck Apron) | CY | 40 | \$690.00 | \$27,600.00 |
| 14 | Minor Concrete (Median Curb) | CY | 40 | \$770.00 | \$30,800.00 |
| 15 | Minor Concrete(Curb-Truck Apron) | CY | 10 | \$780.00 | \$7,800.00 |
| 16 | Minor Concrete (Curb and Gutter) | CY | 80 | \$355.00 | \$28,400.00 |
| 17 | Minor Concrete (Sidewalk) | CY | 140 | \$405.00 | \$56,700.00 |
| 18 | Thermoplastic Traffic Stripe | LF | 3800 | \$2.00 | \$7,600.00 |
| 19 | Thermoplastic Pavement Marking | SQFT | 640 | \$7.00 | \$4,480.00 |
| 20 | Landscape | SQFT | 20000 | \$5.00 | \$100,000.00 |
| 21 | Signs | EA | 30 | \$380.00 | \$11,400.00 |
| 22 | Lighting and Sign Illumination | LS | 1 | \$250,000.00 | \$250,000.00 |
| 23 | Storm Drain System | LS | 1 | \$50,000.00 | \$50,000.00 |
| 24 | Mobilization | LS | 1 | \$82,300.00 | \$82,300.00 |
| | Subtotal (Construction Costs) | | | | \$ 995,177.50 |
| | Minor/ Supplemental Items | | | 30% | \$ 299,000.00 |
| | Construction Contingency | | | 25% | \$ 324,000.00 |
| | Total Construction Costs | | | | \$ 1,618,177.50 |
| | Rounded | | | | \$ 1,620,000.00 |

APPENDIX D – BENEFIT/COST RATIO BACK-UP

| Intersection Control Evaluation Collision Cost Analysis and B/C | | | | | | | |
|--|------------------------------|--------------------------------|-----------------------------------|--------------------------------|---|-------------------------|-----------|
| -- Fill in tan boxes along with 'Area' -- | | | | | | | |
| County | Rte | Postmile | Location Description | | <div style="display: flex; justify-content: space-between;"> <div> Area <input type="radio"/> Rural <input checked="" type="radio"/> Suburban <input type="radio"/> Urban </div> <div> Intersection Types: F - Four-Legged M - Multi-Legged S - Offset-Tee Y - "Y" Wye Z - Others </div> </div> | | |
| Madera | N/A | N/A | 4th/Lake/Central | | | | |
| Existing Condition | | # of Years for Analysis | Rate Group | | | | |
| All Way Stop, Type F, M or S | | 23 | I8 | | | | |
| Existing ADT (x1000) | | Future ADT (x1000) | | | | | |
| Mainline | Cross St | Mainline | Cross St | Average ADT | VCF | | |
| 8.3 | 6.4 | 10.5 | 8.0 | 16.6 | 1.13 | | |
| Est. Capital Cost (x1000) for Desired Improvement | | | | Existing Collision Data | | | |
| Desired Improvement | Const | R/W | Total | Number of Years | 5 | Total Collisions | 10 |
| Yield Control (Roundabout 1-Lane) | \$ 1,620 | \$ 755 | \$ 2,375 | Injury | 1 | PDO | 9 |
| Yield Control (Roundabout 2-Lane) | | \$ - | \$ - | Fatal | | Fat + Inj | 1 |
| Traffic Signal, Type F, M or S | \$ 1,050 | \$ 2 | \$ 1,052 | | | | |
| | | | | | | | |
| Collision Cost (x1000) | | | | | | B/C | |
| | Existing Condition | | Desired Improvement | | Projected Savings | | |
| 1 | All Way Stop, Type F, M or S | \$6,973 | Yield Control (Roundabout 1-Lane) | \$2,330 | \$4,644 | 1.95 | |
| 2 | All Way Stop, Type F, M or S | \$6,973 | Yield Control (Roundabout 2-Lane) | \$3,450 | \$3,524 | 0.00 | |
| 3 | All Way Stop, Type F, M or S | \$6,973 | Traffic Signal, Type F, M or S | \$7,872 | (\$898) | -0.85 | |

v1.00

NOTE: Only average collision costs are used for calculation purposes.**NOTE: Collision costs reported are costs for anticipated collisions over the number of years of analysis (20 years)**

Fill in Orange Cells.

Delay Entry

Enter average vehicle occupancy. This is used to convert vehicle delay to person delay.

Vehicle Occupancy From Caltrans Life-Cycle Benefit-Cost Analysis - Economic Parameters 2016

Enter the duration in hours of each time period of the day. If delay data is not available for a time period, enter a duration of 0.

| Weekday | |
|-----------|--------------------------------|
| AM | <input type="text" value="1"/> |
| PM | <input type="text" value="1"/> |
| Midday | <input type="text"/> |
| Off-Peak1 | <input type="text"/> |
| Off-Peak2 | <input type="text"/> |
| Total | 2 |

| Weekend | |
|-----------|----------------------|
| AM | <input type="text"/> |
| PM | <input type="text"/> |
| Midday | <input type="text"/> |
| Off-Peak1 | <input type="text"/> |
| Off-Peak2 | <input type="text"/> |
| Total | 0 |

This could be used for analysis of certain time periods only.

This could be used for analysis of certain time periods only.

Total for weekday and weekend should equal 24 for analysis of all hours of the week, or should equal less than 24 for analysis of certain time periods only. Full day analysis for weekdays and weekends is recommended if sufficient data is available.

Enter the hourly volume (total entering vehicles) for each time period of the day. This is used to convert average delay per vehicle to person delay. If analysis of certain time periods is not desired, leave cells for that time period blank.

| | Weekday | |
|-----------|-----------------------------------|-----------------------------------|
| | Existing Year | Design Year |
| AM | <input type="text" value="955"/> | <input type="text" value="1203"/> |
| PM | <input type="text" value="1188"/> | <input type="text" value="1495"/> |
| Midday | <input type="text"/> | <input type="text"/> |
| Off-Peak1 | <input type="text"/> | <input type="text"/> |
| Off-Peak2 | <input type="text"/> | <input type="text"/> |

ADT **Requires 24** hour data

| | Weekend | |
|-----------|----------------------|----------------------|
| | Opening Year | Design Year |
| AM | <input type="text"/> | <input type="text"/> |
| PM | <input type="text"/> | <input type="text"/> |
| Midday | <input type="text"/> | <input type="text"/> |
| Off-Peak1 | <input type="text"/> | <input type="text"/> |
| Off-Peak2 | <input type="text"/> | <input type="text"/> |

ADT **Requires 24** hour data

Orange cells in tables below can be left blank if consideration of time period is not desired.
 For example, if it is desired to only analyze peak hours, delay entries for midday and off-peak may be left blank.

Enter the delay from SIDRA outputs.

Weekday

Roundabout Alternative

| | AM | PM | Midday | Off-Peak1 | Off-Peak2 |
|------|---------|---------|---------|-----------|-----------|
| | Delay | Delay | Delay | Delay | Delay |
| | sec/veh | sec/veh | sec/veh | sec/veh | sec/veh |
| 2017 | 7.4 | 7.3 | | | |
| 2040 | 10.3 | 10.1 | | | |

Enter the delay from Synchro/SimTraffic outputs.

Signal Alternative

| | AM | PM | Midday | Off-Peak1 | Off-Peak2 |
|------|---------|---------|---------|-----------|-----------|
| | Delay | Delay | Delay | Delay | Delay |
| | sec/veh | sec/veh | sec/veh | sec/veh | sec/veh |
| 2017 | 23.8 | 24.3 | | | |
| 2040 | 28.2 | 38.3 | | | |

These cells calculate average weekday peak hour totals. No data entry here.

Roundabout Alternative

| Average Week Day Peak Hour Totals | | |
|-----------------------------------|--------|--------------|
| Vehicle Delay | | Person Delay |
| (in sec) | | (in sec) |
| 2017 | 7,870 | 9,050 |
| 2040 | 13,745 | 15,807 |

Signal Alternative

| Average Week Day Peak Hour Totals | | |
|-----------------------------------|--------|--------------|
| Vehicle Delay | | Person Delay |
| (in sec) | | (in sec) |
| 2017 | 25,799 | 29,669 |
| 2040 | 45,592 | 52,430 |

| Annual Costs | | Roundabout Alternative | | Traffic Signal Alternative | |
|---|--|--|--------------|--|--------------|
| Safety | Predicted Fatal/Injury Crashes Predicted PDO Crashes | Predicted Annual Crashes | Safety Cost | Predicted Annual Crashes | Safety Cost |
| | | Safety Data Omitted | 0 | Safety Data Omitted | 0 |
| | | Safety Data Omitted | 0 | Safety Data Omitted | 0 |
| | | Annual Costs of Predicted Crashes | \$ 135,695 | Annual Costs of Predicted Crashes | \$ 202,062 |
| Delay | Average Annual Person (in Vehicle) Delay | Annual Intersection Delay (person-hrs) | Delay Cost | Annual Intersection Delay (person-hrs) | Delay Cost |
| | | 898 | \$ 11,000 | 2965 | \$ 36,000 |
| Operation and Maintenance | Annualized Cost of Signal Retiming Annual Cost of Power for Signal Annual Cost of Illumination Annual Cost of Maintenance | Operation and Maintenance | O&M Cost | Operation and Maintenance | O&M Cost |
| | | | \$ - | Signal Retiming Every 3 Years | \$ 1,000 |
| | | | \$ - | Power for Signal | \$ 750 |
| | | Intersection Illumination | \$ 750 | Intersection Illumination | \$ 750 |
| | | Landscaping Costs | \$ 1,500 | Signal Maintenance Costs (power outage, detection, etc.) | \$ 1,500 |
| | | Total Annual Operation and Maintenance Costs | \$ 2,250 | Total Annual Operation and Maintenance Costs | \$ 4,000 |
| Initial Capital Costs | | Total Capital Costs | Cost | Total Capital Costs | Cost |
| Preliminary Engineering Right-of-way and Utilities Construction | | | \$ 234,392 | | \$ 120,699 |
| | | | \$ 755,410 | | \$ 1,600 |
| | | | \$ 1,620,000 | | \$ 1,050,000 |
| | | | | | |

*Delay cost is based upon an average of the AM and PM peak hours.

| Total Discounted Life Cycle Costs (2017 - 2040) | | Roundabout Alternative | | Traffic Signal Alternative | |
|---|------------------------------------|--|--------------|--|--------------|
| Safety | | Total Predicted Crashes | Safety Cost | Total Predicted Crashes | Safety Cost |
| | Predicted Fatal/Injury Crashes | Safety Data Omitted | \$ - | Safety Data Omitted | \$ - |
| | Predicted PDO Crashes | Safety Data Omitted | \$ - | Safety Data Omitted | \$ - |
| | | Total Costs of Predicted Crashes | \$ 2,016,000 | Total Costs of Predicted Crashes | \$ 3,002,000 |
| Delay | | Total Intersection Delay (person-hrs) | Delay Cost | Total Intersection Delay (person-hrs) | Delay Cost |
| | Total Person (in Vehicle) Delay | 21543 | \$ 260,000 | 71152 | \$ 860,000 |
| Fuel and GHG Cost | | Fuel and Green House Gas Cost | | Fuel and Green House Gas Cost | |
| | | \$ 505,120 | | \$ 536,123 | |
| Operation and Maintenance | | Operation and Maintenance | O&M Cost | Operation and Maintenance | O&M Cost |
| | Annualized Cost of Signal Retiming | \$ - | | Signal Retiming Every 3 Years | \$ 14,857 |
| | Annual Cost of Power for Signal | \$ - | | Power for Signal | \$ 11,143 |
| | Annual Cost of Illumination | Intersection Illumination | \$ 11,143 | Intersection Illumination | \$ 11,143 |
| | Annual Cost of Maintenance | Landscaping Costs | \$ 22,285 | Signal Maintenance Costs (power outage, detection, etc.) | \$ 22,285 |
| | | Total Annual Operation and Maintenance Costs | \$ 33,428 | Total Annual Operation and Maintenance Costs | \$ 59,427 |
| Initial Capital Costs | | Total Capital Costs | Cost | Total Capital Costs | Cost |
| Preliminary Engineering Right-of-way and Utilities Construction | | | \$ 234,392 | | \$ 120,699 |
| | | | \$ 755,410 | | \$ 1,600 |
| | | | \$ 1,620,000 | | \$ 1,050,000 |
| | | Total Initial Capital Costs | \$ 2,609,802 | Total Initial Capital Costs | \$ 1,172,299 |
| Total Life Cycle Costs (Opening Year \$) | | Net Present Value | \$ 4,919,230 | Net Present Value | \$ 5,093,726 |

*Delay cost is based upon an average of the AM and PM peak hours.

Roundabout Alternative

Traffic Signal Alternative

| Life Cycle Benefit/Cost Ratio | |
|------------------------------------|--------------|
| Roundabout Alt vs. Signal Alt | |
| Safety Benefit | \$ 986,000 |
| Delay Reduction Benefit | \$ 600,000 |
| Fuel and GHG Benefit | \$ 31,004 |
| Total Benefits | \$ 1,617,004 |
| Added Operations&Maintenance Costs | \$ (25,999) |
| Added Capital Costs | \$ 1,437,503 |
| Total Costs | \$ 1,411,504 |
| Life Cycle Benefit/Cost Ratio | 1.1 |

Roundabout Preferred

| QUANTITIES | | | | | | | | | |
|---|--|--|------------------------|-------------------------|------------------------|------------------------|------------------------|-------|-------|
| Travel Time (pers-hr) Signal Roundabout Alternative Alternative | | Intersection Performance-Annual Values (From SIDRA Intersection Summary Reports) | | | | | | | |
| | | Fuel (gal/yr) | | Carbon Monoxide (kg/yr) | | Nitrogen Oxide (kg/yr) | | | |
| | | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | | |
| | | 2,143 | 654 | 7,741 | 7,319 | 66.5 | 63.5 | 93.0 | 86.5 |
| | | 3,787 | 1,142 | 12,611 | 11,883 | 118.5 | 116.0 | 132.0 | 131.5 |
| 2017 | | | | 0.07 | 0.07 | 0.10 | 0.10 | | |
| 2040 | | | Convert to tons/yr | 0.13 | 0.13 | 0.15 | 0.14 | | |

| | | Travel Time (pers-hr) | | Fuel (gal/yr) | | Carbon Monoxide (ton/yr) | | Nitrogen Oxide (kg/yr) | |
|---------|------|-----------------------|------------------------|--------------------|------------------------|--------------------------|------------------------|------------------------|------------------------|
| | | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative |
| Year 0 | 2017 | 2143 | 654 | 7741.00 | 7319.00 | 0.07 | 0.07 | 0.10 | 0.10 |
| Year 1 | 2018 | 2214 | 675 | 7952.74 | 7517.43 | 0.08 | 0.07 | 0.10 | 0.10 |
| Year 2 | 2019 | 2286 | 696 | 8164.48 | 7715.87 | 0.08 | 0.08 | 0.11 | 0.10 |
| Year 3 | 2020 | 2357 | 717 | 8376.22 | 7914.30 | 0.08 | 0.08 | 0.11 | 0.10 |
| Year 4 | 2021 | 2429 | 738 | 8587.96 | 8112.74 | 0.08 | 0.08 | 0.11 | 0.10 |
| Year 5 | 2022 | 2500 | 760 | 8799.70 | 8311.17 | 0.09 | 0.08 | 0.11 | 0.11 |
| Year 6 | 2023 | 2572 | 781 | 9011.43 | 8509.61 | 0.09 | 0.09 | 0.11 | 0.11 |
| Year 7 | 2024 | 2643 | 802 | 9223.17 | 8708.04 | 0.09 | 0.09 | 0.12 | 0.11 |
| Year 8 | 2025 | 2715 | 823 | 9434.91 | 8906.48 | 0.09 | 0.09 | 0.12 | 0.11 |
| Year 9 | 2026 | 2786 | 845 | 9646.65 | 9104.91 | 0.10 | 0.09 | 0.12 | 0.11 |
| Year 10 | 2027 | 2857 | 866 | 9858.39 | 9303.35 | 0.10 | 0.10 | 0.12 | 0.12 |
| Year 11 | 2028 | 2929 | 887 | 10070.13 | 9501.78 | 0.10 | 0.10 | 0.12 | 0.12 |
| Year 12 | 2029 | 3000 | 908 | 10281.87 | 9700.22 | 0.10 | 0.10 | 0.12 | 0.12 |
| Year 13 | 2030 | 3072 | 929 | 10493.61 | 9898.65 | 0.11 | 0.10 | 0.13 | 0.12 |
| Year 14 | 2031 | 3143 | 951 | 10705.35 | 10097.09 | 0.11 | 0.11 | 0.13 | 0.13 |
| Year 15 | 2032 | 3215 | 972 | 10917.09 | 10295.52 | 0.11 | 0.11 | 0.13 | 0.13 |
| Year 16 | 2033 | 3286 | 993 | 11128.83 | 10493.96 | 0.11 | 0.11 | 0.13 | 0.13 |
| Year 17 | 2034 | 3358 | 1014 | 11340.57 | 10692.39 | 0.12 | 0.11 | 0.13 | 0.13 |
| Year 18 | 2035 | 3429 | 1036 | 11552.30 | 10890.83 | 0.12 | 0.12 | 0.14 | 0.13 |
| Year 19 | 2036 | 3501 | 1057 | 11764.04 | 11089.26 | 0.12 | 0.12 | 0.14 | 0.14 |
| Year 20 | 2037 | 3572 | 1078 | 11975.78 | 11287.70 | 0.12 | 0.12 | 0.14 | 0.14 |
| Year 21 | 2038 | 3644 | 1099 | 12187.52 | 11486.13 | 0.13 | 0.12 | 0.14 | 0.14 |
| Year 22 | 2039 | 3715 | 1120 | 12399.26 | 11684.57 | 0.13 | 0.13 | 0.14 | 0.14 |
| Year 23 | 2040 | 3787 | 1142 | 12611.00 | 11883.00 | 0.13 | 0.13 | 0.15 | 0.14 |
| Total | | 71152 | 21543 | 244224.00 | 230424.00 | 2.45 | 2.37 | 2.98 | 2.88 |
| Average | | 2965 | 898 | 10176.00 | 9601.00 | 0.10 | 0.10 | 0.12 | 0.12 |

| COSTS | | | |
|---|--|-------------------------|------------------------|
| Life-Cycle Benefit-Cost Analysis | | | |
| Travel Time Parameter | Fuel (gal/yr) | Carbon Monoxide (kg/yr) | Nitrogen Oxide (kg/yr) |
| Auto/Truck Composite (Weighted Average) | Average Fuel Price for Regular Unleaded (Auto) | CA Urban Area | CA Urban Area |
| (\$/per-hr) | (\$/Gal) | (\$/Ton) | (\$/Ton) |
| \$18.95 | \$3.18 | \$80.00 | \$18,700.00 |

| Travel Time (pers-hr) | | Fuel (gal/yr) | | Carbon Monoxide (ton/yr) | | Nitrogen Oxide (kg/yr) | |
|-----------------------|------------------------|--------------------|------------------------|--------------------------|------------------------|------------------------|------------------------|
| Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative |
| \$40,605 | \$12,386 | \$24,616 | \$23,274 | \$6 | \$6 | \$1,917 | \$1,783 |
| \$41,959 | \$12,788 | \$25,290 | \$23,905 | \$6 | \$6 | \$1,952 | \$1,823 |
| \$43,314 | \$13,190 | \$25,963 | \$24,536 | \$6 | \$6 | \$1,987 | \$1,864 |
| \$44,668 | \$13,592 | \$26,636 | \$25,167 | \$6 | \$6 | \$2,022 | \$1,904 |
| \$46,022 | \$13,994 | \$27,310 | \$25,799 | \$7 | \$6 | \$2,057 | \$1,944 |
| \$47,377 | \$14,396 | \$27,983 | \$26,430 | \$7 | \$7 | \$2,092 | \$1,985 |
| \$48,731 | \$14,799 | \$28,656 | \$27,061 | \$7 | \$7 | \$2,127 | \$2,025 |
| \$50,086 | \$15,201 | \$29,330 | \$27,692 | \$7 | \$7 | \$2,162 | \$2,065 |
| \$51,440 | \$15,603 | \$30,003 | \$28,323 | \$7 | \$7 | \$2,197 | \$2,106 |
| \$52,795 | \$16,005 | \$30,676 | \$28,954 | \$8 | \$7 | \$2,232 | \$2,146 |
| \$54,149 | \$16,407 | \$31,350 | \$29,585 | \$8 | \$8 | \$2,267 | \$2,186 |
| \$55,503 | \$16,809 | \$32,023 | \$30,216 | \$8 | \$8 | \$2,302 | \$2,227 |
| \$56,858 | \$17,211 | \$32,696 | \$30,847 | \$8 | \$8 | \$2,336 | \$2,267 |
| \$58,212 | \$17,613 | \$33,370 | \$31,478 | \$8 | \$8 | \$2,371 | \$2,307 |
| \$59,567 | \$18,015 | \$34,043 | \$32,109 | \$9 | \$8 | \$2,406 | \$2,348 |
| \$60,921 | \$18,417 | \$34,716 | \$32,740 | \$9 | \$9 | \$2,441 | \$2,388 |
| \$62,276 | \$18,819 | \$35,390 | \$33,371 | \$9 | \$9 | \$2,476 | \$2,428 |
| \$63,630 | \$19,221 | \$36,063 | \$34,002 | \$9 | \$9 | \$2,511 | \$2,469 |
| \$64,984 | \$19,623 | \$36,736 | \$34,633 | \$9 | \$9 | \$2,546 | \$2,509 |
| \$66,339 | \$20,025 | \$37,410 | \$35,264 | \$10 | \$9 | \$2,581 | \$2,549 |
| \$67,693 | \$20,427 | \$38,083 | \$35,895 | \$10 | \$10 | \$2,616 | \$2,590 |
| \$69,048 | \$20,829 | \$38,756 | \$36,526 | \$10 | \$10 | \$2,651 | \$2,630 |
| \$70,402 | \$21,232 | \$39,430 | \$37,157 | \$10 | \$10 | \$2,686 | \$2,670 |
| \$71,757 | \$21,634 | \$40,103 | \$37,788 | \$10 | \$10 | \$2,721 | \$2,711 |
| \$1,348,336 | \$408,237 | \$ 776,632 | \$ 732,748 | \$ 196 | \$ 190 | \$ 55,656 | \$ 53,924 |
| \$56,181 | \$17,010 | \$32,360 | \$30,531 | \$8 | \$8 | \$2,319 | \$2,247 |

0 1.00000
1 0.96154
2 0.92456
3 0.88900
4 0.85480
5 0.82193
6 0.79031
7 0.75992
8 0.73069
9 0.70259
10 0.67556
11 0.64958
12 0.62460
13 0.60057
14 0.57748
15 0.55526
16 0.53391
17 0.51337
18 0.49363
19 0.47464
20 0.45639
21 0.43883
22 0.42196
23 0.40573

ADJUSTED COSTS

Average Yearly Costs

| Travel Time (pers-hr) | | Fuel (gal/yr) | | Carbon Monoxide (ton/yr) | | Nitrogen Oxide (kg/yr) | |
|-----------------------|------------------------|--------------------|------------------------|--------------------------|------------------------|------------------------|------------------------|
| Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative |
| \$36,000 | \$11,000 | \$21,000 | \$20,000 | \$5 | \$5 | \$1,500 | \$1,500 |

Environmental Costs

| | |
|------------------------|---------|
| Signal Alternative | \$1,505 |
| Roundabout Alternative | \$1,505 |

| Travel Time (pers-hr) | | Fuel (gal/yr) | | Carbon Monoxide (ton/yr) | | Nitrogen Oxide (kg/yr) | |
|-----------------------|------------------------|--------------------|------------------------|--------------------------|------------------------|------------------------|------------------------|
| Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative | Signal Alternative | Roundabout Alternative |
| \$40,605 | \$12,386 | \$24,616 | \$23,274 | \$6 | \$6 | \$1,917 | \$1,783 |
| \$40,345 | \$12,296 | \$24,317 | \$22,986 | \$6 | \$6 | \$1,877 | \$1,753 |
| \$40,046 | \$12,195 | \$24,004 | \$22,685 | \$6 | \$6 | \$1,837 | \$1,723 |
| \$39,710 | \$12,084 | \$23,680 | \$22,374 | \$6 | \$6 | \$1,797 | \$1,693 |
| \$39,340 | \$11,962 | \$23,344 | \$22,053 | \$6 | \$5 | \$1,758 | \$1,662 |
| \$38,940 | \$11,833 | \$23,000 | \$21,723 | \$6 | \$5 | \$1,719 | \$1,631 |
| \$38,513 | \$11,695 | \$22,648 | \$21,386 | \$6 | \$5 | \$1,681 | \$1,600 |
| \$38,061 | \$11,551 | \$22,288 | \$21,043 | \$6 | \$5 | \$1,643 | \$1,569 |
| \$37,587 | \$11,401 | \$21,923 | \$20,695 | \$5 | \$5 | \$1,605 | \$1,539 |
| \$37,093 | \$11,245 | \$21,553 | \$20,342 | \$5 | \$5 | \$1,568 | \$1,508 |
| \$36,581 | \$11,084 | \$21,179 | \$19,986 | \$5 | \$5 | \$1,531 | \$1,477 |
| \$36,054 | \$10,919 | \$20,802 | \$19,628 | \$5 | \$5 | \$1,495 | \$1,446 |
| \$35,513 | \$10,750 | \$20,422 | \$19,267 | \$5 | \$5 | \$1,459 | \$1,416 |
| \$34,961 | \$10,578 | \$20,041 | \$18,905 | \$5 | \$5 | \$1,424 | \$1,386 |
| \$34,398 | \$10,403 | \$19,659 | \$18,542 | \$5 | \$5 | \$1,390 | \$1,356 |
| \$33,827 | \$10,226 | \$19,277 | \$18,179 | \$5 | \$5 | \$1,356 | \$1,326 |
| \$33,249 | \$10,048 | \$18,895 | \$17,817 | \$5 | \$5 | \$1,322 | \$1,297 |
| \$32,666 | \$9,868 | \$18,514 | \$17,456 | \$5 | \$5 | \$1,289 | \$1,267 |
| \$32,078 | \$9,687 | \$18,134 | \$17,096 | \$5 | \$5 | \$1,257 | \$1,239 |
| \$31,487 | \$9,505 | \$17,756 | \$16,738 | \$5 | \$4 | \$1,225 | \$1,210 |
| \$30,894 | \$9,323 | \$17,381 | \$16,382 | \$4 | \$4 | \$1,194 | \$1,182 |
| \$30,300 | \$9,141 | \$17,008 | \$16,029 | \$4 | \$4 | \$1,163 | \$1,154 |
| \$29,707 | \$8,959 | \$16,638 | \$15,679 | \$4 | \$4 | \$1,133 | \$1,127 |
| \$29,114 | \$8,777 | \$16,271 | \$15,332 | \$4 | \$4 | \$1,104 | \$1,100 |
| \$860,000 | \$260,000 | \$ 500,000 | \$ 470,000 | \$ 123 | \$ 120 | \$ 36,000 | \$ 35,000 |
| \$36,000 | \$11,000 | \$21,000 | \$20,000 | \$5 | \$5 | \$1,500 | \$1,500 |

Roundabout Alternative to Signal Alternative

| Life Cycle Costs (20 year design) | Traffic Signal Alternative | Roundabout Alternative |
|---|----------------------------|------------------------|
| Collision and Mobility Costs | | |
| Collision Costs of predicted crashes | \$3,002,000 | \$2,016,000 |
| Delay Costs | \$860,000 | \$260,000 |
| Fuel and GHG Costs | \$537,000 | \$506,000 |
| Project Costs including design, construction and maintenance | | |
| Operations and Maintenance Costs | \$60,000 | \$34,000 |
| Project Costs (including R/W) | \$1,172,299 | \$2,609,802 |
| | | |
| Total Life Cycle Costs (Opening Year \$ - Net Present Value) | \$5,631,299 | \$5,425,802 |

INTERSECTION SUMMARY

 **Site: 1v [2017 AM Peak Hour - Conversion]**

4th Street/Lake Street/Central Avenue

2017 AM Peak Hour

Signals - Pretimed Isolated Cycle Time = 50 seconds (User-Given Cycle Time)

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 15.0 mph | 15.0 mph |
| Travel Distance (Total) | 229.3 veh-mi/h | 275.1 pers-mi/h |
| Travel Time (Total) | 15.3 veh-h/h | 18.3 pers-h/h |
| Demand Flows (Total) | 1165 veh/h | 1399 pers/h |
| Percent Heavy Vehicles (Demand) | 4.0 % | |
| Degree of Saturation | 0.682 | |
| Practical Spare Capacity | 31.9 % | |
| Effective Intersection Capacity | 1708 veh/h | |
| Control Delay (Total) | 6.82 veh-h/h | 8.19 pers-h/h |
| Control Delay (Average) | 21.1 sec | 21.1 sec |
| Control Delay (Worst Lane) | 27.2 sec | |
| Control Delay (Worst Movement) | 27.2 sec | 27.2 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 21.1 sec | |
| Idling Time (Average) | 16.8 sec | |
| Intersection Level of Service (LOS) | LOS C | |
| 95% Back of Queue - Vehicles (Worst Lane) | 7.5 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 192.8 ft | |
| Queue Storage Ratio (Worst Lane) | 0.23 | |
| Total Effective Stops | 930 veh/h | 1116 pers/h |
| Effective Stop Rate | 0.80 per veh | 0.80 per pers |
| Proportion Queued | 0.95 | 0.95 |
| Performance Index | 76.8 | 76.8 |
| Cost (Total) | 280.89 \$/h | 280.89 \$/h |
| Fuel Consumption (Total) | 17.0 gal/h | |
| Carbon Dioxide (Total) | 152.3 kg/h | |
| Hydrocarbons (Total) | 0.015 kg/h | |
| Carbon Monoxide (Total) | 0.147 kg/h | |
| NOx (Total) | 0.280 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 559,407 veh/y | 671,289 pers/y |
| Delay | 3,274 veh-h/y | 3,929 pers-h/y |
| Effective Stops | 446,557 veh/y | 535,868 pers/y |
| Travel Distance | 110,045 veh-mi/y | 132,054 pers-mi/y |
| Travel Time | 7,327 veh-h/y | 8,793 pers-h/y |
| Cost | 134,828 \$/y | 134,828 \$/y |
| Fuel Consumption | 8,153 gal/y | |
| Carbon Dioxide | 73,080 kg/y | |
| Hydrocarbons | 7 kg/y | |
| Carbon Monoxide | 70 kg/y | |
| NOx | 134 kg/y | |

INTERSECTION SUMMARY

 **Site: 1v [2017 PM Peak Hour - Conversion]**

4th Street/Lake Street/Central Avenue

2017 PM Peak Hour

Signals - Pretimed Isolated Cycle Time = 55 seconds (User-Given Cycle Time)

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 14.8 mph | 14.8 mph |
| Travel Distance (Total) | 230.1 veh-mi/h | 276.1 pers-mi/h |
| Travel Time (Total) | 15.5 veh-h/h | 18.6 pers-h/h |
| Demand Flows (Total) | 1156 veh/h | 1387 pers/h |
| Percent Heavy Vehicles (Demand) | 1.0 % | |
| Degree of Saturation | 0.658 | |
| Practical Spare Capacity | 36.9 % | |
| Effective Intersection Capacity | 1758 veh/h | |
| Control Delay (Total) | 7.18 veh-h/h | 8.62 pers-h/h |
| Control Delay (Average) | 22.4 sec | 22.4 sec |
| Control Delay (Worst Lane) | 24.4 sec | |
| Control Delay (Worst Movement) | 24.4 sec | 24.4 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 22.4 sec | |
| Idling Time (Average) | 18.2 sec | |
| Intersection Level of Service (LOS) | LOS C | |
| 95% Back of Queue - Vehicles (Worst Lane) | 7.4 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 185.9 ft | |
| Queue Storage Ratio (Worst Lane) | 0.32 | |
| Total Effective Stops | 910 veh/h | 1092 pers/h |
| Effective Stop Rate | 0.79 per veh | 0.79 per pers |
| Proportion Queued | 0.95 | 0.95 |
| Performance Index | 79.7 | 79.7 |
| Cost (Total) | 267.60 \$/h | 267.60 \$/h |
| Fuel Consumption (Total) | 15.3 gal/h | |
| Carbon Dioxide (Total) | 136.1 kg/h | |
| Hydrocarbons (Total) | 0.013 kg/h | |
| Carbon Monoxide (Total) | 0.130 kg/h | |
| NOx (Total) | 0.108 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 554,939 veh/y | 665,927 pers/y |
| Delay | 3,448 veh-h/y | 4,138 pers-h/y |
| Effective Stops | 436,731 veh/y | 524,078 pers/y |
| Travel Distance | 110,447 veh-mi/y | 132,536 pers-mi/y |
| Travel Time | 7,457 veh-h/y | 8,949 pers-h/y |
| Cost | 128,447 \$/y | 128,447 \$/y |
| Fuel Consumption | 7,328 gal/y | |
| Carbon Dioxide | 65,329 kg/y | |
| Hydrocarbons | 6 kg/y | |
| Carbon Monoxide | 63 kg/y | |
| NOx | 52 kg/y | |

INTERSECTION SUMMARY

 **Site: 1 [2017 AM Peak Hour]**

4th Street/Lake Street/Central Avenue
2017 AM Peak Hour
Roundabout

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 23.1 mph | 23.1 mph |
| Travel Distance (Total) | 243.6 veh-mi/h | 292.3 pers-mi/h |
| Travel Time (Total) | 10.5 veh-h/h | 12.7 pers-h/h |
| Demand Flows (Total) | 1164 veh/h | 1397 pers/h |
| Percent Heavy Vehicles (Demand) | 4.0 % | |
| Degree of Saturation | 0.385 | |
| Practical Spare Capacity | 120.8 % | |
| Effective Intersection Capacity | 3023 veh/h | |
| Control Delay (Total) | 1.96 veh-h/h | 2.36 pers-h/h |
| Control Delay (Average) | 6.1 sec | 6.1 sec |
| Control Delay (Worst Lane) | 6.5 sec | |
| Control Delay (Worst Movement) | 6.5 sec | 6.5 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 6.1 sec | |
| Idling Time (Average) | 4.1 sec | |
| Intersection Level of Service (LOS) | LOS A | |
| 95% Back of Queue - Vehicles (Worst Lane) | 3.0 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 77.4 ft | |
| Queue Storage Ratio (Worst Lane) | 0.06 | |
| Total Effective Stops | 327 veh/h | 392 pers/h |
| Effective Stop Rate | 0.28 per veh | 0.28 per pers |
| Proportion Queued | 0.44 | 0.44 |
| Performance Index | 27.2 | 27.2 |
| Cost (Total) | 218.18 \$/h | 218.18 \$/h |
| Fuel Consumption (Total) | 15.6 gal/h | |
| Carbon Dioxide (Total) | 140.1 kg/h | |
| Hydrocarbons (Total) | 0.013 kg/h | |
| Carbon Monoxide (Total) | 0.135 kg/h | |
| NOx (Total) | 0.255 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 558,815 veh/y | 670,578 pers/y |
| Delay | 943 veh-h/y | 1,132 pers-h/y |
| Effective Stops | 156,735 veh/y | 188,082 pers/y |
| Travel Distance | 116,907 veh-mi/y | 140,288 pers-mi/y |
| Travel Time | 5,062 veh-h/y | 6,074 pers-h/y |
| Cost | 104,727 \$/y | 104,727 \$/y |
| Fuel Consumption | 7,499 gal/y | |
| Carbon Dioxide | 67,232 kg/y | |
| Hydrocarbons | 6 kg/y | |
| Carbon Monoxide | 65 kg/y | |

NOx

122 kg/y

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INTERSECTION SUMMARY

Site: 1 [2017 PM Peak Hour]

4th Street/Lake Street/Central Avenue
2017 PM Peak Hour
Roundabout

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 23.2 mph | 23.2 mph |
| Travel Distance (Total) | 258.1 veh-mi/h | 309.7 pers-mi/h |
| Travel Time (Total) | 11.1 veh-h/h | 13.3 pers-h/h |
| Demand Flows (Total) | 1218 veh/h | 1462 pers/h |
| Percent Heavy Vehicles (Demand) | 1.0 % | |
| Degree of Saturation | 0.353 | |
| Practical Spare Capacity | 140.7 % | |
| Effective Intersection Capacity | 3450 veh/h | |
| Control Delay (Total) | 2.07 veh-h/h | 2.48 pers-h/h |
| Control Delay (Average) | 6.1 sec | 6.1 sec |
| Control Delay (Worst Lane) | 6.9 sec | |
| Control Delay (Worst Movement) | 6.9 sec | 6.9 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 6.1 sec | |
| Idling Time (Average) | 4.0 sec | |
| Intersection Level of Service (LOS) | LOS A | |
| 95% Back of Queue - Vehicles (Worst Lane) | 2.4 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 59.3 ft | |
| Queue Storage Ratio (Worst Lane) | 0.07 | |
| Total Effective Stops | 390 veh/h | 468 pers/h |
| Effective Stop Rate | 0.32 per veh | 0.32 per pers |
| Proportion Queued | 0.48 | 0.48 |
| Performance Index | 28.6 | 28.6 |
| Cost (Total) | 216.00 \$/h | 216.00 \$/h |
| Fuel Consumption (Total) | 14.9 gal/h | |
| Carbon Dioxide (Total) | 132.6 kg/h | |
| Hydrocarbons (Total) | 0.012 kg/h | |
| Carbon Monoxide (Total) | 0.130 kg/h | |
| NOx (Total) | 0.107 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 584,774 veh/y | 701,729 pers/y |
| Delay | 992 veh-h/y | 1,191 pers-h/y |
| Effective Stops | 187,234 veh/y | 224,681 pers/y |
| Travel Distance | 123,875 veh-mi/y | 148,650 pers-mi/y |
| Travel Time | 5,335 veh-h/y | 6,402 pers-h/y |
| Cost | 103,682 \$/y | 103,682 \$/y |
| Fuel Consumption | 7,139 gal/y | |
| Carbon Dioxide | 63,648 kg/y | |
| Hydrocarbons | 6 kg/y | |
| Carbon Monoxide | 62 kg/y | |

NOx

51 kg/y

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INTERSECTION SUMMARY

 **Site: 1v [2040 AM Peak Hour - Conversion]**

4th Street/Lake Street/Central Avenue

2040 AM Peak Hour

Signals - Pretimed Isolated Cycle Time = 50 seconds (User-Given Cycle Time)

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 11.9 mph | 11.9 mph |
| Travel Distance (Total) | 276.3 veh-mi/h | 331.6 pers-mi/h |
| Travel Time (Total) | 23.2 veh-h/h | 27.8 pers-h/h |
| Demand Flows (Total) | 1464 veh/h | 1757 pers/h |
| Percent Heavy Vehicles (Demand) | 4.0 % | |
| Degree of Saturation | 0.891 | |
| Practical Spare Capacity | 1.0 % | |
| Effective Intersection Capacity | 1643 veh/h | |
| Control Delay (Total) | 12.84 veh-h/h | 15.41 pers-h/h |
| Control Delay (Average) | 31.6 sec | 31.6 sec |
| Control Delay (Worst Lane) | 50.2 sec | |
| Control Delay (Worst Movement) | 50.2 sec | 50.2 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 31.6 sec | |
| Idling Time (Average) | 26.0 sec | |
| Intersection Level of Service (LOS) | LOS C | |
| 95% Back of Queue - Vehicles (Worst Lane) | 11.3 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 291.1 ft | |
| Queue Storage Ratio (Worst Lane) | 0.38 | |
| Total Effective Stops | 1332 veh/h | 1598 pers/h |
| Effective Stop Rate | 0.91 per veh | 0.91 per pers |
| Proportion Queued | 0.98 | 0.98 |
| Performance Index | 112.3 | 112.3 |
| Cost (Total) | 445.08 \$/h | 445.08 \$/h |
| Fuel Consumption (Total) | 25.5 gal/h | |
| Carbon Dioxide (Total) | 228.4 kg/h | |
| Hydrocarbons (Total) | 0.024 kg/h | |
| Carbon Monoxide (Total) | 0.242 kg/h | |
| NOx (Total) | 0.378 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 702,815 veh/y | 843,378 pers/y |
| Delay | 6,165 veh-h/y | 7,398 pers-h/y |
| Effective Stops | 639,207 veh/y | 767,049 pers/y |
| Travel Distance | 132,642 veh-mi/y | 159,170 pers-mi/y |
| Travel Time | 11,115 veh-h/y | 13,338 pers-h/y |
| Cost | 213,639 \$/y | 213,639 \$/y |
| Fuel Consumption | 12,239 gal/y | |
| Carbon Dioxide | 109,625 kg/y | |
| Hydrocarbons | 12 kg/y | |
| Carbon Monoxide | 116 kg/y | |
| NOx | 181 kg/y | |

INTERSECTION SUMMARY

 **Site: 1v [2040 PM Peak Hour - Conversion]**

4th Street/Lake Street/Central Avenue

2040 PM Peak Hour

Signals - Actuated Isolated Cycle Time = 75 seconds (User-Given Phase Times)

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 9.8 mph | 9.8 mph |
| Travel Distance (Total) | 302.7 veh-mi/h | 363.3 pers-mi/h |
| Travel Time (Total) | 30.8 veh-h/h | 37.0 pers-h/h |
| Demand Flows (Total) | 1597 veh/h | 1916 pers/h |
| Percent Heavy Vehicles (Demand) | 1.0 % | |
| Degree of Saturation | 0.813 | |
| Practical Spare Capacity | 10.7 % | |
| Effective Intersection Capacity | 1964 veh/h | |
| Control Delay (Total) | 19.71 veh-h/h | 23.65 pers-h/h |
| Control Delay (Average) | 44.4 sec | 44.4 sec |
| Control Delay (Worst Lane) | 55.1 sec | |
| Control Delay (Worst Movement) | 55.1 sec | 55.1 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 44.4 sec | |
| Idling Time (Average) | 40.6 sec | |
| Intersection Level of Service (LOS) | LOS D | |
| 95% Back of Queue - Vehicles (Worst Lane) | 14.9 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 376.0 ft | |
| Queue Storage Ratio (Worst Lane) | 0.64 | |
| Total Effective Stops | 1270 veh/h | 1524 pers/h |
| Effective Stop Rate | 0.80 per veh | 0.80 per pers |
| Proportion Queued | 0.95 | 0.95 |
| Performance Index | 160.7 | 160.7 |
| Cost (Total) | 540.71 \$/h | 540.71 \$/h |
| Fuel Consumption (Total) | 27.0 gal/h | |
| Carbon Dioxide (Total) | 241.0 kg/h | |
| Hydrocarbons (Total) | 0.026 kg/h | |
| Carbon Monoxide (Total) | 0.251 kg/h | |
| NOx (Total) | 0.172 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 766,435 veh/y | 919,722 pers/y |
| Delay | 9,460 veh-h/y | 11,352 pers-h/y |
| Effective Stops | 609,616 veh/y | 731,539 pers/y |
| Travel Distance | 145,314 veh-mi/y | 174,377 pers-mi/y |
| Travel Time | 14,795 veh-h/y | 17,754 pers-h/y |
| Cost | 259,540 \$/y | 259,540 \$/y |
| Fuel Consumption | 12,982 gal/y | |
| Carbon Dioxide | 115,694 kg/y | |
| Hydrocarbons | 12 kg/y | |
| Carbon Monoxide | 121 kg/y | |
| NOx | 83 kg/y | |

INTERSECTION SUMMARY

 **Site: 1 [2040 AM Peak Hour]**

4th Street/Lake Street/Central Avenue
2040 AM Peak Hour
Roundabout

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 19.3 mph | 19.3 mph |
| Travel Distance (Total) | 297.7 veh-mi/h | 357.2 pers-mi/h |
| Travel Time (Total) | 15.4 veh-h/h | 18.5 pers-h/h |
| Demand Flows (Total) | 1464 veh/h | 1757 pers/h |
| Percent Heavy Vehicles (Demand) | 4.0 % | |
| Degree of Saturation | 0.658 | |
| Practical Spare Capacity | 29.2 % | |
| Effective Intersection Capacity | 2225 veh/h | |
| Control Delay (Total) | 4.21 veh-h/h | 5.05 pers-h/h |
| Control Delay (Average) | 10.3 sec | 10.3 sec |
| Control Delay (Worst Lane) | 13.6 sec | |
| Control Delay (Worst Movement) | 13.6 sec | 13.6 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 10.3 sec | |
| Idling Time (Average) | 6.2 sec | |
| Intersection Level of Service (LOS) | LOS B | |
| 95% Back of Queue - Vehicles (Worst Lane) | 9.1 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 235.6 ft | |
| Queue Storage Ratio (Worst Lane) | 0.13 | |
| Total Effective Stops | 950 veh/h | 1141 pers/h |
| Effective Stop Rate | 0.65 per veh | 0.65 per pers |
| Proportion Queued | 0.73 | 0.73 |
| Performance Index | 53.8 | 53.8 |
| Cost (Total) | 347.98 \$/h | 347.98 \$/h |
| Fuel Consumption (Total) | 24.6 gal/h | |
| Carbon Dioxide (Total) | 219.9 kg/h | |
| Hydrocarbons (Total) | 0.022 kg/h | |
| Carbon Monoxide (Total) | 0.237 kg/h | |
| NOx (Total) | 0.372 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 702,815 veh/y | 843,378 pers/y |
| Delay | 2,019 veh-h/y | 2,423 pers-h/y |
| Effective Stops | 456,215 veh/y | 547,458 pers/y |
| Travel Distance | 142,897 veh-mi/y | 171,476 pers-mi/y |
| Travel Time | 7,404 veh-h/y | 8,885 pers-h/y |
| Cost | 167,029 \$/y | 167,029 \$/y |
| Fuel Consumption | 11,785 gal/y | |
| Carbon Dioxide | 105,567 kg/y | |
| Hydrocarbons | 11 kg/y | |
| Carbon Monoxide | 114 kg/y | |

NOx

179 kg/y

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INTERSECTION SUMMARY

 **Site: 1 [2040 PM Peak Hour]**

4th Street/Lake Street/Central Avenue
2040 PM Peak Hour
Roundabout

| Intersection Performance - Hourly Values | | |
|---|----------------|-----------------|
| Performance Measure | Vehicles | Persons |
| Travel Speed (Average) | 19.3 mph | 19.3 mph |
| Travel Distance (Total) | 327.6 veh-mi/h | 393.2 pers-mi/h |
| Travel Time (Total) | 16.9 veh-h/h | 20.3 pers-h/h |
| Demand Flows (Total) | 1597 veh/h | 1916 pers/h |
| Percent Heavy Vehicles (Demand) | 1.0 % | |
| Degree of Saturation | 0.602 | |
| Practical Spare Capacity | 41.3 % | |
| Effective Intersection Capacity | 2654 veh/h | |
| Control Delay (Total) | 4.56 veh-h/h | 5.47 pers-h/h |
| Control Delay (Average) | 10.3 sec | 10.3 sec |
| Control Delay (Worst Lane) | 12.6 sec | |
| Control Delay (Worst Movement) | 12.6 sec | 12.6 sec |
| Geometric Delay (Average) | 0.0 sec | |
| Stop-Line Delay (Average) | 10.3 sec | |
| Idling Time (Average) | 6.4 sec | |
| Intersection Level of Service (LOS) | LOS B | |
| 95% Back of Queue - Vehicles (Worst Lane) | 6.9 veh | |
| 95% Back of Queue - Distance (Worst Lane) | 175.1 ft | |
| Queue Storage Ratio (Worst Lane) | 0.11 | |
| Total Effective Stops | 1065 veh/h | 1278 pers/h |
| Effective Stop Rate | 0.67 per veh | 0.67 per pers |
| Proportion Queued | 0.75 | 0.75 |
| Performance Index | 55.1 | 55.1 |
| Cost (Total) | 368.43 \$/h | 368.43 \$/h |
| Fuel Consumption (Total) | 25.0 gal/h | |
| Carbon Dioxide (Total) | 222.5 kg/h | |
| Hydrocarbons (Total) | 0.023 kg/h | |
| Carbon Monoxide (Total) | 0.245 kg/h | |
| NOx (Total) | 0.176 kg/h | |

Site Level of Service (LOS) Method: Delay & v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Intersection LOS value for Vehicles is based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

| Intersection Performance - Annual Values | | |
|--|------------------|-------------------|
| Performance Measure | Vehicles | Persons |
| Demand Flows (Total) | 766,435 veh/y | 919,722 pers/y |
| Delay | 2,187 veh-h/y | 2,624 pers-h/y |
| Effective Stops | 511,127 veh/y | 613,352 pers/y |
| Travel Distance | 157,271 veh-mi/y | 188,725 pers-mi/y |
| Travel Time | 8,133 veh-h/y | 9,760 pers-h/y |
| Cost | 176,849 \$/y | 176,849 \$/y |
| Fuel Consumption | 11,981 gal/y | |
| Carbon Dioxide | 106,781 kg/y | |
| Hydrocarbons | 11 kg/y | |
| Carbon Monoxide | 118 kg/y | |

NOx

84 kg/y

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APPENDIX E – ALTERNATIVES COMPARISON BACK-UP

Alternatives Performance Comparison

| Performance Measure | Traffic Signal Alternative | Roundabout Alternative |
|--|----------------------------|-----------------------------------|
| Cumulative Condition | | |
| Delay - All approaches LOS "D" or better LOS A rated at 5 and E rated at 1. | 2.4 ✓ | 4.8 ✓✓ |
| 95 th % Queue - Adequate queue storage | ✓ | ✓✓ |
| Future Investment Needs | | |
| Service Life – function past the design year | D ✓ | B ✓✓ |
| Costs | | |
| Operations & Maintenance - Annualized | \$3,000 | \$1,700 ✓ |
| Collision Costs - Annualized | \$150,100 | \$100,800 ✓ |
| Delay Costs - Annualized | \$36,000 | \$11,000 ✓ |
| Fuel Costs - Annualized | \$21,000 | \$20,000 ✓ |
| Environmental Costs - Annualized | \$1,505 | \$1,505 |
| Capital Costs - Annualized | \$48,000 ✓ | \$119,000 |
| Truck Accommodations | | |
| Serves design vehicle for all movements | ✓ | ✓ |
| Safety | | |
| Predictive Measures - Greatest crash reduction potential for expected fatal and injury crashes | 17% | 56% ✓ |
| Vehicle Conflicts - The number of potential conflict points that may occur at the intersection based on layout geometry | 32 | 8 ✓ |
| Pedestrian Safety - Exposure to traffic in terms of number of lanes, conflict points, crossing times, and expected vehicular speeds. | 4 35-45 mph | 1 15-25mph ✓✓ |
| Bicycle Safety - Exposure to traffic in terms of number of lanes, conflict points, and speed differential | | ✓ |
| Property Impacts | | |
| Property Impacts | ✓✓ | |
| Local Access | | |
| Maintains local access and circulation | ✓ | ✓ |
| Total Performance Measures Met | 8 | 17 |

Performance Measures Procedures/Definitions

Except where noted, a check mark will be placed in each category for the alternative that performs the best. In instances where both alternatives meet the criteria, each will receive a check mark.

Delay: Level of Service (LOS) A will be rated at 5.0 and E will be rated at 1.0. The average score is shown as a composite of each approach's AM and PM LOS score. A check mark is given to the alternative that has all approaches scoring a LOS of D or higher in both peak hours. Another check mark is given to the alternative with the highest score.

95th Percentile Queue: Adequate queue storage provided to prevent blocking of turning movements by approach will get a check mark.

Service Life: Will the alternative function acceptably beyond the design year.

Operations and Maintenance: Total annualized cost for landscape maintenance, electrical service, signal maintenance, and pavement rehabilitation.

Crash Costs: Derived from applying crash reduction factors (CRF) per FHWA "Desktop Reference for Crash Reduction Factors".

Delay Costs: Cumulative vehicle delay derived from SIDRA multiplied by \$18.95/hr; per Caltrans Life-Cycle Benefit-Cost Analysis Economic Parameters 2016.

Fuel Costs: Derived from SIDRA: fuel consumption * \$3.18/gal per Caltrans Life-Cycle Benefit-Cost Analysis Economic Parameters 2016.

Environmental Costs: Emissions derived from SIDRA: CO * \$80/ton, and NOx * \$18,700/ton; per Caltrans Life-Cycle Benefit-Cost Analysis Economic Parameters 2016.

Capital Cost (Annualized): Total Construction + ROW Cost divided by Service Life (20 yr).

Serves Design Vehicle for All Movements: Check mark if all movements are served for the design vehicle

Safety Predictive Measures: Greatest crash reduction potential based on fatal and injury crashes between the alternatives.

Vehicle Conflicts: Number of conflict points.

Pedestrian Safety: Most # of lanes crossed at a time, expected vehicle speeds

Bicycle Safety: Access, exposure to traffic, and speed differential (# conflict points * (vehicle speed - 15 mph average bicycle speed)).

Maintains existing access and circulation: Percentage of existing access/turning movements maintained.